TOWN OF VERNON Inland Wetlands Commission (IWC) Meeting Notice & Agenda **Tuesday April 20, 2021, 7:00 PM** VIA Teleconference

Join Zoom Meeting by link: https://us02web.zoom.us/j/81676941684?pwd=WGRtTml5ejhNWG5idXMrNWtDZm8wUT09

> Meeting ID: 816 7694 1684 Passcode: G5APTK or Dial by your location (646) 876 9923 Meeting ID: 816 7694 1684 Passcode: 424103

AGENDA

- 1. Call to Order & Roll Call
- 2. Administrative Actions
 - 2.1 Amendment/Adoption of Agenda Additional business to be considered under agenda item #8 "Other Business" requires Commission vote
 - 2.2 Approval of the Minutes from the March 23, 2021 regular meeting
 - 2.3 Communications received NOT related to Agenda items, if any
 - 2.4 Call for filing(s) of Intervener petition(s) and determination of status
- 3. New Applications for Receipt and Determination of Significance
- 4. Public Hearing and Action on New Application(s)
 - 4.1 Application **IWC-2021-03**, of The Town of Vernon, Town Engineer for a wetlands permit by Commission, for the repair of an erosion problem (Mary Lane Drainage Project) at 152 West St. (Assessor's ID: Map 21, Block 021F, Parcel 0002A). **[Action Only]**
 - 4.1 Application IWC-2021-04, of Rashid Hamid, for a wetlands re-designation and a wetlands permit by Commission, for the development of a +-70 unit townhouse residential project, at 291 and 293 Talcottville Rd. (Assessor ID: Map 3 Block 4 Parcels 9A & 9E) and at 27, 32, 37, 38, and 46 Naek Rd. (Assessor ID: Map 3 Block 4 Parcels 008-8, 7,4, 6, 5).
- 5. Status of Cease & Correct Orders, if any
- 6. Wetlands Enforcement Officer Report, if any
- 7. Inland Wetlands Agent Approvals, if any

8. Other Business

8.1 Draft Future Land Use Summary & Maps-Link Below

https://www.vernon-ct.gov/departments-services/departments/planning-and-development/pocd

9. Adjournment

Rachel Stansel, Chairperson Inland Wetlands Commission

Draft Minutes

Town of Vernon Inland Wetlands Commission (IWC) Tuesday, March 23, 2021, 7:00 p.m. Teleconference Meeting

DRAFT MINUTES

1. Call to Order and Roll Call

Chairperson Rachel Stansel called the meeting to order at 7:00 p.m. Also in attendance were Commission Members Don Schubert, and Kathy Minor. Staff members present were David Smith, Town Engineer, and George McGregor, Town Planner.

- 2. Administrative Actions
 - 2.1 Amendment/Adoption of Agenda Additional business to be considered under agenda item #8 "Other Business" requires Commission vote None
 - 2.2 Approval of Minutes from the February 23, 2021, regular meeting Don Schubert made a motion seconded by Kathy Minor to approve the minutes of February 23, 2021. Motion carried unanimously.
 - 2.3 Communications received NOT related to Agenda items, if any None
 - 2.4 Call for filing(s) of Intervener petition(s) and determination of status. None
- 3. New Applications for Receipt and Determination of Significance
 - 3.1 Application **IWC-2021-03**, of the Town of Vernon, Town Engineer for a wetlands permit by Commission, for the repair of an erosion problem (Mary Lane Drainage Project) at 152 West Street (Assessor's ID: Map 21, Block 021F, Parcel 0002A).

David Smith explained the application's purpose. Discussion took place.

Don Schubert made a motion seconded by Chairperson Stansel that the Inland Wetlands Commission finds that **IWC-2021-03**, an Application of Town of Vernon, does NOT represent a significant activity, and places it on the regular IWC for April 20, 2021, for ACTION. Motion carried unanimously.

3.2 Application **IWC-2021-04**, of Rashid Hamid, for a wetlands re-designation and a wetlands permit by Commission, for the development of a +-70 unit

townhouse residential project, at 291 and 293 Talcottville Rd. (Assessor ID: Map 3, Block 4, Parcels 9A and 9E) and at 27, 32, 37, 38, and 46 Naek Rd. (Assessor ID: Map 3, Block 4, Parcels 008-8,7,4,6,5).

Town Engineer explained the Application and project. Discussion took place.

Kathy Minor made a motion seconded by Chairperson Stansel that the Inland Wetlands Commission finds that **IWC-2021-04**, an Application of Rashid Hamid, represents a significant activity, and places it on the regular IWC for April 20, 2021, for Public Hearing ACTION. Motion carried unanimously.

- 4. Public Hearing and Action on New Application(s)
 - 4.1 Application **IWC-2021-01**, of Richard and Julie Clay for a wetlands permit by Commission, for the construction of a +-2,500 s.f. single-family home at 58 Wildwood Dr. (Assessor's ID: Map 52, Block 139, Parcel 50)

Town Engineer explained the Application and plans. Discussion took place.

Chairperson Stansel made a motion second by Don Schubert that the Vernon Inland Wetlands and Watercourses Commission does hereby APPROVE the Application **(IWC-2021-01)** for a Wetlands permit by Commission, subject to the plan dated February 9, 2021, revised March 5, 2021, prepared by Bongiovanni Group, Inc. and based upon the following findings:

- 1. The project will have no adverse impacts on wetlands or watercourses;
- 2. The mitigation measures are acceptable. Motion carried unanimously.
- 4.2 Application IWC-2021-02, of Pam Gieras for a wetlands permit by Commission, for the construction of a +2,200 s.f. single-family home at 7 Beechwood Rd. (Assessor's ID: Map 52, Block 140F, Parcels 2,3,4,5)

Town Engineer discussed the Application. Discussion took place.

Chairperson Stansel made a motion seconded by Kathy Minor that the Vernon Inland Wetlands and Watercourses Commission does hereby APPROVE, the application **(IWC-2021-02)** for a Wetlands permit by Commission, subject to the plan dated February 15, 2021, revised March 5, 2021, prepared by Bushnell Associates, LLC, and based upon the following findings:

- 1. The project will have no adverse impacts on wetlands or watercourses;
- 2. The mitigation measures are acceptable. Motion carried unanimously.
- 5. Status of Cease & Correct Orders, if any None

- 6. Wetlands Enforcement Officer Report, if any None
- 7. Inland Wetlands Agent Approvals, if any
 - 7.1 **WA-2021-03** 205 Lake Street, for the work associated with the proposed access drive as shown on the proposed site plans provide to the Wetlands Agent Certified Letter dated March 5, 2021, included in Commission packet.
- 8. Other Business
 - 8.1 Connecticut Association of Wetland Scientists 2021 Meeting. Information included in Commission packet.
- 9. Adjournment

Meeting adjourned at 7:25p.m.

Respectfully Submitted

Susan Hewett Recording Secretary

APPLICATION 1

IWC-2021-03



TOWN OF VERNON INLAND WETLANDS COMMISSION (IWC)

APPLICATION

This form is to be used to apply to the Vernon Inland Wetlands Commission (IWC) for approval for a redesignation of a wetlands area, a change to the Inland Wetlands and Watercourses Regulations, and/or a permit to conduct a regulated activity in a wetland, watercourse, or upland review area (URA), which are defined as areas within one hundred (100) feet from the boundary of a wetland, watercourse, or intermittent watercourse and areas within two hundred (200) feet from the boundary of Gage's Brook, Hockanum River, Ogden Brook, Railroad Brook, Tankerhoosen River, Valley Falls Pond, Walker Reservoir East, Walker Reservoir West. Any activity that the Commission determines is likely to impact or affect wetlands or watercourses may be considered a regulated activity. **Provide all the information requested**.

The Applicant must be the property owner, the property owner's agent, the Town of Vernon, or someone with a direct financial interest in the subject property. Said interest shall be explained. If the applicant is not the property owner, written permission for this Application must be obtained from the property owner and submitted by letter signed by the property owner authorizing submission of the Application.

The Applicant understands that the Application is complete only when all information and documents required by IWC have been submitted and that any approval by the IWC relies upon complete and accurate information being provided by the Applicant. Incorrect information provided by the Applicant may make the approval invalid. The IWC may require additional information to be provided by the Applicant.

I. APPLICANT (S)
Name: Town of Vernon David Smith
Title: Town Engineer
Company: Town of Vernon
Address: 55 West Main St.
Telephone: <u>860-870-3664</u> Fax: <u>860-870-3683</u>
E-mail: dasnith@vernon-ct.gov
II. PROPERTY OWNERS
Name: Richard A Bruley
Title: NA
Company: N/H
Address: 152 West St.
Telephone: Fax:
E-mail:

III. PROPERTY
Address: 152 West St.
Assessor ID Code: Map # 2 Block # 021F Lot/Parcel # 0002 A
Land Record Reference to Deed Description: Volume: 2333 Page 18
USGA Location: Rockville
Circle the Map Quadrangle Name: Manchester # 38 Rockville #39
Circle the Sub regional Drainage Basin #: 3108 4500 4502 4503
Zoning District: $\int -22$
IV. PROJECT
Project Name: Mary Lane Prainage Improvements
Project Contact Person:
Name: David Snith, P.E., L.S.
Title: Town Engineer
Company: Town of Vernon
Address: 55 West Main St.
Telephone: 860-870-3664 Fax: 860-870-3683
E-mail: dasmith @ vernon-ct.gov
V. PROJECT SUMMARY
Describe the project briefly in regard to the purpose of the project and the activities that will occur. Attach to this application a complete and detailed description with maps and documentation as required by the "The Town of Vernon Inland Wetlands and Watercourses Regulations".
Purpose: Repair an erasion problem
General Activities: re-shape eroded embankment, deposit
various sized rock for stabilization, create plunge pool area.
Regulated Activities:
Watercourse disturbance (linear feet):
Wetlands disturbance (acres or sq. ft.):
Upland Review Area (URA) disturbance: Acres
Nonregulated activities & activities outside URA: ACHCS

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VI. APPLICATION

- Redesignation of Wetlands
- Amendment of Inland Wetlands and Watercourses Regulations
- Modification of a Wetlands Redesignation

Wetlands Permit

- Non-significant activity
- _____ Significant activity with less than ½ acre site disturbance
- Significant activity with site disturbance from ½ acre to and including 2 acres
- Significant activity with site disturbance greater than 2 acres
- Commission modification of a wetland permit in effect
- Modification of a wetland permit by ;the Wetlands Agent
- Approval of a license by the Wetlands Agent for activities in an upland
- Appeal of a decision by the Wetlands Agent
 - Subdivision review per CGS Section 8-26
 - Jurisdictional ruling regarding permitted and nonregulated uses
 - Waiver, reduction, or delayed payment of fees (attach statement of justification)
 - V Waiver
 - ____ Reduction to \$____
 - Delay of payment to

VII. CERTIFICATION AND SIGNATURE

I, the undersigned Applicant or applicant's Agent, hereby certify that I have reviewed the "Town of Vernon Inland Wetlands and Watercourses Regulations" and have prepared this Application with complete and accurate information.

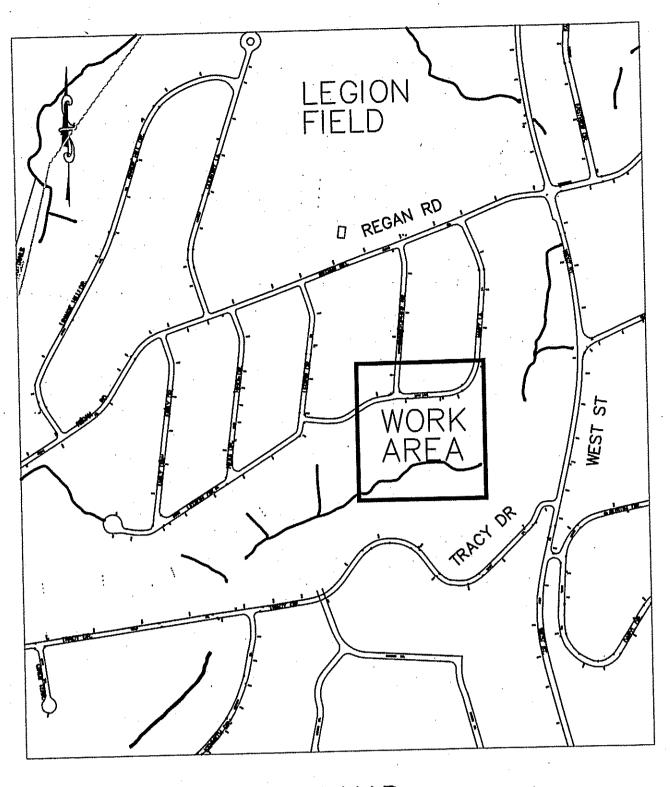
Property owner, Applicant, or Applicant	's Agent:	r 1
hall	DAVID A. SMITH	39/21
Applicant or Agent Signature	Printed Name	Date
Owner's Signature, if different	Printed Name	

TO BE FILLED IN BY THE PLANNING DEPARTMENT

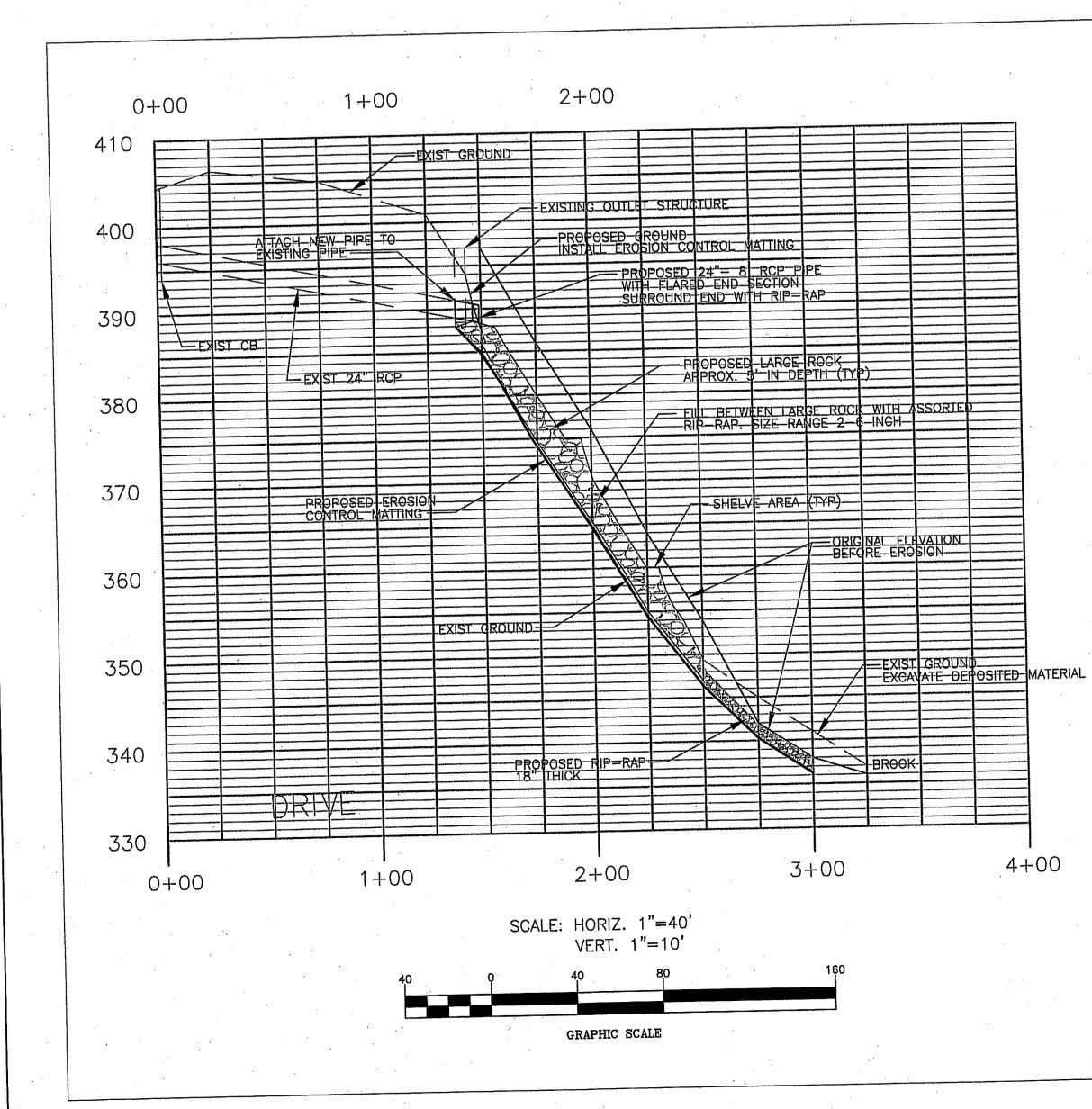
DATE APPLICATION SUBMITTED

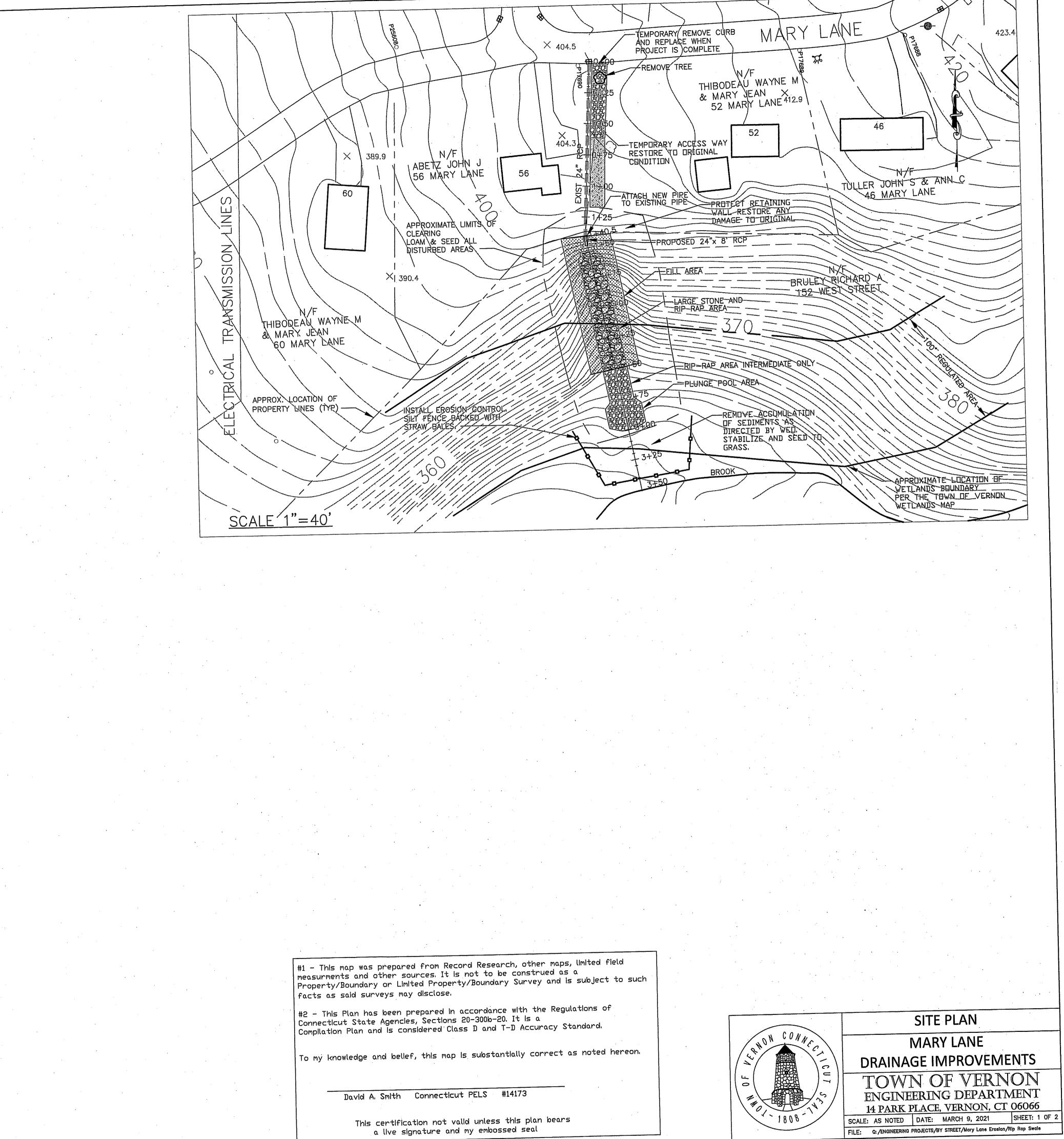
DATE APPLICATION RECEIVED BY COMMISSION

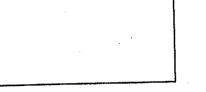
IWC:FILE:

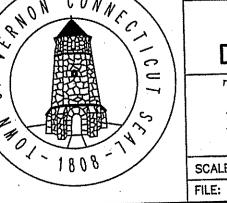


KEY MAP SCALE 1"=500'









GENERAL NOTES -

1. ALL WORK MUST BE PERFORMED IN ACCORDANCE WITH THESE PLANS, SPECIFICATIONS, AND CONDITIONS OF APPROVAL, AND ALL APPLICABLE REQUIREMENTS, RULES, REGULATIONS, STATUTORY REQUIREMENTS, CODES, LAWS, AND STANDARDS OF ALL GOVERNMENTAL ENTITIES WITH JURISDICTION OVER THIS PROJECT. 2. THE TOWN OF VERNON (TOV) PUBLIC WORKS DEPARTMENT (PWD) MUST FIELD VERIFY EXISTING CONDITIONS AND NOTIFY THE TOV ENGINEERING DEPARTMENT, IN WRITING, IMMEDIATELY IF ACTUAL CONDITIONS DIFFER FROM THOSE SHOWN ON THE PLAN, OR IF THE PROPOSED WORK CONFLICTS WITH ANY OTHER SITE FEATURES. 3. ALL DIMENSIONS SHOWN ON THE PLANS MUST BE FIELD VERIFIED BY THE PWD PRIOR TO THE START OF CONSTRUCTION. PWD MUST NOTIFY THE TOV ENGINEERING DEPARTMENT, IN WRITING, IF ANY CONFLICTS OR DISCREPANCIES EXIST PRIOR TO PROCEEDING WITH CONSTRUCTION.

4. THE PWD IS RESPONSIBLE FOR REPAIRING ANY DAMAGE DONE TO ANY PROPERTY DURING THE COURSE OF CONSTRUCTION. 5. ALL CONSTRUCTION AND MATERIALS MUST COMPLY WITH AND CONFORM TO APPLICABLE FEDERAL, STATE AND LOCAL REGULATIONS, LAWS, ORDINANCES, RULES AND CODES, AND ALL APPLICABLE OSHA REQUIREMENTS.

GENERAL EROSION AND SEDIMENT CONTROL NOTES -

1. ALL EROSION AND SEDIMENT CONTROLS MEASURES SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STANDARDS AND SPECIFICATIONS OF THE "GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL" BY THE CONNECTICUT COUNCIL ON SOIL AND WATER CONSERVATION. 2. ALL SEDIMENT CONTROL PRACTICES AND MEASURES SHALL BE CONSTRUCTED, APPLIED AND MAINTAINED IN ACCORDANCE WITH THE APPROVED SEDIMENT CONTROL PLAN. EROSION CONTROLS MUST BE INSPECTED AFTER EACH RAINFALL. 3. SILT SHALL BE REMOVED FROM BARRIERS IF GREATER THAN 6-INCHES

DEEP OR AS NEEDED. 4. DAMAGED OR DETERIORATED ITEMS WILL BE REPAIRED IMMEDIATELY AFTER IDENTIFICATION. 5. TOPSOIL REQUIRED TO ESTABLISH VEGETATION SHALL BE STOCKPILED IN THE AMOUNT NECESSARY TO COMPLETE THE FINISHED GRADING OF ALL THE DISTURBED AREAS.

6. AREAS TO BE FILLED SHALL BE CLEARED, GRUBBED AND STRIPPED OF TOPSOIL, PRIOR TO FILLING. 7. ALL FILL AREAS ARE TO BE COMPACTED AS REQUIRED TO MINIMIZE EROSION, SLIPPAGE AND SETTLEMENT. FILL INTENDED TO SUPPORT STRUCTURES, DRAINAGE, ETC. SHALL BE COMPACTED IN ACCORDANCE WITH THE APPROPRIATE STATE AND LOCAL SPECIFICATIONS. 8. FILL MATERIALS SHALL BE FREE OF BRUSH, RUBBISH, LARGE ROCKS, LOGS, STUMPS, BUILDING MATERIALS, COMPRESSIBLE MATERIALS AND ALL OTHER MATERIALS WHICH MAY INTERFERE WITH OR PREVENT CONSTRUCTION OF SATISFACTORY FILLS.

9. FROZEN MATERIAL, SOFT MUCK, HIGHLY COMPRESSIBLE MATERIALS AND OTHER OBJECTIONABLE MATERIALS SHALL NOT BE INCORPORATED INTO FILLS. 10. SEEPS AND SPRINGS ENCOUNTERED DURING CONSTRUCTION SHALL BE HANDLED IN ACCORDANCE WITH ACCEPTED INDUSTRY STANDARDS. 11. ALL GRADING AREAS SHALL BE PERMANENTLY STANDARDS. FOLLOWING ESTABLISHMENT OF THE FINAL GRADE. IF FINISHED GRADING IS TO BE DELAYED FOR MORE THAN 30 DAYS AFTER DISTURBANCE, TEMPORARY SOIL STABILIZATION MEASURES, INCLUDING TEMPORARY SEEDING, SHALL BE APPLIED. 12. TOPSOIL SHALL BE SPREAD TO A MINIMUM DEPTH OF 4". IMPORT TOPSOIL AS NEEDED TO SUPPLEMENT RESERVED TOPSOIL. 13. APPLY SEED UNIFORMLY BY HAND, CYCLONE SEEDER, DRILL CULTIPACKER

TYPE SEEDER OR HYDROSEEDER. NORMAL SEEDING DEPTH IS FROM ¼" TO ½". HYDROSEEDING WHICH IS MULCHED MAY BE LEFT ON THE SURFACE. 14. WHERE FEASIBLE, EXCEPT WHERE EITHER A CULTIPACKER SEEDER OR HYDROSEEDING IS USED, THE SEEDBED SHOULD BE FIRMED FOLLOWING SEEDING WITH A ROLLER OR LIGHT DRAG. 15. INSPECT THE SEEDED PRIOR TO SEEDING. IF TRAFFIC HAS LEFT THE SOIL COMPACTED, THE AREA MUST BE RE-TILLED BEFORE SEEDING.

CT DOT FORM 816

M.12.02 RIP RAPI

M.12.02.1 STANDARD, THE MATERIAL SHLL CONFORM TO THE FOLLOWING REQUIREMENTS: NOT MORE THAN 15% LESS THAN 6', NO STONE LARGER THAN 30', 75% AT LEAST 15".

M.12.02.2 INTERMEDIATE: THE MATERIAL SHLL CONFORM TO THE FOLLOWING REQUIREMENTS:

STONE SIZE	<u>% OF THE WEIGHT</u>
18 in	0
10 in to 18 in	30-50
6 In to 10 In	30-50
4 in to 6 in	20-30
2 In to 4 In	10-20
less than 2 in	0-10

M.12.02.2 INTERMEDIATE: THE MATERIAL SHLL CONFORM TO THE FOLLOWING REQUIREMENTS:

STONE SIZE	% OF THE WEIGHT
10 In	0
6 In to 10 In	20-50
4 In to 6 In	. 30-60
2 In to 4 in	30-40
1 In to 2 In	10-20
less than 1 in	0-10

SUGGESTED CONSTRUCTION SEQUENCE -

- DEFINE LIMITS OF CLEARING. ESTABLISH ANTI-TRACKING ENTRANCE. . REMOVE TREES AND WOODY VEGETATION WITHIN CLEARING LIMITS. INSTALL SILTATION BARRIER. RESHAPE SWALE AREA. USE DEPOSITED MATERIAL FROM LOWER AREA AND ANY ADDITIONAL SUITABLE MATERIAL AS NEEDED. COMPACT SOIL. . INSTALL EROSION CONTROL MATTING. PLACE LARGE ROCK AND ASSORTED RIP-RAP WITHIN THE FILL AREA. SHAPE FILL AREA TO DESIRED CONTOUR. CREATE SHELF AREAS WITHIN THE FILL AREA. CREATE PLUNGE POOL AREA. 10. INSTALL NEW RCP PIPE AND FLARED END OVER SUITABLE COMPACTED MATERIAL. 11. RESHAPE SURROUNDING ROCK AND RIP-RAP AS NEEDED. 12. RESHAPE ANY DISTURBED AREAS. 13. LOAM AND SEED ALL DISTURBED AREAS.
- 14. REMOVE SAND BAGS FROM CATCH BASIN, IF NECESSARY. 15. REMOVE ANTI-TRACKING PAD.
- 16. RESTORE TEMPORARY ACCESS DRIVE. 17. REMOVE EROSION CONTROLS WHEN THE SITE IS FULLY STABILIZED.

NOTES -

- 1. PROPOSED GRADES ARE GUIDELINES AND WILL BE ADJUSTED FOR FIELD CONDITIONS RELATED TO CUTS AND FILLS. PERIMETER AEAS THAT ARE DISTURBED, BUT ULTIMATELY NOT PROTECTED WITH RIP-RAP SHALL BE STABILIZED, SEEDED TO GRASS AND MULCHED.
 SHOULDERS OF PIPING AND DISTURBED AREAS ABOVE THE DISCHARGE TO ALSO BE PROTECTED BY RIP-RAP. 4. THE TOV ENGINEERING DEPARTMENT IS SUGGESTING THAT A SAND BAG
- MAJOR WASH-OUT BEFORE THE SWALE IS FULLY CONSTRUCTED.

CT DOT - 2" (MIN.) CRUSHED STONE

PLAN NOT TO SCALE

PLUG BE INSTALLED IN THE EXISTING CATCH BASIN LOCATED ON MARY LANE PRIOR TO CONSTRUCTION OF THE FILL AREA. THIS MAY PREVENT A

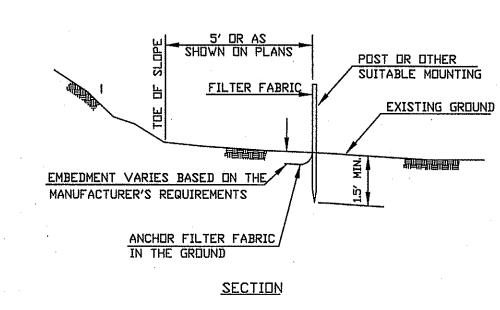
-ALIGN WITH EXISTING PAVEMENT

4" MINIMUN DEPTH-----

COMPACTED SUBGRADE -----

CONSTRUCTION PROJECT PROGRESSES. 3. THE CONTRACTOR SHALL DAILY, OR AS DIRECTED, SWEEP THE PAVED RUADWAYS ADJACENT TO THE WORK AREA AND CONDUCT HIS ACTIVITIES TO MINIMIZE THE TRACKING OF SOIL ONTO THE ROADWAYS,

GENERAL NOTES



1, THE CONTRACTOR SHALL INSTALL AND MAINTAIN THE EROSION CONTROL

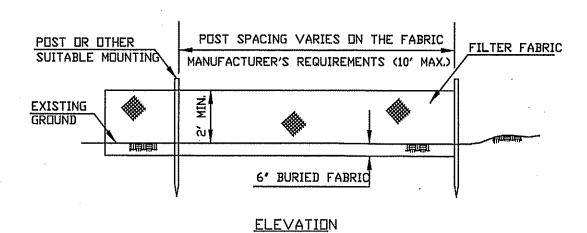
ACTIVITY WHICH DISTURBS EXISTING VEGETATIVE GROUND COVER.

ADDITIONAL MEASURES, AS REQUIRED, TO CONTROL EROSION AS THE

2. SEDIMENTATION AND ERUSION CONTROL MEASURES SHOWN ARE THE

MINIMUM REQUIRED, CONTRACTOR SHALL INSTALL AND MAINTAIN

SYSTEM AS SHOWN ON THE PLANS PRIOR TO INITIATING ANY CONSTRUCTION



SEDIMENTATION CONTROL SYSTEM - GEOTEXTILE FENCE NOT TO SCALE

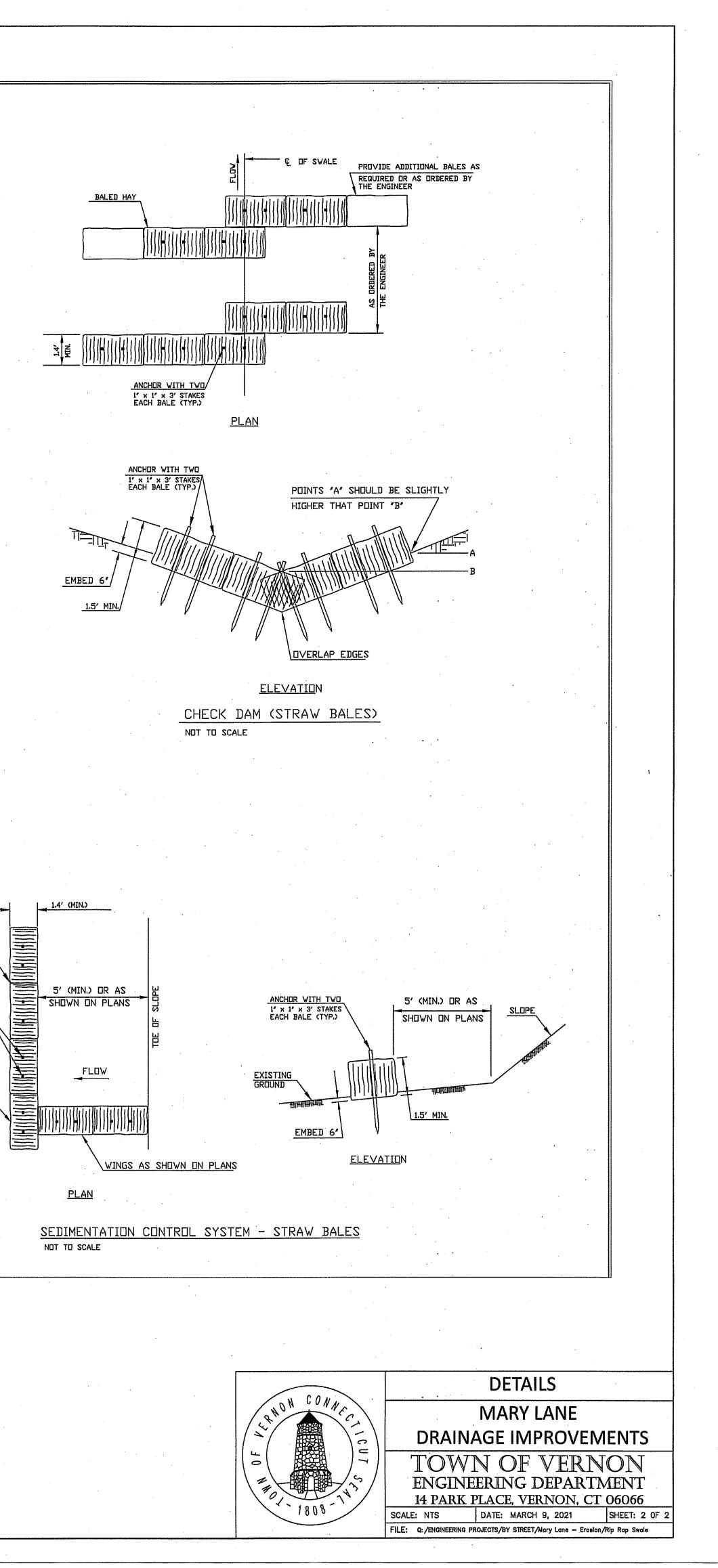
EXISTING PAVEMENT /--- 2" (MIN.) CRUSHED STONE BALES TO BUTT TOGETHER FILTER FABRIC -COMPACTED SUBGRADE ANCHOR WITH TWO 1' × 1' × 3' STAKES EACH BALE (TYP.)

SECTION NOT TO SCALE

BALED STRAW

ANTI-TRACKING PAD

AS SHOWN



STAFF COMMENTS



TOWN OF VERNON

55 West Main St., VERNON, CT 06066-3291 (860) 870-3640 gmcgregor@vernon-ct.gov

OFFICE OF THE TOWN PLANNER

MEMORANDUM

TO: Inland Wetlands Commission

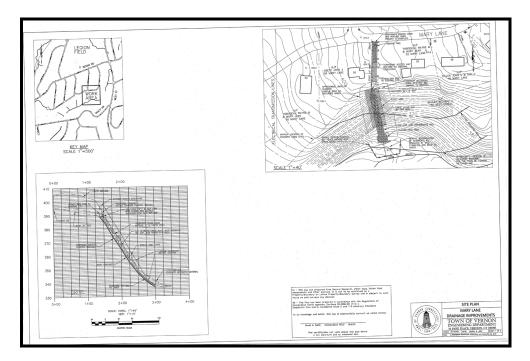
FROM: George K. McGregor, AICP, Town Planner

SUBJECT: IWC 2021-03, Mary Lane Drainage

DATE: March 23, 2021

Request

Application **IWC-2021-03**, of The Town of Vernon, Town Engineer for a wetlands permit by Commission, for the repair of an erosion problem (Mary Lane Drainage Project) at 152 West St. (Assessor's ID: Map 21, Block 021F, Parcel 0002A). The proposal plans to reshape an eroded embankment, deposit rock for stabilization, and create a plunge hole area.



Staff Comments

There are no outstanding issues.

Draft Motions

MOVED, that the Vernon Inland Wetlands and Watercourses Commission does hereby APPROVE, the application **(IWC-2021-03)** for a Wetlands permit by Commission, subject to the site plan entitled *Mary Lane Drainage Improvements* dated March 9, 2021, prepared by the Town of Vernon, and based upon the following findings:

1. The project will have no adverse impacts on wetlands or watercourses;

OR

MOVED, an Alternate Motion

GKM

APPLICATION 2

RECEIVED

MAR 182021



TOWN OF VERNON OWN PLANNERS OFFICE INLAND WETLANDS COMMISSION (IWC)

APPLICATION

This form is to be used to apply to the Vernon Inland Wetlands Commission (IWC) for approval for a redesignation of a wetlands area, a change to the Inland Wetlands and Watercourses Regulations, and/or a permit to conduct a regulated activity in a wetland, watercourse, or upland review area (URA), which are defined as areas within one hundred (100) feet from the boundary of a wetland, watercourse, or intermittent watercourse and areas within two hundred (200) feet from the boundary of Gage's Brook, Hockanum River, Ogden Brook, Railroad Brook, Tankerhoosen River, Valley Falls Pond, Walker Reservoir East, Walker Reservoir West. Any activity that the Commission determines is likely to impact or affect wetlands or watercourses may be considered a regulated activity. **Provide all the information requested.**

The Applicant must be the property owner, the property owner's agent, the Town of Vernon, or someone with a direct financial interest in the subject property. Said interest shall be explained. If the applicant is not the property owner, written permission for this Application must be obtained from the property owner and submitted by letter signed by the property owner authorizing submission of the Application.

The Applicant understands that the Application is complete only when all information and documents required by IWC have been submitted and that any approval by the IWC relies upon complete and accurate information being provided by the Applicant. Incorrect information provided by the Applicant may make the approval invalid. The IWC may require additional information to be provided by the Applicant.

I. APPLICANT (S)

Name: Rashid Hamid

Title: President

Company: Naek Construction Co., Inc.

Address: 27 Naek Road, Vernon, CT 06066

Telephone: 860-875-1895 Fax: 860-872-3251

E-mail: rashidnaek@aol.com

II. PROPERTY OWNERS

Name: The Rashid Hamid Family, LLP

Title: N/A

Company: c/o Naek Construction Company, Inc.

Address: 27 Naek Road

Vernon, CT 06066

Telephone: 860-875-1895 Fax: 860-872-3251

E-mail: rashidnaek@aol.com

			<u>, III. I</u>	PROPE	RTY	
Address: 291 and 293	Talcottville Road	and 26	, 32, 37	, 38, an	d 46 Nael	k Road
Assessor ID Code:	Map # <u>03</u>	Block #	0004		Lot/Par	cel # <u>See atta</u> chment
Land Record Reference	e to Deed Descrij	otion:	Volum	ie:		Page <u>See atta</u> chment
USGA Location:						
Circle the Map Quadrar	igle Name:	Manch	ester #	38	XRockvil	le #39
Circle the Sub regional	Drainage Basin	#:	3108	X 4500	4502	4503
Zoning District: PDZ-G	erber Farm Area					
			<u>IV.</u>	PROJ	ECT	
Project Name: Village a	at Naek Road					
Project Contact Person	:					5
Name: Rashid Hamid						
Title: President						
Company: <u>Naek Const</u>	ruction Co., Inc.					
Address: 27 Naek Roa	ad					
Vernon, CT	06066					
Telephone: <u>860-875-1</u>	895		Fax: <u>86</u>	50-872-3	3251	
E-mail: <u>rashidnaek@a</u>	ol.com					

V. PROJECT SUMMARY

Describe the project briefly in regard to the purpose of the project and the activities that will occur. Attach to this application a complete and detailed description with maps and documentation as required by the "The Town of Vernon Inland Wetlands and Watercourses Regulations".

Purpose: Development of the Village at Naek Road, a residential townhouse community

General Activities: Site preparation, grading, and installation of utilities for construction of 70 townhouse

dwelling units in 17 buildings, with driveways, sidewalks, lighting, storm drainage, amenities, and other related improvements. Regulated Activities:

Watercourse disturbance (linear feet): None.

Wetlands disturbance (acres or sq. ft.): None.

Upland Review Area (URA) disturbance: 4.0 acres for construction of stormwater basin, storm drainage,

buildings, driveways, utilities, and parking areas.

Nonregulated activities & activities outside URA: <u>8.2 acres for construction of stormwater basin, storm</u> drainage, buildings, driveways, utilities, sidewalks, and parking areas.

VI. APPLICATION

- X Redesignation of Wetlands
- Amendment of Inland Wetlands and Watercourses Regulations
- ____ Modification of a Wetlands Redesignation
- X____ Wetlands Permit
 - ____ Non-significant activity
 - Significant activity with less than ½ acre site disturbance
 - Significant activity with site disturbance from ½ acre to and including 2 acres
 - X Significant activity with site disturbance greater than 2 acres
 - Commission modification of a wetland permit in effect
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- Approval of a license by the Wetlands Agent for activities in an upland
- Appeal of a decision by the Wetlands Agent
- _____ Subdivision review per CGS Section 8-26
- _____ Jurisdictional ruling regarding permitted and nonregulated uses
- Waiver, reduction, or delayed payment of fees (attach statement of justification)
 - _____ Waiver
 - ____ Reduction to \$_____
 - ____ Delay of payment to _____

VII. CERTIFICATION AND SIGNATURE

I, the undersigned Applicant or applicant's Agent, hereby certify that I have reviewed the "Town of Vernon Inland Wetlands and Watercourses Regulations" and have prepared this Application with complete and accurate information.

Property Owner, Applicant, or Applicant's Agent:

than hormand	Rashid Hamid	
Applicant or Agent Signature	Printed Name	Date
Handwins	Rashid Hamid	
Owner's Signature, if different	Printed Name	Date

TO BE FILLED IN BY THE PLANNING DEPARTMENT

DATE APPLICATION SUBMITTED	
DATE APPLICATION RECEIVED BY COMMISSION	

TOWN OF VERNON INLAND WETLANDS COMMISSION (IWC) SUPPLEMENT TO APPLICATION

PURPOSE AND DESCRIPTION OF PROPOSED ACTIVITY, PROPOSED EROSION AND SEDIMENTATION CONTROLS AND OTHER MANAGEMENT PRACTICES

The Vernon Inland Wetlands and Watercourses Regulations require a statement of the purpose and a description of the proposed activity and proposed erosion and sedimentation controls and other management practices and mitigation measures which may be considered as a condition of issuing a permit for the proposed regulated activity including, but not limited to, measures to (1) prevent or minimize pollution or other environmental damage, (2) maintain or enhance existing environmental quality, (3) in the following order of priority: restore, enhance, and create productive wetland or watercourse resources; and (4) mitigate the impact of the proposed activity.

The report from George Logan, Professional Wetland Scientist, Associate Wildlife Biologist, Soil Scientist, and Ecologist, at REMA Ecological Services, LLC provides this information.

ALTERNATIVE THAT WOULD CAUSE LESS OR NO ENVIRONMENTAL IMPACT TO WETLANDS OR WATERCOURSES

The Regulations require the Applicant to state an alternative which would cause less or no environmental impact to wetlands or watercourses and why the alternative as set forth in the application was chosen, with all such alternatives diagramed on a site plan or drawing. Because the proposed activities will not have any environmental impact to wetlands or watercourses, no statement of alternatives is necessary.

ECOLOGICAL COMMUNITIES AND FUNCTIONS OF WETLANDS OR WATERCOURSES

The Regulations require descriptions of the following: (1) the ecological communities and functions of the wetlands or watercourses involved with the Application and the effects of the proposed activity on these communities and wetland functions; and (2) how the Applicant will change, diminish, or enhance the ecological communities and functions of the wetlands or watercourses involved in the application and each alternative which would cause less or no environmental impact to wetlands or watercourses, and a description of why each alternative considered was deemed neither feasible nor prudent.

The report from George Logan, Professional Wetland Scientist, Associate Wildlife Biologist, Soil Scientist, and Ecologist, at REMA Ecological Services, LLC provides this information.

STATEMENTS AND CERTIFICATIONS BY APPLICANT

1. The Applicant is familiar with all the information provided in the Application.

2. The Applicant certifies the accuracy of the Application and all supporting information.

3. The Applicant is aware of the penalties for obtaining a permit through deception or through inaccurate or misleading information.

4. The Applicant authorizes the members and agents of the Commission to inspect the subject land, at reasonable times, during the pendency of an application and for the life of the permit.

5. The Applicant certifies the following:

a. No portion of the property on which the regulated activity is proposed is located within 500 feet of the boundary of an adjoining municipality;

b. No traffic attributable to the completed project on the site will use streets within an adjoining municipality to enter or exit the site;

c. No sewer or water drainage from the project site will flow through and impact the sewage or drainage system within an adjoining municipality; and

d. No water run-off from the improved site will impact streets or other municipal or private property within an adjoining municipality.

TOWN OF VERNON INLAND WETLANDS COMMISSION (IWC) SUPPLEMENT TO APPLICATION

PARCEL IDENTIFICATION INFORMATION

Address: 291 Talcottville Road Map #03 Block #0004 Lot/Parcel #0009A Assessor's ID Code: Land Record Reference to Deed Description: Volume 2592 Page 218 Address: 293 Talcottville Road Map #03 Block #0004 Lot/Parcel #0009E Assessor's ID Code: Land Record Reference to Deed Description: Volume 2592 Page 218 Address: 26 Naek Road Map #03 Block #0004 Lot/Parcel #008-8 Assessor's ID Code: Land Record Reference to Deed Description: Volume 2097 Page 54 Address[.] 32 Naek Road Assessor's ID Code: Map #03 Block #0004 Lot/Parcel #008-7 Land Record Reference to Deed Description: Volume 2097 Page 54 37 Naek Road Address: Map #03 Block #0004 Lot/Parcel #008-4 Assessor's ID Code: Land Record Reference to Deed Description: Volume 2097 Page 54 38 Naek Road Address: Assessor's ID Code: Map #03 Block #0004 Lot/Parcel #008-6 Land Record Reference to Deed Description: Volume 2097 Page 54 Address: 46 Naek Road Assessor's ID Code: Map #03 Block #0004 Lot/Parcel #008-5 Land Record Reference to Deed Description: Volume 2097 Page 54

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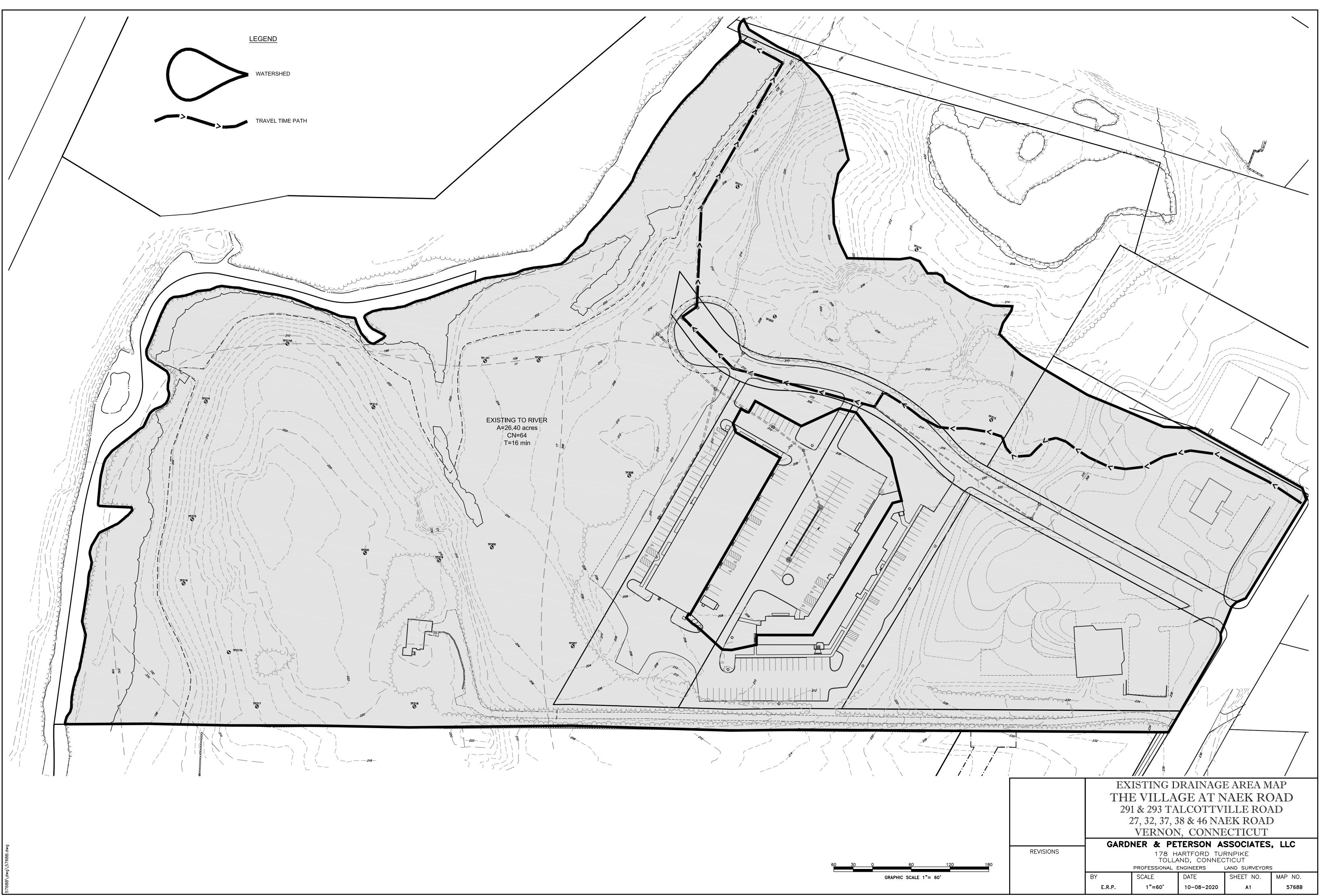
5. The Applicant certifies the following:

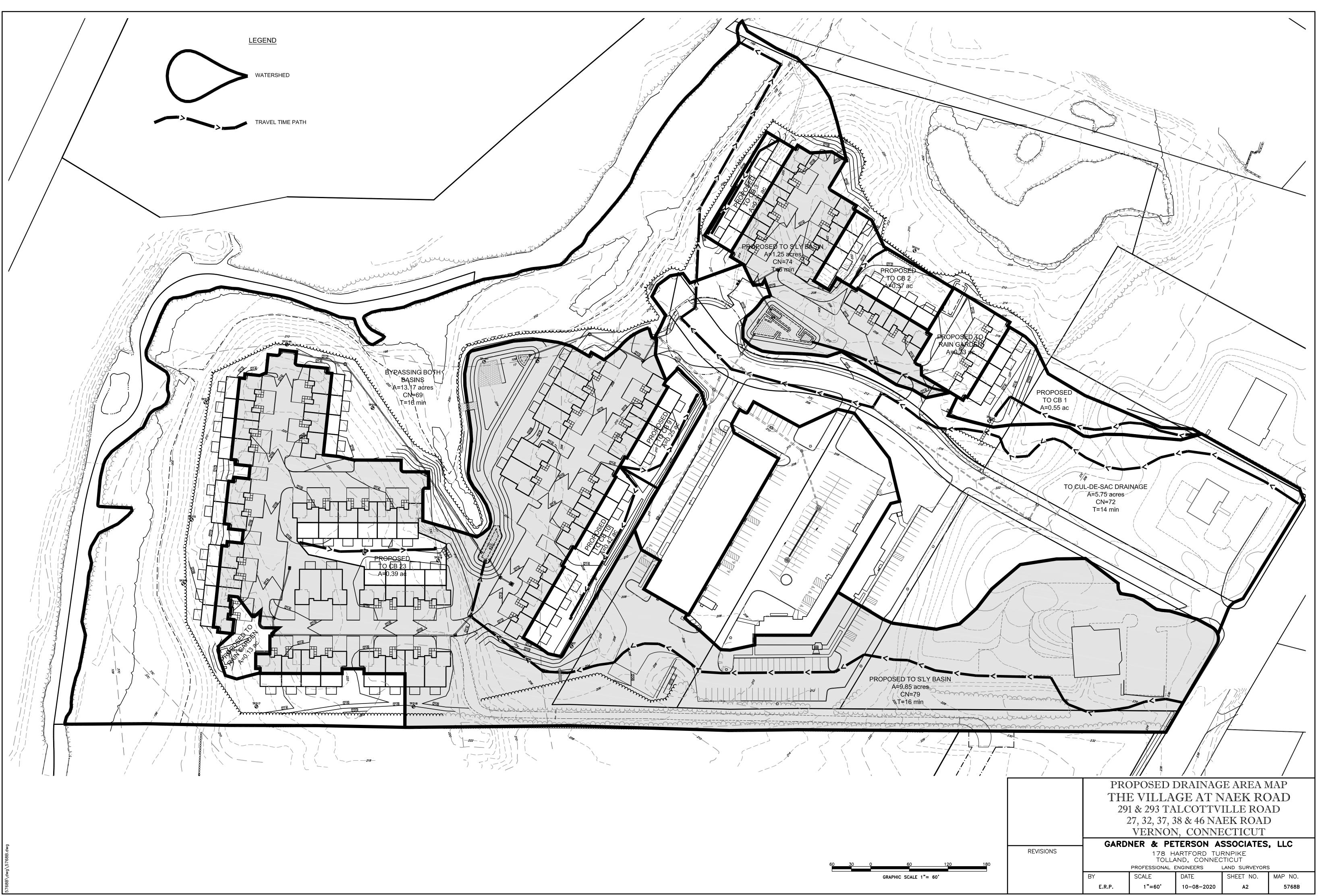
a. No portion of the property on which the regulated activity is proposed is located within 500 feet of the boundary of an adjoining municipality;

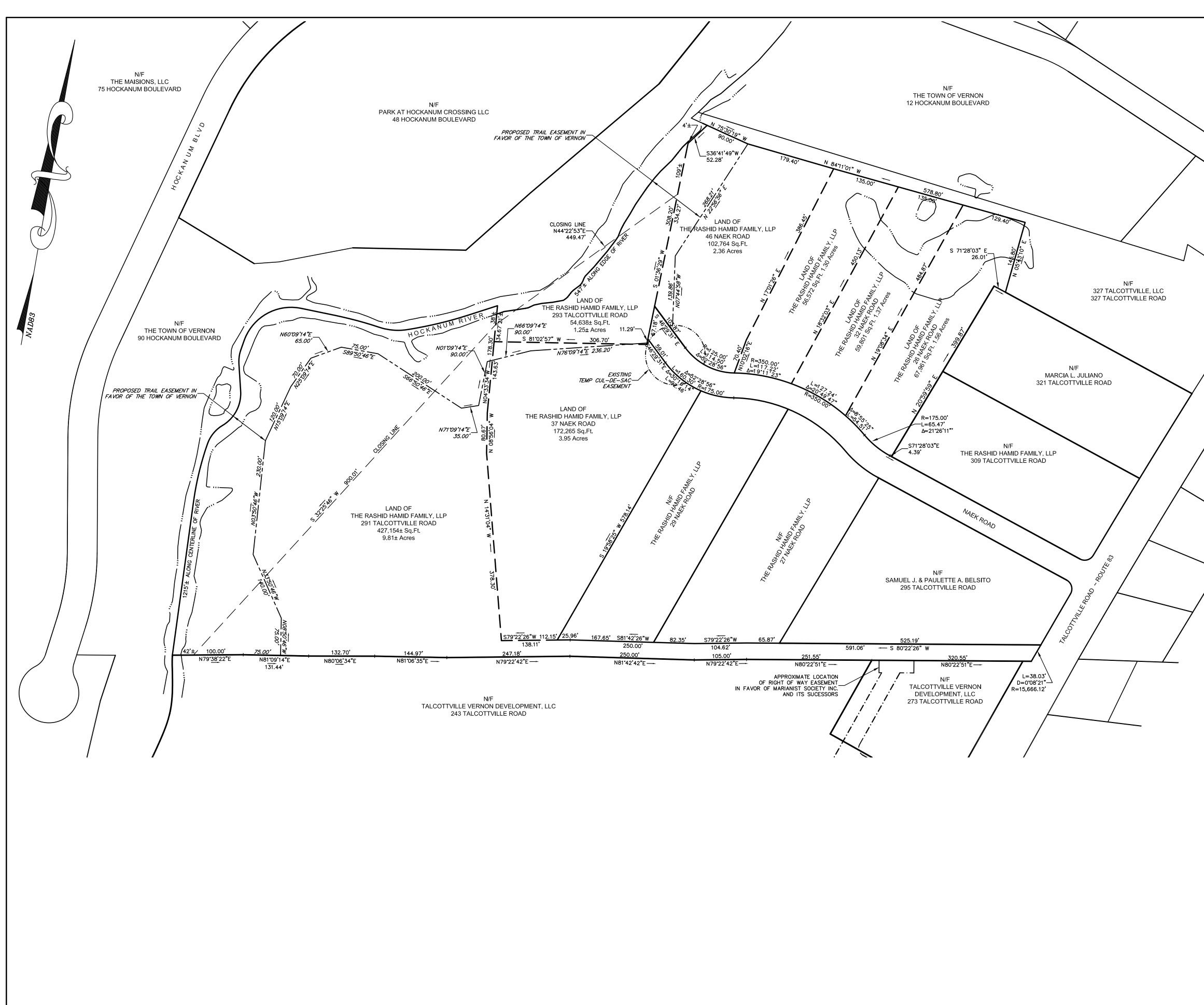
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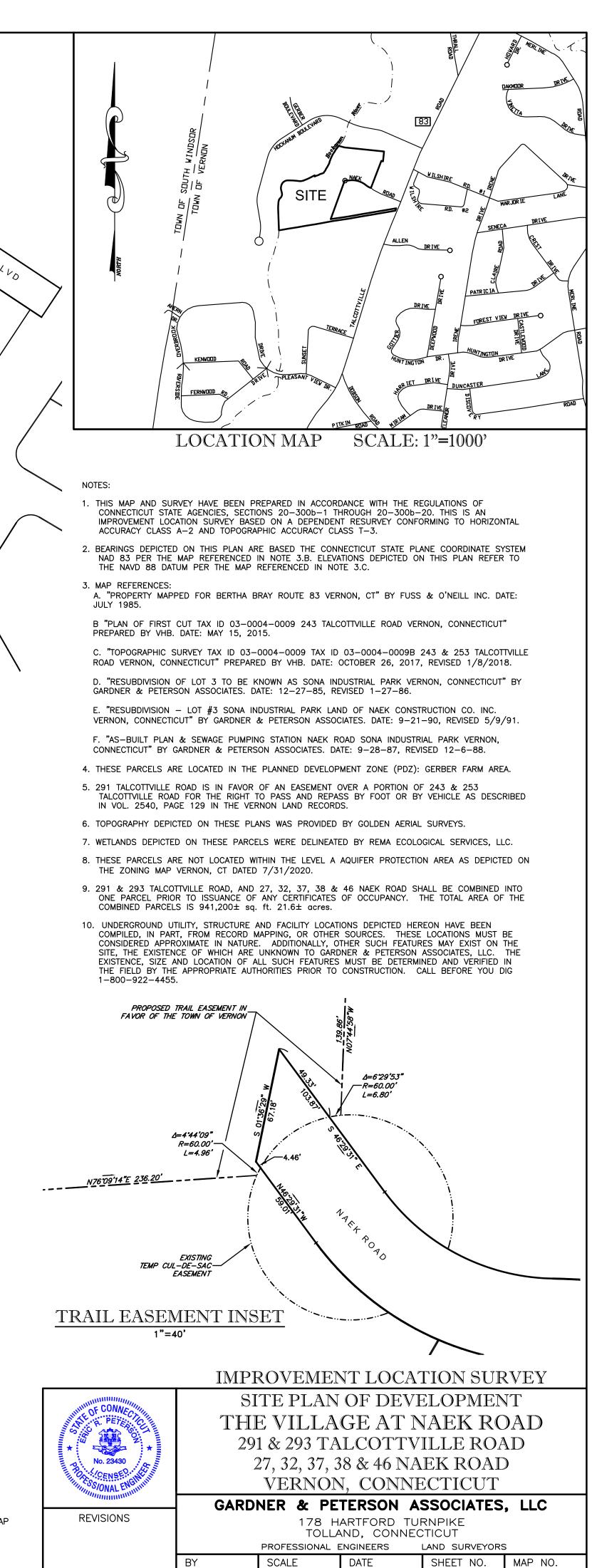




I HEREBY DECLARE THAT, TO THE BEST OF MY KNOWLEDGE AND BELIEF, THIS MAP IS SUBSTANTIALLY CORRECT AS NOTED HEREON.







E.R.P.

1"=100'

03-17-2021

1 OF 10

5768B



N)TES:
1.	THIS MAP AND SURVEY HAVE BEEN PREPARED IN ACCORDANCE WITH THE REGULATIONS OF CONNECTICUT STATE AGENCIES, SECTIONS 20-300b-1 THROUGH 20-300b-20. THIS IS AN IMPROVEMENT LOCATION SURVEY BASED ON A DEPENDENT RESURVEY CONFORMING TO HORIZONTAL ACCURACY CLASS A-2 AND TOPOGRAPHIC ACCURACY CLASS T-3.
2.	BEARINGS DEPICTED ON THIS PLAN ARE BASED THE CONNECTICUT STATE PLANE COORDINATE SYSTEM NAD 83 PER THE MAP REFERENCED IN NOTE 3.B. ELEVATIONS DEPICTED ON THIS PLAN REFER TO THE NAVD 88 DATUM PER THE MAP REFERENCED IN NOTE 3.C.
3.	MAP REFERENCES: A. "PROPERTY MAPPED FOR BERTHA BRAY ROUTE 83 VERNON, CT" BY FUSS & O'NEILL INC. DATE: JULY 1985.
	B "PLAN OF FIRST CUT TAX ID 03–0004–0009 243 TALCOTTVILLE ROAD VERNON, CONNECTICUT" PREPARED BY VHB. DATE: MAY 15, 2015.
	C. "TOPOGRAPHIC SURVEY TAX ID 03-0004-0009 TAX ID 03-0004-0009B 243 & 253 TALCOTTVILLE ROAD VERNON, CONNECTICUT" PREPARED BY VHB. DATE: OCTOBER 26, 2017, REVISED 1/8/2018.
	D. "RESUBDIVISION OF LOT 3 TO BE KNOWN AS SONA INDUSTRIAL PARK VERNON, CONNECTICUT" BY GARDNER & PETERSON ASSOCIATES. DATE: 12–27–85, REVISED 1–27–86.
	E. "RESUBDIVISION – LOT #3 SONA INDUSTRIAL PARK LAND OF NAEK CONSTRUCTION CO. INC. VERNON, CONNECTICUT" BY GARDNER & PETERSON ASSOCIATES. DATE: $9-21-90$, REVISED 5/9/91.
	F. "AS-BUILT PLAN & SEWAGE PUMPING STATION NAEK ROAD SONA INDUSTRIAL PARK VERNON, CONNECTICUT" BY GARDNER & PETERSON ASSOCIATES. DATE: 9–28–87, REVISED 12–6–88.
4.	THESE PARCELS ARE LOCATED IN THE PLANNED DEVELOPMENT ZONE (PDZ): GERBER FARM AREA.
5.	291 TALCOTTVILLE ROAD IS IN FAVOR OF AN EASEMENT OVER A PORTION OF 243 & 253 TALCOTTVILLE ROAD FOR THE RIGHT TO PASS AND REPASS BY FOOT OR BY VEHICLE AS DESCRIBED IN VOL. 2540, PAGE 129 IN THE VERNON LAND RECORDS.
6.	TOPOGRAPHY DEPICTED ON THESE PLANS WAS PROVIDED BY GOLDEN AERIAL SURVEYS.
7.	WETLANDS DEPICTED ON THESE PARCELS WERE DELINEATED BY REMA ECOLOGICAL SERVICES, LLC.
8.	THESE PARCELS ARE NOT LOCATED WITHIN THE LEVEL A AQUIFER PROTECTION AREA AS DEPICTED ON THE ZONING MAP VERNON, CT DATED 7/31/2020.
9.	291 & 293 TALCOTTVILLE ROAD, AND 27, 32, 37, 38 & 46 NAEK ROAD SHALL BE COMBINED INTO ONE PARCEL PRIOR TO ISSUANCE OF ANY CERTIFICATES OF OCCUPANCY. THE TOTAL AREA OF THE COMBINED PARCELS IS 941,200 \pm sq. ft. 21.6 \pm acres.
10	. UNDERGROUND UTILITY, STRUCTURE AND FACILITY LOCATIONS DEPICTED HEREON HAVE BEEN COMPILED, IN PART, FROM RECORD MAPPING, OR OTHER SOURCES. THESE LOCATIONS MUST BE CONSIDERED APPROXIMATE IN NATURE. ADDITIONALLY, OTHER SUCH FEATURES MAY EXIST ON THE SITE, THE EXISTENCE OF WHICH ARE UNKNOWN TO GARDNER & PETERSON ASSOCIATES, LLC. THE EXISTENCE, SIZE AND LOCATION OF ALL SUCH FEATURES MUST BE DETERMINED AND VERIFIED IN THE FIELD BY THE APPROPRIATE AUTHORITIES PRIOR TO CONSTRUCTION. CALL BEFORE YOU DIG 1-800-922-4455.
	HEREBY DECLARE THAT, TO THE BEST OF MY KNOWLEDGE AND BELIEF, THIS MAP SUBSTANTIALLY CORRECT AS NOTED HEREON.

ERIC R. PETERSON

L.S. 23430 REGISTRATION NO.

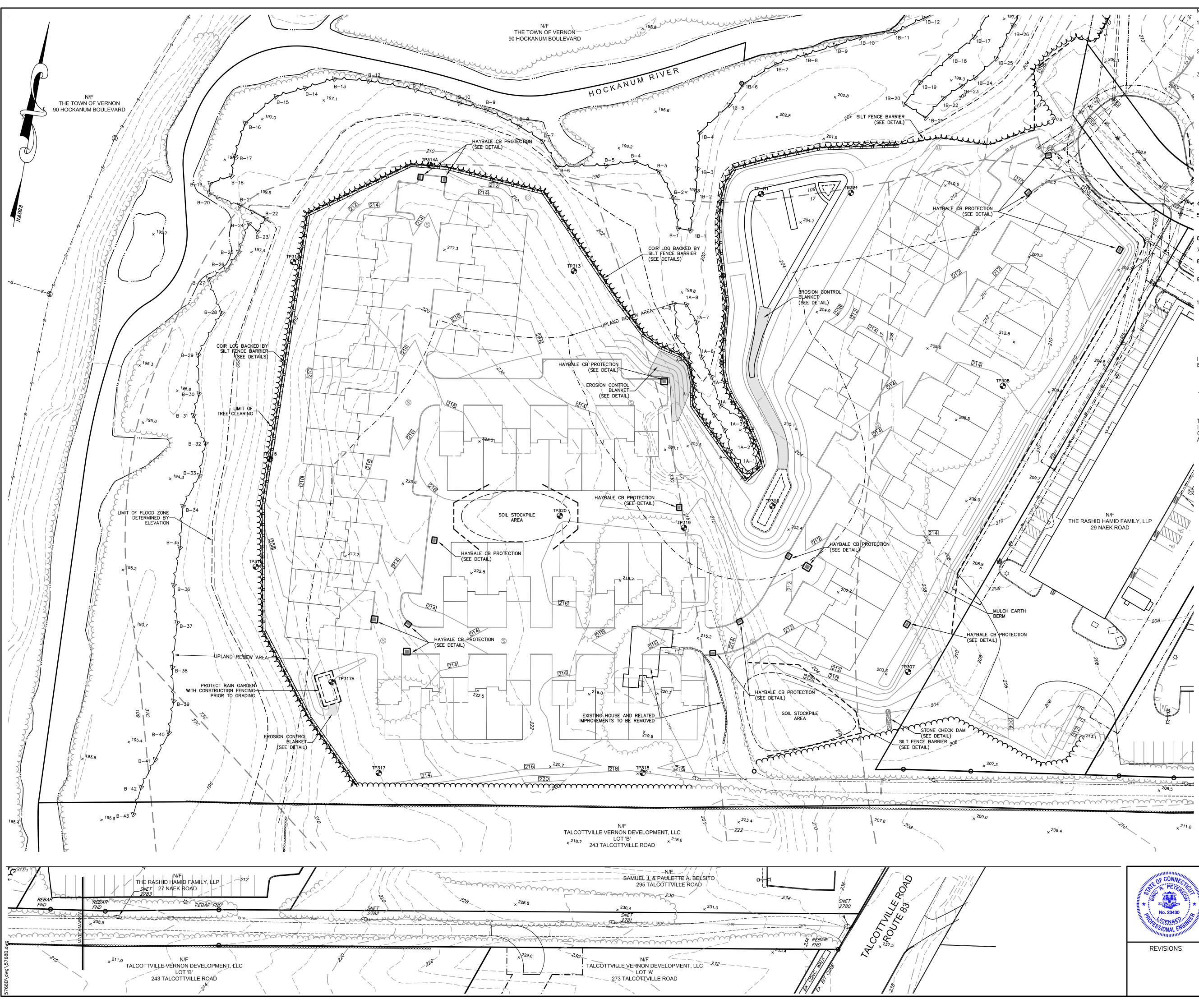
THE WETLAND SOILS ON THIS PROPERTY WERE IDENTIFIED IN THE FIELD USING THE CRITERIA REQUIRED BY CONNECTICUT P.A. 72–155 AS AMENDED BY P.A. 73–571 AND ARE ACCURATELY REPRESENTED ON THIS PLAN.

Nezze / Jogan GEORGE T. LOGAN, M\$, PWS Registered Soil Scientist



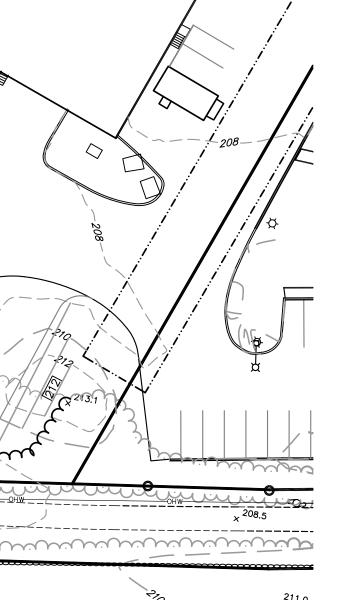
EXISTING	LEGEND	PROPOSED
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	MONUMENT FOUND	
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x603.5	SPOT ELEVATION	×603.5
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	CATCH BASIN/CULVERT	
	STORM MANHOLE	Ø
	FOOTING DRAIN	F
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Ķ	HYDRANT	<b>X</b>
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No. 23430		27, 32, 37, 3	88 & 46 NA	EK ROAL	
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	GARD	NER & PE	TERSON A	SSOCIATES	, LLC
REVISIONS			ARTFORD TUR		
		PROFESSIONAL	*	LAND SURVEYORS	6
	BY	SCALE	DATE	SHEET NO.	MAP NO.
	E.R.P.	1"=40'	03-17-2021	2 OF 10	5768B



	NOTES:	
	1. THIS MAP AND SURVEY HAVE BEEN PREPARED IN CONNECTICUT STATE AGENCIES, SECTIONS 20–300 IMPROVEMENT LOCATION SURVEY BASED ON A DEF HORIZONTAL ACCURACY CLASS A-2 AND TOPOGRA	b-1 THROUGH 20-300b-20. THIS IS AN PENDENT RESURVEY CONFORMING TO
209 3	2. BEARINGS DEPICTED ON THIS PLAN ARE BASED TH SYSTEM NAD 83 PER THE MAP REFERENCED IN N REFER TO THE NAVD 88 DATUM PER THE MAP RE	OTE 3.B. ELEVATIONS DEPICTED ON THIS PLAN
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	C. "TOPOGRAPHIC SURVEY TAX ID 03-0004-0009 TALCOTTVILLE ROAD VERNON, CONNECTICUT" PREPAI REVISED 1/8/2018.	
298.8	D. "RESUBDIVISION OF LOT 3 TO BE KNOWN AS SO BY GARDNER & PETERSON ASSOCIATES. DATE: 12-	
	E. "RESUBDIVISION – LOT #3 SONA INDUSTRIAL PA VERNON, CONNECTICUT" BY GARDNER & PETERSON 5/9/91.	
	F. "AS-BUILT PLAN & SEWAGE PUMPING STATION N CONNECTICUT" BY GARDNER & PETERSON ASSOCIAT	
	eq 4. These parcels are located in the planned di	EVELOPMENT ZONE (PDZ): GERBER FARM AREA.
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209.8	I HEREBY DECLARE THAT, TO THE BEST OF MY KN IS SUBSTANTIALLY CORRECT AS NOTED HEREON.	OWLEDGE AND BELIEF, THIS MAP
	Vic R. Poter	L.S. 23430
× / /////	ERIC R. PETERSON	REGISTRATION NO.

L.S. 23430 REGISTRATION NO. THE WETLAND SOILS ON THIS PROPERTY WERE IDENTIFIED IN THE FIELD USING THE CRITERIA REQUIRED BY CONNECTICUT P.A. 72–155 AS AMENDED BY P.A. 73–571 AND ARE ACCURATELY REPRESENTED ON THIS PLAN. No. 23430 122de 1. Abgan GEORGE T. LOGAN, MS, PWS Registered Soil Scientist LEGEND EXISTING PROPOSED PROPERTY BOUNDARY ZONING SETBACK _____ EASEMENT ____ . . ___ . . ___ . . ___ . . ___ IRON PIN/PIPE FOUND 0 MONUMENT FOUND 600 ELEVATION CONTOUR ×603.5 x603.5 SPOT ELEVATION TREE LINE  $\sim\sim\sim\sim$ SANITARY SEWER — — — s—_s— — s— = = = = = =CATCH BASIN/CULVER1 STORM MANHOLE D FOOTING DRAIN -----F------— — 💑 w___ ___w_ WATER MAIN ______₩_____ Ъ. HYDRANT — _____G___ _____ GAS MAIN ____G______



N/F

THE RASHID HAMID FAMILY, I 29 NAEK ROAD

x^{211.0} × ^{209.4}

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	GRAPHIC SCALE 1"= 40'
	IMPROVEMENT LOCATION SURVEY
	EROSION & SEDIMENT CONTROL PLAN
	THE VILLAGE AT NAEK ROAD
	291 & 293 TALCOTTVILLE ROAD
mm.	27, 32, 37, 38 & 46 NAEK ROAD
in.	VERNON, CONNECTICUT
	GARDNER & PETERSON ASSOCIATES, LLC
	178 HARTFORD TURNPIKE TOLLAND, CONNECTICUT
	PROFESSIONAL ENGINEERS LAND SURVEYORS

DATE

03-17-2021

LIGHT

UTILITY POLE

OVERHEAD WIRES

SIGN

TEST PIT

SOIL CLASSIFICATION

SILT FENCE

COIR LOG

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SCALE

1"=40'

E.R.P.

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SHEET NO.

3 OF 10

MAP NO.

5768B

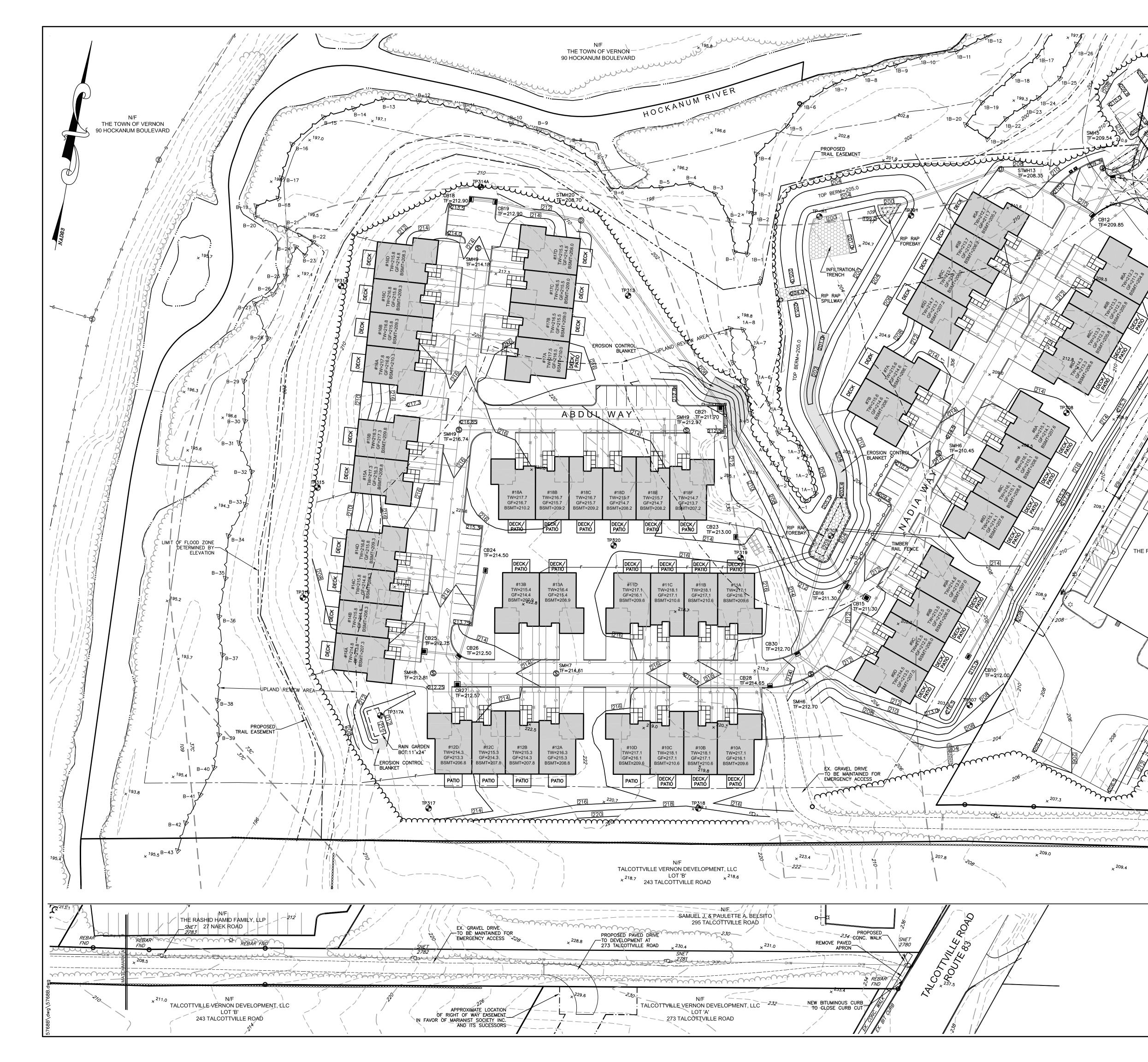
REVISIONS



CONNECTICUT STAT	TE AGENCIES, SECTIONS 20-3	N ACCORDANCE WITH THE REGU 500b-1 THROUGH 20-300b-20. DEPENDENT RESURVEY CONFORM JRACY CLASS T-3.	THIS IS AN
NAD 83 PER THE		THE CONNECTICUT STATE PLANE 3.B. ELEVATIONS DEPICTED ON T ED IN NOTE 3.C.	
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		9 TAX ID 03-0004-0009B 243 B. DATE: OCTOBER 26, 2017, R	
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ERIC R. PETER	RSON	L.S. 23430 REGISTRATION NO.	*
THE WETLAND SOILS IN THE FIELD USING	ON THIS PROPERTY WERE THE CRITERIA REQUIRED I	REGISTRATION NO. IDENTIFIED BY	* No. 23430
THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7	ON THIS PROPERTY WERE	REGISTRATION NO. IDENTIFIED BY 2.A. 73–571	1 AND
THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7	ON THIS PROPERTY WERE THE CRITERIA REQUIRED I 72-155 AS AMENDED BY F LY REPRESENTED ON THIS Jogan AN, M\$, PWS	REGISTRATION NO. IDENTIFIED BY 2.A. 73–571	1 AND
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THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7 AND ARE ACCURATEL	ON THIS PROPERTY WERE THE CRITERIA REQUIRED BY P LY REPRESENTED ON THIS AN, MS, PWS Scientist EXISTING	IDENTIFIED         A. 73-571         PLAN.         PLAN.         PROPERTY BOUNDARY         ZONING SETBACK         EASEMENT         IRON PIN/PIPE FOUND         MONUMENT FOUND         ELEVATION CONTOUR         SPOT ELEVATION         TREE LINE         SANITARY SEWER	<u>PROPOSI</u>
THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7 AND ARE ACCURATEL	ON THIS PROPERTY WERE THE CRITERIA REQUIRED BY P PLY REPRESENTED ON THIS ANY, M\$, PWS Scientist	IDENTIFIED         A. 73-571         PLAN.         PROPERTY BOUNDARY         ZONING SETBACK         EASEMENT         IRON PIN/PIPE FOUND         MONUMENT FOUND         MONUMENT FOUND         SPOT ELEVATION         TREE LINE         SANITARY SEWER         CATCH BASIN/CULVERT         STORM MANHOLE	
THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7 AND ARE ACCURATEL	ON THIS PROPERTY WERE THE CRITERIA REQUIRED BY P LY REPRESENTED ON THIS AN, MS, PWS Scientist EXISTING	REGISTRATION NO.  IDENTIFIED Y A. 73–571 PLAN.  PROPERTY BOUNDARY PROPERTY BOUNDARY PROPERTY BOUNDARY ZONING SETBACK EASEMENT IRON PIN/PIPE FOUND MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION KELINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN	
THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7 AND ARE ACCURATEL	ON THIS PROPERTY WERE THE CRITERIA REQUIRED BY P PLY REPRESENTED ON THIS ANY, M\$, PWS Scientist	EGISTRATION NO.	
THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7 AND ARE ACCURATEL	ON THIS PROPERTY WERE THE CRITERIA REQUIRED BY P Y REPRESENTED ON THIS WATTON NY, MS, PWS Scientist	REGISTRATION NO.  DENTIFIED  A. 73–571 PLAN.  PROPERTY BOUNDARY PROPERTY BOUNDARY ZONING SETBACK EASEMENT IRON PIN/PIPE FOUND MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION ELEVATION CONTOUR SPOT ELEVATION FREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES	
THE WETLAND SOILS IN THE FIELD USING CONNECTICUT P.A. 7 AND ARE ACCURATEL	ON THIS PROPERTY WERE THE CRITERIA REQUIRED BY P LY REPRESENTED ON THIS MANN M\$, PWS Scientist	REGISTRATION NO.  IDENTIFIED  A. 73–571 PLAN.  PROPERTY BOUNDARY PROPERTY BOUNDARY PROPERTY BOUNDARY ZONING SETBACK EASEMENT IRON PIN/PIPE FOUND MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN HYDRANT GAS MAIN LIGHT UTILITY POLE	

IMPROVEMENT LOCATION SURVEY SITE GRADING PLAN THE VILLAGE AT NAEK ROAD 291 & 293 TALCOTTVILLE ROAD 27, 32, 37, 38 & 46 NAEK ROAD lo. 23430 VERNON, CONNECTICUT GARDNER & PETERSON ASSOCIATES, LLC REVISIONS 178 HARTFORD TURNPIKE TOLLAND, CONNECTICUT PROFESSIONAL ENGINEERS LAND SURVEYORS SHEET NO. MAP NO. SCALE DATE BY E.R.P. 1"=40' 03-17-2021 4 OF 10 5768B

GRAPHIC SCALE 1"= 40'



		S MAP AND SURVEY HAVE BE NNECTICUT STATE AGENCIES, PROVEMENT LOCATION SURVEY	EEN PREPARED IN ACCORDANC SECTIONS 20-300b-1 THROU Y BASED ON A DEPENDENT RE A-2 AND TOPOGRAPHIC ACCUR	GH 20-300b-20. THIS IS AN SURVEY CONFORMING TO
20g 3	SY: RE	STEM NAD 83 PER THE MAP		CUT STATE PLANE COORDINATE LEVATIONS DEPICTED ON THIS PLAN IN NOTE 3.C.
	A. "		THA BRAY ROUTE 83 VERNON,	CT" BY FUSS & O'NEILL INC.
	PRE	PLAN OF FIRST CUT TAX ID ( PARED BY VHB. DATE: MAY 1		ILLE ROAD VERNON, CONNECTICUT"
			D 03–0004–0009 TAX ID 03– NNECTICUT" PREPARED BY VHE	
$X \times X \times T$			BE KNOWN AS SONA INDUST CIATES. DATE: 12–27–85, REV	RIAL PARK VERNON, CONNECTICUT" 'ISED 1–27–86.
_CB11 TF=209.05	VER		DNA INDUSTRIAL PARK LAND OF DNER & PETERSON ASSOCIATES	F NAEK CONSTRUCTION CO. INC. S. DATE: 9–21–90, REVISED
	CON	INECTICUT" BY GARDNER & P	PETERSON ASSOCIATES. DATE: 9	SONA INDUSTRIAL PARK VERNON, 9–28–87, REVISED 12–6–88. 7 ZONE (PDZ): GERBER FARM AREA.
CB9 TF=211.00	5. 291 TAI DE	TALCOTTVILLE ROAD IS IN F LCOTTVILLE ROAD FOR THE R SCRIBED IN VOL. 2540, PAGE	FAVOR OF AN EASEMENT OVER RIGHT TO PASS AND REPASS B E 129 IN THE VERNON LAND F SE PLANS WAS PROVIDED BY (	A PORTION OF 243 & 253 Y FOOT OR BY VEHICLE AS RECORDS.
	7. WET	LANDS DEPICTED ON THESE	PARCELS WERE DELINEATED B	Y REMA ECOLOGICAL SERVICES, LLC FER PROTECTION AREA AS DEPICTED
	INT	O ONE PARCEL PRIOR TO IS		NAEK ROAD SHALL BE COMBINED OF OCCUPANCY. THE TOTAL AREA s.
		MPILED, IN PART, FROM REC INSIDERED APPROXIMATE IN N E SITE, THE EXISTENCE OF W E EXISTENCE, SIZE AND LOCA	ORD MAPPING, OR OTHER SOU JATURE. ADDITIONALLY, OTHER WHICH ARE UNKNOWN TO GARD ATION OF ALL SUCH FEATURES APPROPRIATE AUTHORITIES PR	DEPICTED HEREON HAVE BEEN IRCES. THESE LOCATIONS MUST BE SUCH FEATURES MAY EXIST ON ONER & PETERSON ASSOCIATES, LLC MUST BE DETERMINED AND CIOR TO CONSTRUCTION. CALL
209.8		EBY DECLARE THAT, TO THE BSTANTIALLY CORRECT AS N	E BEST OF MY KNOWLEDGE A NOTED HEREON.	ND BELIEF, THIS MAP
		. <u>R. Patere</u> eric r. peterson	L.S. 2 REGISTRAT	
				OF CONNECTION
	IN TH CONNI	VETLAND SOILS ON THIS PI E FIELD USING THE CRITER ECTICUT P.A. 72–155 AS / ARE ACCURATELY REPRESEN	RIA REQUIRED BY AMENDED BY P.A. 73–571	*
	E	Nesege T. Jogaz	2	* No. 23430 AND SURVEYOR
		EORGÉ T. LOGAN, M\$, PWS egistered Soil Scientist		SURVE SURVE
7				
N/F RASHID HAMID FAMILY, LLP 29 NAEK ROAD		EXISTING	LEGEND	PROPOSED
			PROPERTY BOUNDARY ZONING SETBACK	
			EASEMENT	
	~ /	0	IRON PIN/PIPE FOUND	
			MONUMENT FOUND	600
				600 x603.5
	108-11E	□ 6 ₀₀	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE	
	108-11	□ 6 ₀₀	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION	
	08-11	□ 6 ₀₀	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE	
208	08-11 X	□ 6 ₀₀	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN	×603.5 
	08-11 X	□ 6 ₀₀	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE	×603.5 
	08-11 X	$\Box$ $600$ $x603.5$ $SSS$ $===================================$	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN	×603.5 
	AND	$\Box$ $600$ $x603.5$ $SSS$ $===================================$	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT	×603.5 
208	DOB-TH		MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT	×603.5 
208			MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN	×603.5 
208			MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES	×603.5 
208			MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT	×603.5 
208			MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT	×603.5 
208			MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT	×603.5 
208			MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT SOIL CLASSIFICATION	
		$ \begin{array}{c}                                     $	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT SOIL CLASSIFICATION	
		$ \begin{array}{c}                                     $	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT SOIL CLASSIFICATION	x60315 S S S S C T X X X X X X X X X X X X X
		$ \begin{array}{c}                                     $	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT SOIL CLASSIFICATION	x60315 S S S S S S S S S S S S S
		$\begin{bmatrix} & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & $	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT SOIL CLASSIFICATION	x60315 S S S S S S S S S S S S S
		$ \begin{array}{c}                                     $	MONUMENT FOUND ELEVATION CONTOUR SPOT ELEVATION TREE LINE SANITARY SEWER CATCH BASIN/CULVERT STORM MANHOLE FOOTING DRAIN WATER MAIN HYDRANT GAS MAIN LIGHT UTILITY POLE OVERHEAD WIRES SIGN TEST PIT SOIL CLASSIFICATION	NEDIJE

REVISIONS

E.R.P.

ENIMON, CONNECTION GARDNER & PETERSON ASSOCIATES, LLC 178 HARTFORD TURNPIKE TOLLAND, CONNECTICUT PROFESSIONAL ENGINEERS LAND SURVEYORS SCALE DATE SHEET NO. MAP NO.

03-17-2021

1"=40'

5 OF 10

5768B

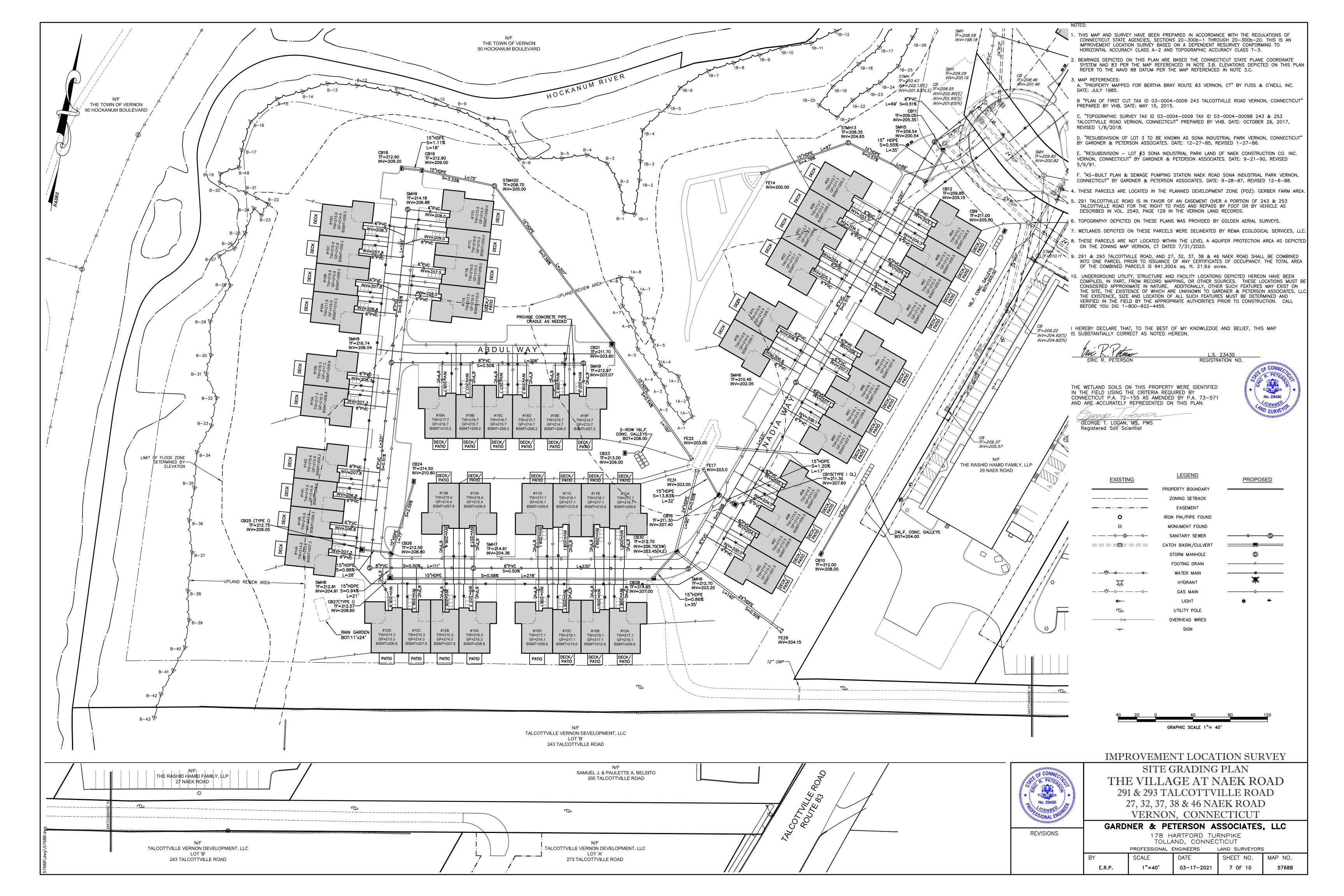


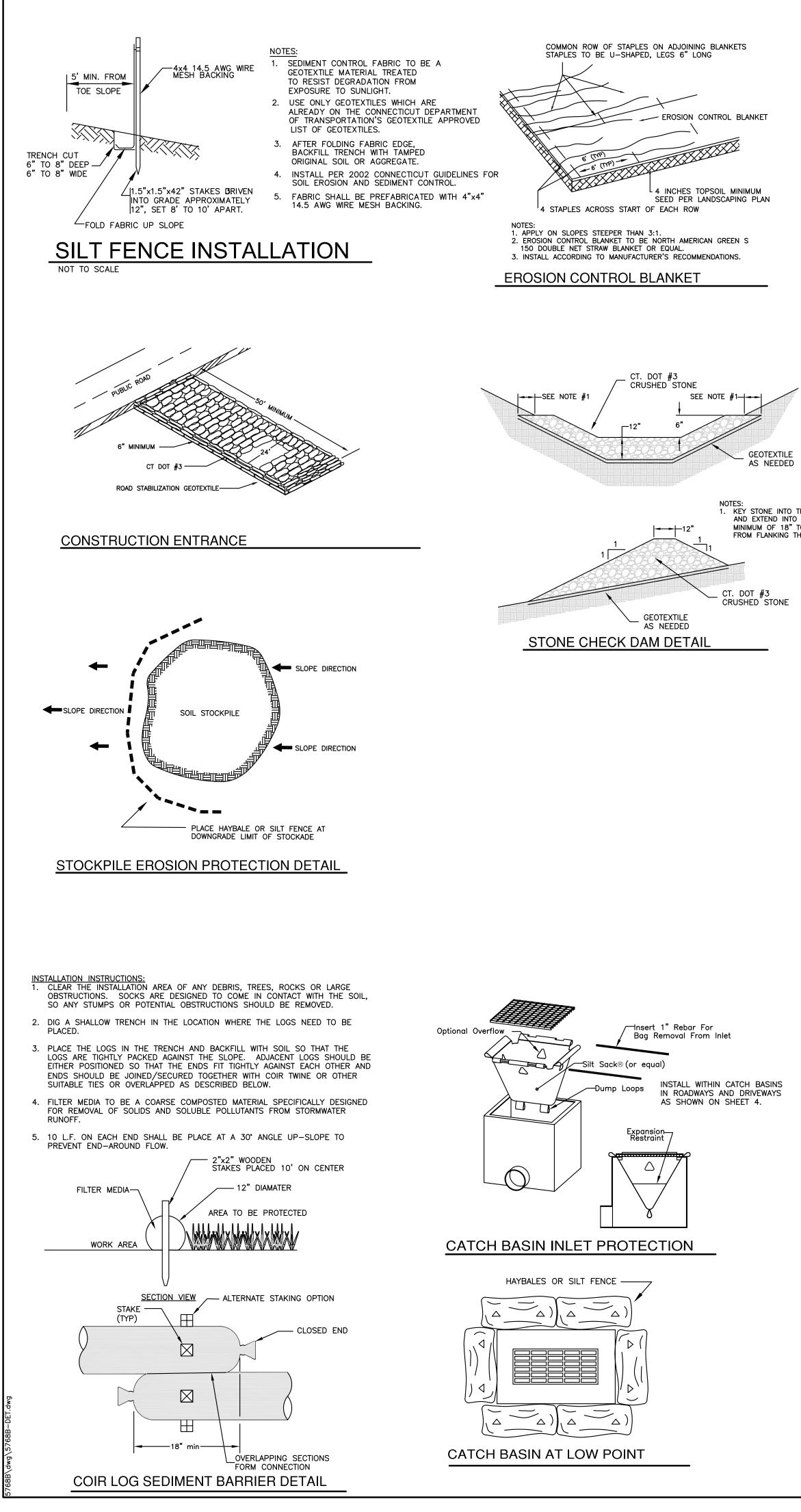
NC	DTES:
1.	THIS MAP AND SURVEY HAVE BEEN PREPARED IN ACCORDANCE WITH THE REGULATIONS OF CONNECTICUT STATE AGENCIES, SECTIONS 20–300b–1 THROUGH 20–300b–20. THIS IS AN IMPROVEMENT LOCATION SURVEY BASED ON A DEPENDENT RESURVEY CONFORMING TO HORIZONTAL ACCURACY CLASS A–2 AND TOPOGRAPHIC ACCURACY CLASS T–3.
2.	BEARINGS DEPICTED ON THIS PLAN ARE BASED THE CONNECTICUT STATE PLANE COORDINATE SYSTEM NAD 83 PER THE MAP REFERENCED IN NOTE 3.B. ELEVATIONS DEPICTED ON THIS PLAN REFER TO THE NAVD 88 DATUM PER THE MAP REFERENCED IN NOTE 3.C.
3.	MAP REFERENCES: A. "PROPERTY MAPPED FOR BERTHA BRAY ROUTE 83 VERNON, CT" BY FUSS & O'NEILL INC. DATE: JULY 1985.
	B "PLAN OF FIRST CUT TAX ID 03-0004-0009 243 TALCOTTVILLE ROAD VERNON, CONNECTICUT" PREPARED BY VHB. DATE: MAY 15, 2015.
	C. "TOPOGRAPHIC SURVEY TAX ID 03-0004-0009 TAX ID 03-0004-0009B 243 & 253 TALCOTTVILLE ROAD VERNON, CONNECTICUT" PREPARED BY VHB. DATE: OCTOBER 26, 2017, REVISED 1/8/2018.
	D. "RESUBDIVISION OF LOT 3 TO BE KNOWN AS SONA INDUSTRIAL PARK VERNON, CONNECTICUT" BY GARDNER & PETERSON ASSOCIATES. DATE: $12-27-85$ , REVISED $1-27-86$ .
	E. "RESUBDIVISION – LOT #3 SONA INDUSTRIAL PARK LAND OF NAEK CONSTRUCTION CO. INC. VERNON, CONNECTICUT" BY GARDNER & PETERSON ASSOCIATES. DATE: $9-21-90$ , REVISED 5/9/91.
	F. "AS-BUILT PLAN & SEWAGE PUMPING STATION NAEK ROAD SONA INDUSTRIAL PARK VERNON, CONNECTICUT" BY GARDNER & PETERSON ASSOCIATES. DATE: 9–28–87, REVISED 12–6–88.
4.	THESE PARCELS ARE LOCATED IN THE PLANNED DEVELOPMENT ZONE (PDZ): GERBER FARM AREA.
5.	291 TALCOTTVILLE ROAD IS IN FAVOR OF AN EASEMENT OVER A PORTION OF 243 & 253 TALCOTTVILLE ROAD FOR THE RIGHT TO PASS AND REPASS BY FOOT OR BY VEHICLE AS DESCRIBED IN VOL. 2540, PAGE 129 IN THE VERNON LAND RECORDS.
6.	TOPOGRAPHY DEPICTED ON THESE PLANS WAS PROVIDED BY GOLDEN AERIAL SURVEYS.
7.	WETLANDS DEPICTED ON THESE PARCELS WERE DELINEATED BY REMA ECOLOGICAL SERVICES, LLC.
8.	THESE PARCELS ARE NOT LOCATED WITHIN THE LEVEL A AQUIFER PROTECTION AREA AS DEPICTED ON THE ZONING MAP VERNON, CT DATED 7/31/2020.
9.	291 & 293 TALCOTTVILLE ROAD, AND 27, 32, 37, 38 & 46 NAEK ROAD SHALL BE COMBINED INTO ONE PARCEL PRIOR TO ISSUANCE OF ANY CERTIFICATES OF OCCUPANCY. THE TOTAL AREA OF THE COMBINED PARCELS IS 941,200 $\pm$ sq. ft. 21.6 $\pm$ acres.
10	D. UNDERGROUND UTILITY, STRUCTURE AND FACILITY LOCATIONS DEPICTED HEREON HAVE BEEN COMPILED, IN PART, FROM RECORD MAPPING, OR OTHER SOURCES. THESE LOCATIONS MUST BE CONSIDERED APPROXIMATE IN NATURE. ADDITIONALLY, OTHER SUCH FEATURES MAY EXIST ON THE SITE, THE EXISTENCE OF WHICH ARE UNKNOWN TO GARDNER & PETERSON ASSOCIATES, LLC. THE EXISTENCE, SIZE AND LOCATION OF ALL SUCH FEATURES MUST BE DETERMINED AND VERIFIED IN THE FIELD BY THE APPROPRIATE AUTHORITIES PRIOR TO CONSTRUCTION. CALL BEFORE YOU DIG 1–800–922–4455.
	HEREBY DECLARE THAT, TO THE BEST OF MY KNOWLEDGE AND BELIEF, THIS MAP SUBSTANTIALLY CORRECT AS NOTED HEREON.
_	Vic R. Poters L.S. 23430
	ERIC R. PETERSON REGISTRATION NO.
IN C(	HE WETLAND SOILS ON THIS PROPERTY WERE IDENTIFIED I THE FIELD USING THE CRITERIA REQUIRED BY ONNECTICUT P.A. 72–155 AS AMENDED BY P.A. 73–571 ND ARE ACCURATELY REPRESENTED ON THIS PLAN.

Norge / Jogar GEORGE T. LOGAN, MS, PWS Registered Soil Scientist

LEGEND PROPOSED **EXISTING** PROPERTY BOUNDARY ZONING SETBACK _____ EASEMENT ____. . . ___. . . ___. . . ___. IRON PIN/PIPE FOUND 0 MONUMENT FOUND Ō — — —s—_s—_s— SANITARY SEWER —(S)— = = = = = = Catch Basin/Culvert STORM MANHOLE D FOOTING DRAIN ____F_____ — — <del>*°° — W —</del> — — <del>W –</del> WATER MAIN _____<del>W</del>_____ Ъ. HYDRANT GAS MAIN _____G_____ _____ LIGHT * ¥ UTILITY POLE ပ် OVERHEAD WIRES —онw— SIGN <del>___</del> GRAPHIC SCALE 1"= 40' IMDDOUEMENTT I OCATION SUDVEV

	IMPROVEMENT LOCATION SURVEY				
STATE CONNO-		UT	ILITY PL	AN	
A PETER	THE VILLAGE AT NAEK ROAD				
*	291 & 293 TALCOTTVILLE ROAD				
No. 23430	4	27, 32, 37, 3	88 & 46 NA	EK ROAI	
SONAL ENGINEERING		VERNON	I, CONNE	ECTICUT	
annum	GARD	NER & PE	TERSON A	SSOCIATES	, LLC
REVISIONS	178 HARTFORD TURNPIKE TOLLAND, CONNECTICUT				
	PROFESSIONAL ENGINEERS LAND SURVEYORS				
	BY	SCALE	DATE	SHEET NO.	MAP NO.
	E.R.P.	1"=40'	03-17-2021	6 OF 10	5768B





. KEY STONE INTO THE DITCH BANKS AND EXTEND INTO THE ABUTMENTS A MINIMUM OF 18" TO PREVENT FLOW FROM FLANKING THE CHECK DAM.

Mai<u>ntenance</u> Maintenance Item Frequency erground Stormwater Chambe Visual Inspection Semi- Annually Remove inspection port caps to verify that runoff has infiltrated & leaves/debris are not collecting in system. Check sediment depth and vacuum when 6' of sediment has accumulated. Catch Basins Monthly Inspect grates for litter and debris and remove as needed Annually Remove sediment in sumps immediately after spring snowmelt Grass Swale Monthly Maintain grass at a height of 4 to 6 inches during the growing season Semi-Annuall Remove debris/sediment in swale Check for evidence of water overflowing Semi-Annually 6. TEST PIT DATA: WITNESSED BY E. PETERSON, P.E. GARDNER & PETERSON ASSOCIATES, LLC 7. 06/02/2020 TP 303: 0-9" TOPSOIL 8. 9-14" COARSE LOAMY SAND 14-108" COARSE SAND W/ COBBLES 9. 0-13" TOPSOIL 10. 13-22" Y.BR. FINE SANDY LOAM 22-72" R.BR. TILL, COMPACT MOTTLING @ 16" 11. SEEPAGE @ 68" TP 307: 0-18" TOPSOIL/FILL 18-30" Y.BR. FINE SANDY LOAM 12. 30–72" R.BR. TILL MOTTLING @ 18" SEEPAGE @ 40" TP 308 0-38" SAND & GRAVEL FILL 38-44" BURIED TOPSOIL 44-138" SAND & GRAVEL SHGW @ 108" PERM @ 58" RATE: 190 FT/DAY TP 310: 0-11" TOPSOIL 11-28" BR. FINE SANDY LOAM 28-84" FIRM R.BR. SILT 84-144" MED. SAND W/ COBBLES, SOME SILT GW @ 126" PERM #1 @ 115' RATE: 70 FT/DAY STANDPIPE SET: DRY ON 06/16/2020 TP 311: 0-11" TOPSOIL 11-102" BR. SAND & GRAVEL 192-144" COMPACT FINE SAND W/ SILT PERM #2 @ 50" RATE: 61 FT/DAY TP 312: 0-16" TOPSOIL 16-32" FINE SANDY LOAM 32-144" SAND & GRAVEL PERM #3 @ 36" RATE: 41 FT/DAY TP 313 TOPSOIL 0-7" 7-15" Y.BR. FINE SANDY LOAM 15-43" R.BR LOAMY SAND W/ COBBLES, SOMEWHAT FIRM LEDGE @ 43" TP 314: LEDGE 🕲 24" TP 314A: 0-36" FRACTURED ROCK TP 315: LEDGE @ 36" (WEST) LEDGE @ 30" (EAST) TP 316 TOPSOIL 0-4" 4-33" BR. FINE SANDY LOAM W/ COBBLES 33-54" BR. COMPACT TILL W/ FLAT BOULDERS 54-78" SAND & GRAVEL W/ BOULDERS LEDGE @ 78" PERM #12 @ 23" RATE: 0.4 FT/DAY TP 317: 0-10" TOPSOIL 10-58" BONEY BR. FINE SANDY LOAM LEDGE @ 58" TP 317A: 0-8" TOPSOIL 8-30" BR. FINE SANDY LOAM W/ COBBLES 30-78" R.BR. COMPACT TILL W/ FLAT BOULDERS LEDGE @ 78" TP 318: 0-8" TOPSOIL 8-36" Y.BR. FINE SANDY LOAM W/ COBBLES, FIRM 36-60" R.BR. TILL W/ COBBLES 60-80" DECOMPOSED LEDGE TP 319: 0-9" TOPSOIL 9-24" Y.BR. LOAMY SAND W/ COBBLES 24-60" SAND & GRAVEL 60-132" COARSE SAND PERM #70 @ 36" RATE: 370 FT/DAY TP 320: LEDGE @ 32" TP 321: 0-12" TOPSOIL 12-20" Y.BR. FINE SANDY LOAM 20-116" SAND & GRAVEL SEEPAGE 🞯 116" 08/16/2020 TP H1: TOPSOIL 0-6" 6-28" Y.BR. FINE SANDY LOAM 28-36" MED. SAND W/ COBBLES PERM #1 @ 32" RATE: 12 FT/DAY SOLID TOP (16) 3/8" DIA. HOLES ALL AROUND PIPE EVERY 8" IN HEIGHT - STONE TO BOTTOM OF BELL 18" MIN. TOP ELEVATION TO EQUAL TOP BERM WRAP SIDES OF RISER PIPE DUPONT TYPAR 3341

Maintenance Schedule

ALL EROSION AND SEDIMENT CONTROL
IN ACCORDANCE WITH THE STANDARDS
FOR SOIL EROSION AND SEDIMENT CO
SOIL AND WATER CONSERVATION.
ALL SEDIMENT CONTROL PRACTICES AND

ICES AND MEASURES SHALL BE CONSTRUCTED, APPLIED AND MAINTAINED IN ACCORDANCE WITH THE APPROVED SEDIMENT CONTROL PLAN.

TOPSOIL REQUIRED FOR THE ESTABLISHMENT OF VEGETATION SHALL BE STOCKPILED IN THE AMOUNT NECESSARY TO COMPLETE THE FINISHED GRADING OF ALL EXPOSED 

AREAS TO BE FILLED SHALL BE CLEARED, GRUBBED AND STRIPPED OF TOPSOIL TO REMOVE TREES, VEGETATION, ROOTS OR OTHER OBJECTIONABLE MATERIAL. ALL FILLS SHALL BE COMPACTED AS REQUIRED TO MINIMIZE EROSION, SLIPPAGE, AND SETTLEMENT. FILL INTENDED TO SUPPORT STRUCTURES, DRAINAGE, ETC. SHALL BE COMPACTED IN ACCORDANCE WITH THE APPROPRIATE STATE AND/OR

LOCAL SPECIFICATIONS FILL MATERIAL SHALL BE FREE OF BRUSH, RUBBISH, LARGE ROCKS, LOGS, STUMPS, BUILDING MATERIAL, COMPRESSIBLE MATERIAL, AND OTHER MATERIALS WHICH MAY INTERFERE WITH OR PREVENT CONSTRUCTION OF SATISFACTORY FILLS. FROZEN MATERIAL OR SOFT MUCKY OR HIGHLY COMPRESSIBLE MATERIALS SHALL

NOT BE INCORPORATED INTO FILLS.

FILL SHALL NOT BE PLACED ON A FROZEN FOUNDATION. ALL BENCHES SHALL BE KEPT FREE OF SEDIMENT DURING ALL PHASES OF DEVELOPMEN[®]

SEEPS OR SPRINGS ENCOUNTERED DURING CONSTRUCTION SHALL BE HANDLED IN ACCORDANCE WITH SOUND CONSTRUCTION PRACTICE.

ALL GRADED AREAS SHALL BE PERMANENTLY STABILIZED IMMEDIATELY FOLLOWING FINISH GRADING. IF FINISH GRADING IS TO BE DELAYED FOR MORE THAN 30 DAYS AFTER DISTURBANCE IS COMPLETE, TEMPORARY SOIL STABILIZATION MEASURES SHALL BE APPLIED. AREAS LEFT OVER 30 DAYS SHALL BE CONSIDERED "LONG TERM" AND SHALL RECEIVE TEMPORARY SEEDING WITHIN THE FIRST 15 DAYS

PREPARATION, SEEDING, MULCHING, AND MAINTENANCE UNLESS OTHERWISE SPECIFIED IN THE PLANS

CUT AND FILL SLOPES SHALL NOT BE STEEPER THAN 2:1. TOPSOIL SHALL BE SPREAD TO A MINIMUM DEPTH OF 4". ADDITIONAL TOPSOIL MAY BE REQUIRED TO MEET MINIMUM 13. DEPTHS. NO TOPSOIL SHALL BE REMOVED FROM THIS SITE.

APPLY SEED UNIFORMLY BY HAND, CYCLONE SEEDER, DRILL CULTIPACKER TYPE SEEDER, OR HYDROSEEDER (SLURRY INCLUDING SEED AND FERTILIZER). NORMAL SEEDING DEPTH IS FROM 1/4" TO 1/2" INCH. HYDROSEEDING WHICH IS MULCHED MAY BE LEFT ON THE 14. SOIL SURFÁCE.

WHERE FEASIBLE, EXCEPT WHERE EITHER A CULTIPACKER TYPE SEEDER OR HYDROSEEDER 15. IS USED, THE SEEDBED SHOULD BE FIRMED FOLLOWING SEEDING WITH A ROLLER OR LIGHT DRAG.

16. CONTOUR

REMOVE FROM THE SURFACE ALL STONES TWO INCHES OR LARGER. REMOVE ALL OTHER 17. DEBRIS SUCH AS WIRE, TREE ROOTS, PIECES OF CONCRETE, OR OTHER UNSUITABLE

18.

WHERE GRASSES PREDOMINATE, FERTILIZE ACCORDING TO SOIL ANALYSIS, OR SPREAD 19. 300 POUNDS OF 10-10-10 OR EQUIVALENT PER ACRE (7.5 POUNDS PER 1000 S.F.). 20. CALCIUM CHLORIDE WILL BE AVAILABLE FOR DUST CONTROL ON GRAVEL TRAVEL SURFACES.

TEMPORARY SEEDING SCHEDULE: SPECIES LBS/ACRE ANNUAL RYEGRASS WINTER RYE

TEMPORARY SEEDING IS NOT LIMITED TO THE SPECIES SHOWN. OTHER SPECIES RECOMMENDED BY THE SCS OR AS LIMITED BY SITE CONDITIONS MAY BE USED. STRAW MULCH IS TO BE APPLIED TO SEEDED AREA AT THE RATE OF 1-1/2 to 2 tons per ACRE, 70 TO 90 LBS. PER 1000 SQ. FT.

FINAL SEEDING SCHEDULE:

SUDANGRASS

PROVIDE 4 INCHES OF TOPSOIL MINIMUM, FREE OF ROOTS, LARGE STONES, AND OTHER OBJECTS. SPECIES LBS/ACRE SEEDING DATES

KENTUCKY BLUEGRASS CREEPING RED FESCUE PERENNIAL RYEGRASS

TURF MANAGEMENT PLAN

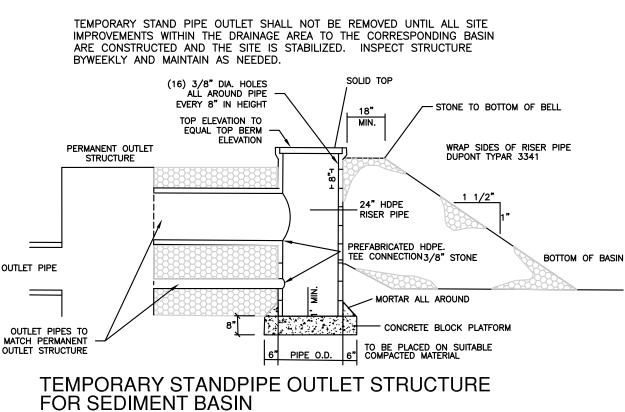
<u>Soil Testing</u> A composite soil sample from the subject property will be collected and delivered to a University of Connecticut Cooperative Extension office for testing of soil nutrient levels (i.e., pH, nitrogen, phosphorus, calcium, magnesium, potassium) prior to a fertilizer application. The Extension office will recommend a fertilizer application rate based upon these test results. The actual fertilizer application rate will follow this recommendation. This will ensure against an excessive fertilizer application, which could lead to chemical leaching or export.

2. <u>Slow-Release Fertilizers</u> Slow—release fertilizers will be applied to lawns, planted trees and shrubs. These can include, but are not limited to, organic-based fertilizers. A variety of commercial slow-release nitrogen fertilizer products are available (e.g., Milorganite, isobutylidene diurea, coated ureas, etc.). Advantages of slow-release fertilizers include the supply of a steady nitrogen source, and reduced nitrogen leaching. By combining small amounts of soluble nitrogen sources with slow release nitrogen products, nitrogen availability can be extended without a threat of leaching.

3. <u>Fertilizer Application Schedule</u> Fertilizer will be applied three times annually to the subject property: early to late May (after the threat of cool, wet weather has passed), late August to early September, and mid-September to mid-October. If the soil test indicates a need for lime, it will be applied at the last fertilization date.

<u>Integrated Pest Management (IPM)</u> IPM is an integrated, preventative approach to maintaining healthy turf and landscape plants. IPM recognizes that, although chemicals are an important component of a turf management plan, other strategies are available to maintain a healthy lawn. A central premise of IPM is to treat pest problems as they arise on an as-needed basis only, using a variety of biological (e.g., natural predators), chemical and cultural (e.g., disease-resistant seed) practices.

To be successful, IPM requires periodic monitoring by an experienced practitioner to detect pest problems at an early stage and develop an effective, environmentally responsible action plan. It is recommended that the contractor that is hired to maintain the grounds have training and experience in the practice of IPM.



#### MEASURES SHALL BE CONSTRUCTED AND SPECIFICATIONS OF THE "GUIDELINES ONTROL" BY THE CONNECTICUT COUNCIL ON

SITE IS TO BE GRADED TO PERMIT THE USE OF CONVENTIONAL EQUIPMENT FOR SEEDBED

### FERTILIZER AND LIME ARE TO BE WORKED INTO THE SOIL AS NEARLY AS PRACTICAL TO A DEPTH OF 4 INCHES WITH A DISC, SPRING TOOTH HARROW OR OTHER SUITABLE EQUIPMENT. THE FINAL HARROWING OR DISC OPERATION SHOULD BE ALONG THE

#### INSPECT SEEDBED BEFORE SEEDING. IF TRAFFIC HAS LEFT THE SOIL COMPACTED, THE AREA MUST BE RETILLED BEFORE SEEDING, THEN FIRMED AS DESCRIBED ABOVE.

LBS/1000SF 1.0 0.7

SEEDING DATES 3/1-6/15, 8/1-10/15 4/15-7/1, 8/15-10/15 5/15-8/1

LBS/1000SF 0.45

0.45

4/1-6/15, 8/15-10/⁻ 4/1-6/15, 8/15-10/1 4/1-6/15, 8/15-10/1

PROJECT NAME: THE VILLAGE A NAEK ROAD						
LOCATION: NAEK ROAD – VERNON, CT						
PROJECT DESCRIPTION: MULTI-FAMILY HOUSING DEVELOPMENT						
PARCEL AREA: 21.6 AC.	PARCEL AREA: 21.6 AC.					
RESPONSIBLE PERSONNEL: R.HAMID, NAEK CONSTRUCTION, 27 NAEK ROAD, VERNON, CT 860-875-1895						
WORK DESCRIPTION	EROSION & SEDIMENT CONTROL MEASURES	DATE INSTALLED	INITIALS			
CLEAR TREES AND BRUSH	INSTALL ANTI-TRACKING PAD					
REMOVE STUMPS	INSTALL SILT FENCE BARRIERS DOWNGRADE OF CONSTRUCTION ACTIVITY AS SHOWN					
	INSTALL INLET PROTECTION IN EXISTING CATCH BASINS					
EXCAVATE SEDIMENT BASINS AND ROUGH GRADE SITE	PROTECT INFILTRATION GALLEY AREAS FROM DISTURBANCE AND COMPACTION					
	PROTECT STOCKPILE AREAS WITH SILT FENCE					
	INSTALL EROSION BLANKET ON SLOPES STEEPER THAN 3:1					
I	INSPECT AND MAINTAIN SEDIMENT BARRIERS WEEKLY AND AFTER RAIN EVENTS OVER 0.5-INCH.					
EXCAVATE FOR BUILDING FOUNDATIONS						
INSTALL SEWER, DRAINAGE AND UTILITIES	INSTALL HAYBALES AROUND NEW CATCH BASIN INLETS ONCE INSTALLED					
INSTALL PAVEMENT BINDER COAT IN AREAS WHERE FOUNDATIONS AND UTILITIES ARE COMPLETE	TOPSOIL, SEED AND MULCH AREA ADJACENT TO EACH BUILDING AS IT IS COMPLETED					
FINAL GRADE AND FINAL PAVE	TOPSOIL, SEED AND MULCH REMAINDER OF SITE					
	REMOVE SEDIMENT FROM DRAINAGE STRUCTURES AND INSTALL INFILTRATION TRENCHES WITHIN					

CONSTRUCTION SCHEDULE &

EROSION & SEDIMENT CONTROL CHECKLIST

PROJECT DATES: DATE OF CONSTRUCTION START JULY 1, 2021 DATE OF CONSTRUCTION COMPLETION NOVEMBER 30, 2022

EROSION AND SEDIMENT CONTROL PROCEDURES SHALL ESSENTIALLY BE IN ACCORDANCE WITH THESE PLANS, AS REQUIRED BY TOWN REGULATIONS, AND THE MANUAL, "GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL" FOR CONNECTICUT, BY THE COUNCIL ON SOIL AND WATER CONSERVATION, 1985, REVISED TO 2002.

SITE IS STABILIZED

REMOVE EROSION CONTROLS WHEN

### PROJECT NARRATIVE

The purpose of this project is to construct nineteen new apartment buildings and the driveways, parking and utilities to service them. The proposed buildings are to be serviced by public sanitary sewer and water, and the new buildings will be accessed by two new curb cuts off Mount Vernon Drive.

Initial construction will commence at the northerly portion of the site and conclude at the southerly portion of the site. The schedule of construction activities from the northerly, to the middle, to the southerly portion of the site shall generally follow the same sequence. Construction activities shall commence with the installation of the construction entrance and sedimentation barriers, followed by tree cutting and stumping. The rain garden area and infiltration galley areas shall be protected from construction activities and compaction prior to rough grading. Rough grading shall commence with the excavation of the sediment trap and/or sediment basin as depicted. Installation of the drainage structures, and piping shall proceed as the construction schedule allows. Leave grade 6" below catch basin tops to prevent silt laden runoff from entering the drainage system

During rough grading, haybales or silt fence shall be installed as shown at the toe of cut and fill slopes. Installation of drainage structures and piping may proceed as the construction schedule allows.

Completion of storm drainage and utility installation is to be followed by placing processed gravel, and final grading of the paved areas. All erosion control measures shall be maintained and upgraded as needed until stable vegetative growth has been established. At all times erosion of exposed and stockpiled materials shall be prevented using measures specified in these plans. Once the site is stabilized, sediment within the basin will be removed and the sediment will be seeded as depicted on these plans.

Proposed soil erosion and sediment control measures were designed using criteria set forth by the "Connecticut Guidelines for Soil Erosion and Sediment Control", revised to

## PROJECT NARRATIVE

The purpose of this project is to construct 18 new multi-family buildings and the driveway, parking and utilities to service the buildings. The proposed buildings are to be serviced by public water and sanitary sewer. A house currently exists on the property which will be removed and the existing curb cut along Talcottville Road will be closed. Access to the site will be from new curb cuts off of Naek Road.

Construction activities shall commence with the installation of the construction entrances followed by tree cutting. Sedimentation barriers shall be installed prior to stumping. The infiltration galley areas shall be protected from construction activities and compaction prior to rough grading. Inspect condition of sedimentation barriers prior to rough grading

Rough grading shall commence with the excavation of the sediment basins as depicted. Installation of the drainage structures, and piping shall proceed as the construction schedule allows. Leave grade 6" below catch basin tops to prevent silt laden runoff from entering the drainage system. The middle of each building shall be rough graded to shed runoff back towards the center of the site drives.

Completion of storm drainage and utility installation is to be followed by placing processed gravel, and final grading of the paved areas. The first coat of all paved site drives shall be installed once all foundations have been poured. The installatoin of the infiltration trenches wintin the stormwater basins shall be completed once the site is paved and a vegetative growth on disturbed areas has been established. All erosion control measures shall be maintained and upgraded as needed until stable vegetative growth has been established. At all times erosion of exposed and stockpiled materials shall be prevented using measures specified in these plans. Once the site is stabilized, sediment within the basin will be removed and the sediment will be seeded as depicted on these plans. Proposed soil erosion and sediment control measures were designed using criteria set forth by the "Connecticut Guidelines for Soil Erosion and Sediment Control", revised to

**EROSION & SEDIMENT CONTROL DETAILS** SITE PLAN OF DEVELOPMENT

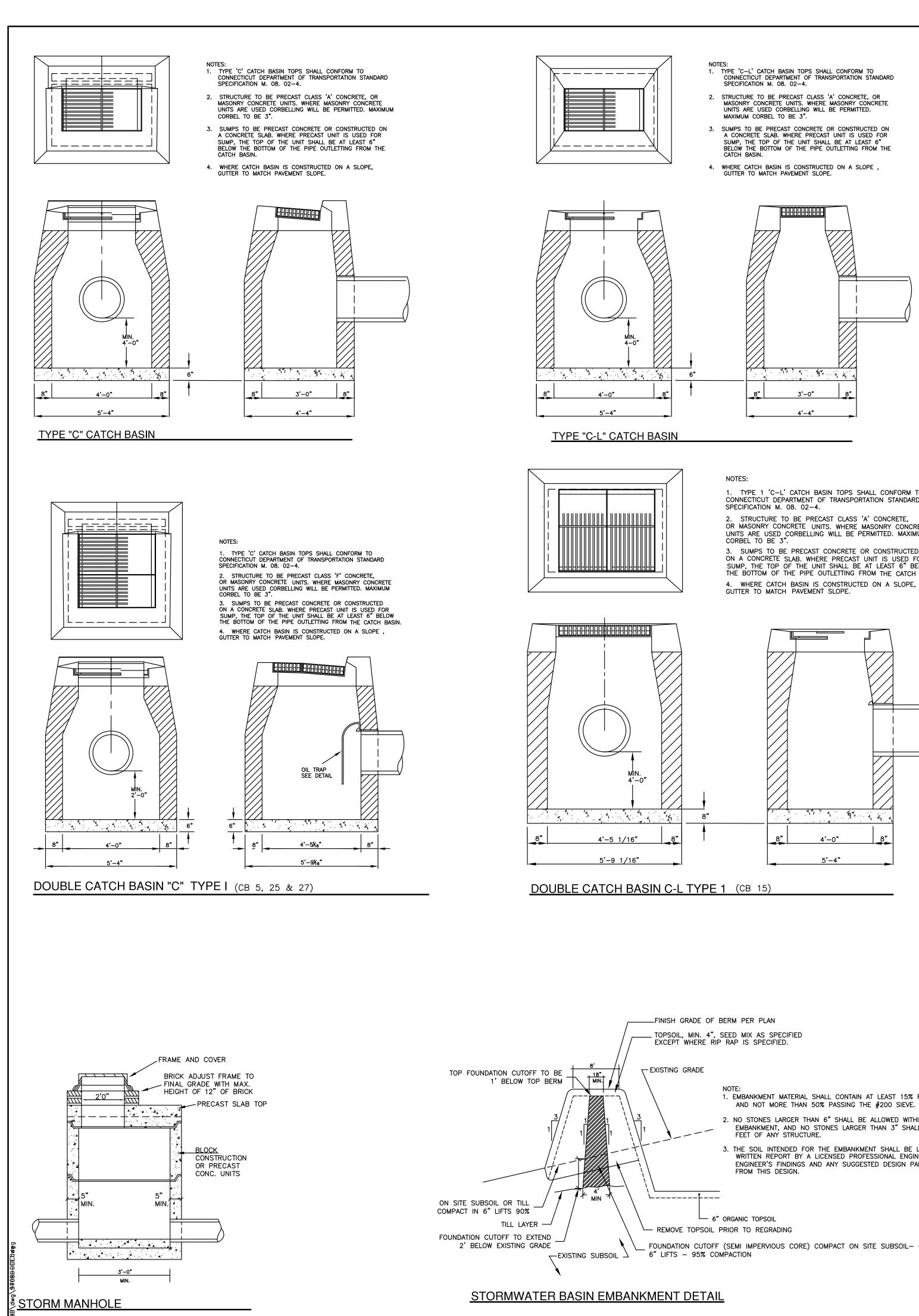
## THE VILLAGE AT NAEK ROAD 291 & 293 TALCOTTVILLE ROAD 27, 32, 37, 38 & 46 NAEK ROAD

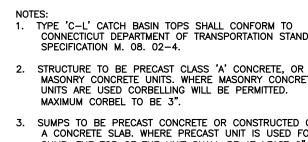
#### VERNON, CONNECTICUT GARDNER & PETERSON ASSOCIATES, LLC 178 HARTFORD TURNPIKE TOLLAND, CONNECTICUT PROFESSIONAL ENGINEERS LAND SURVEYORS SCALE DATE SHEET NO. MAP NO. 03-17-2021 5768B E.R.P. N.T.S. 8 OF 10

No. 23430

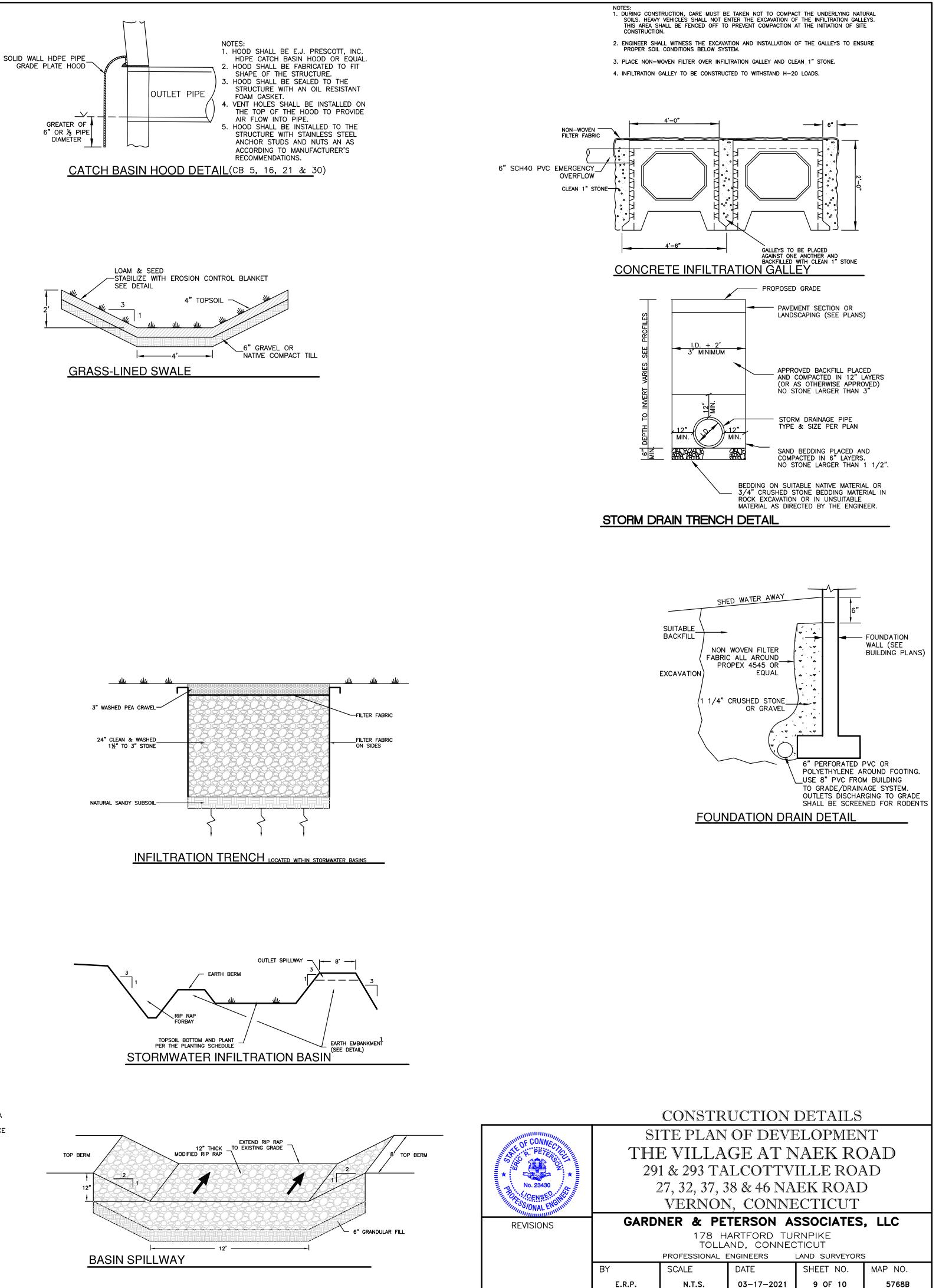
2002

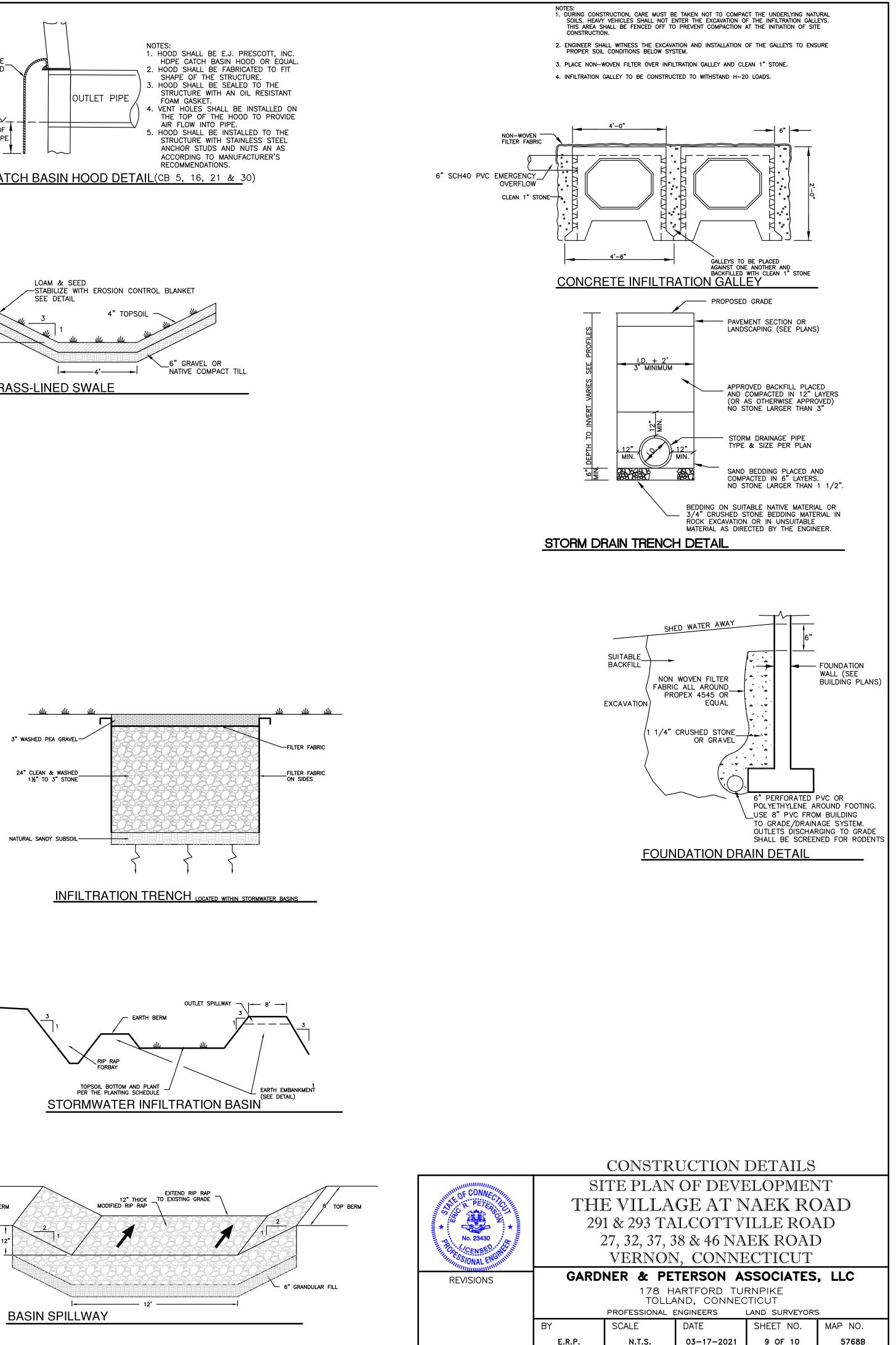
REVISIONS

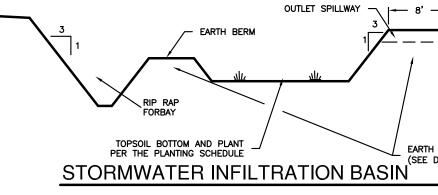


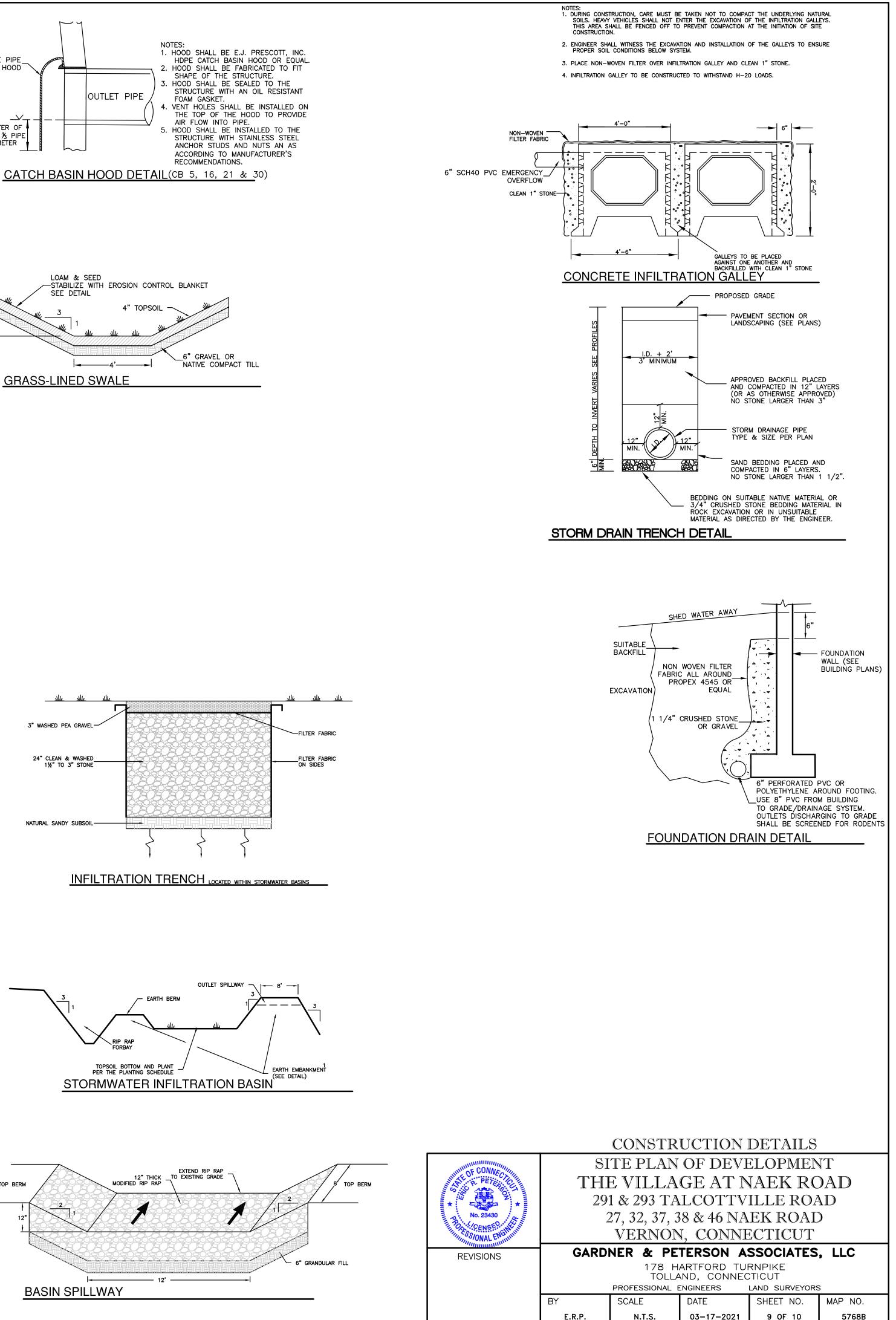


1. TYPE 1 'C-L' CATCH BASIN TOPS SHALL CONFORM TO CONNECTICUT DEPARTMENT OF TRANSPORTATION STANDARD OR MASONRY CONCRETE UNITS. WHERE MASONRY CONCRETE UNITS ARE USED CORBELLING WILL BE PERMITTED. MAXIMUM 5. SUMPS TO BE PRECAST CONCRETE OR CONSTRUCTED ON A CONCRETE SLAB. WHERE PRECAST UNIT IS USED FOR SUMP, THE TOP OF THE UNIT SHALL BE AT LEAST 6" BELOW THE BOTTOM OF THE PIPE OUTLETTING FROM THE CATCH BASIN.



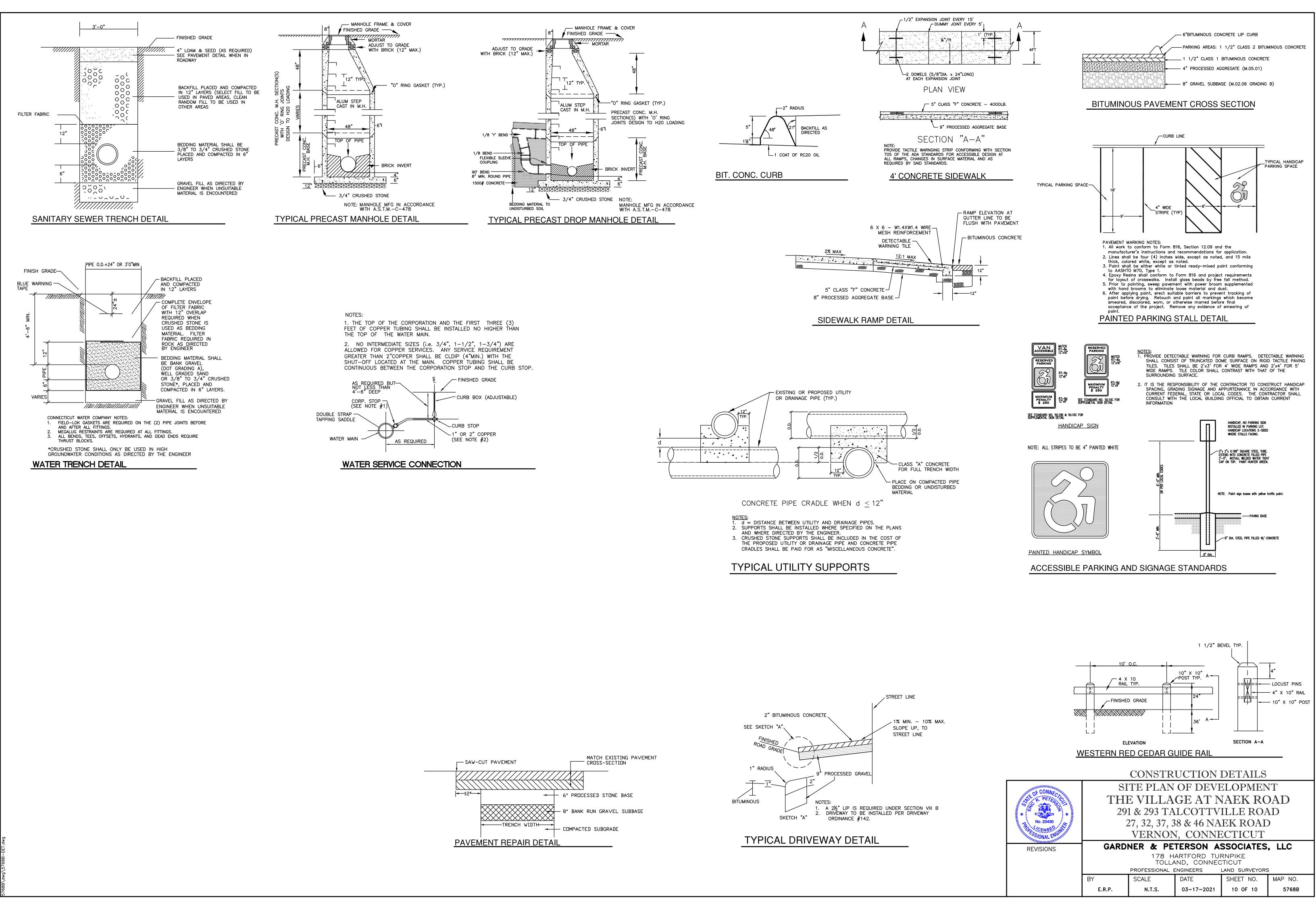


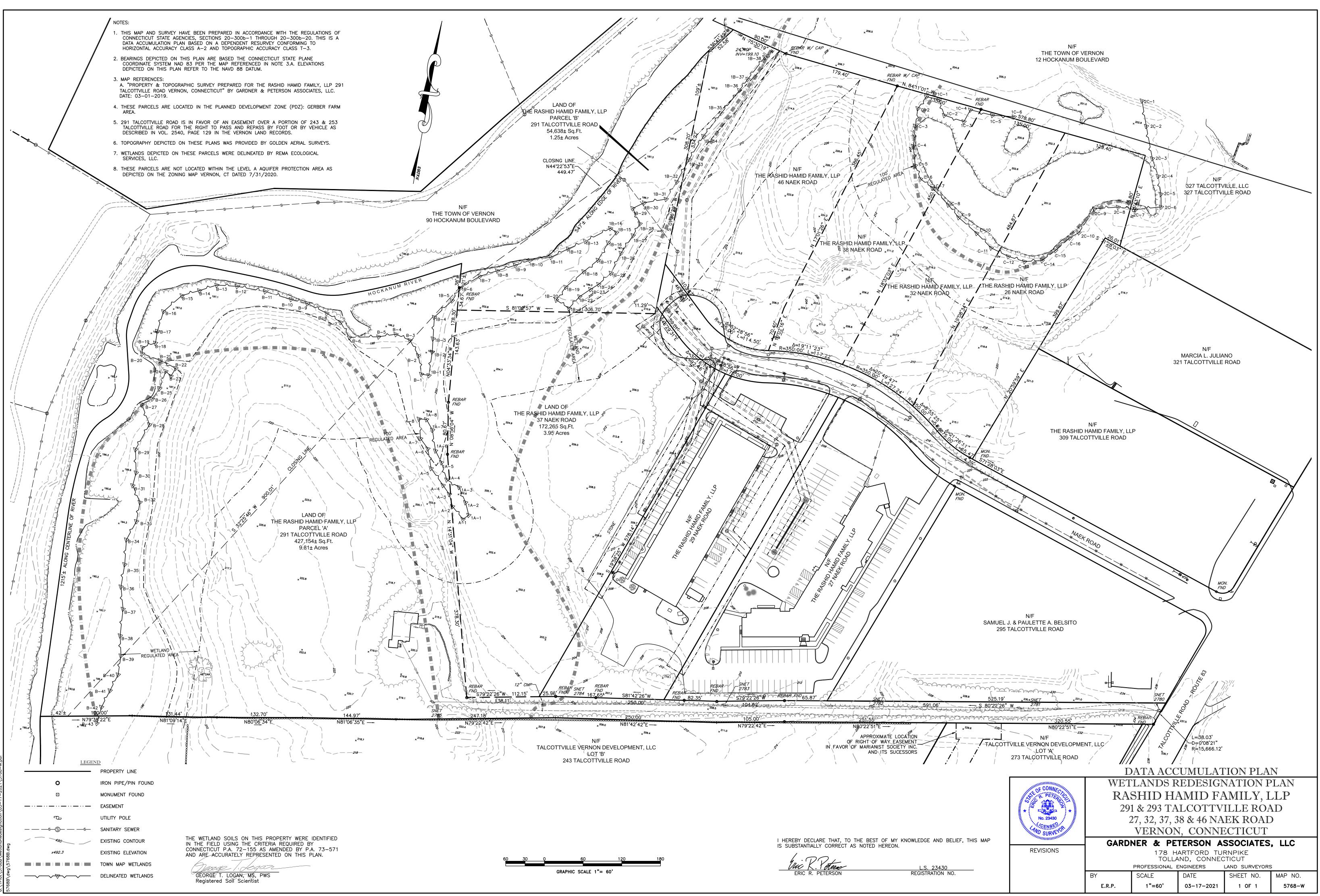




1. EMBANKMENT MATERIAL SHALL CONTAIN AT LEAST 15% PASSING THE #200 SIEVE 2. NO STONES LARGER THAN 6" SHALL BE ALLOWED WITHIN THE COMPACTED EMBANKMENT, AND NO STONES LARGER THAN 3" SHALL BE ALLOWED WITHIN TWO 3. THE SOIL INTENDED FOR THE EMBANKMENT SHALL BE LABORATORY TESTED WITH A WRITTEN REPORT BY A LICENSED PROFESSIONAL ENGINEER PROVIDING THE ENGINEER'S FINDINGS AND ANY SUGGESTED DESIGN PARAMETERS IF AT A VARIANCE

FOUNDATION CUTOFF (SEMI IMPERVIOUS CORE) COMPACT ON SITE SUBSOIL- GLACIAL TILL







**REMA ECOLOGICAL SERVICES, LLC** 

164 East Center Street, Suite 8 Manchester, CT 06040 860.649.REMA (7362)

ON-SITE SOIL INVESTIGATION & WETLAND DELINEATION REPORT

PROJECT NAME & SITE LOCATION:	<b>REMA Job No.:</b> <u>18-2112-VER47</u>
<u>(+/- 21.05 acres) (6 parcels)</u>	Field Investigation Date(s): <u>9/17, 11/27 § 11/28/18</u>
291 Talcotville Road & Naek Road	Field Investigation Method(s):
Vernon, CT	Spade and Auger
	Backhoe Test Pits Other:
<b>Report Prepared For:</b>	Field Conditions:
Naek Construction Company, Inc.	Weather: <u>Partly sunny, lower 80s to 40s</u>
27 Naek Road	Soil Moisture: <u>moderate to high</u>
Vernon, CT 06066	Snow Depth: N/A
<u>Attn.: Sebastían Testa, SPM</u>	Frost Depth: N/A
Purpose of Investigation:	
Wetland Delineation/Flagging in 1	Field
Wetland Mapping on Sketch Plan	
High Intensity Soil Mapping by S	oil Scientist
Medium Intensity Soil Mapping fr	rom The Soil Survey of Connecticut Maps (USDA-NRCS)
Other:	
Base Map Source: CT Soil Survey web; USI	DA-NRCS) (attached); Fígures A & A1 (attached)

Wetland Boundary Marker Series: <u>RES-A-1 to RES-A-8 tied to RES-1A-1 to RES-1A-8 (closed loop), and</u> <u>RES B-1 to RES B-40 tied to RES-1B-1 to RES-1B-38 (open line), RES- C-1 to RES-C-16 tied to RES-1C-1 to</u> <u>RES-1C-6, tied to RES-2C-1 to RES-2C-10</u>

General Site Description/Comments: The "study area", or "site", is +/-21.05 acres of land (6 contiguous parcels) located west of Talcottville Road and southwest and north of Naek Road, in Vernon, CT. Much of the western study area boundary is defined by the Hockanum River, which flows southwesterly and then southerly past the study area. The majority of the site is forested and with a single-family residence in its southwestern section, and some equipment storage in its eastern section. The site's soils are primarily derived from glaciofluvial deposits (i.e. stratified sand and gravel), and from alluvial deposits (i.e. stratified sand and silt). The "C-series" wetland has organics derived soils (i.e. peat/muck). The upland-type soils are the excessively drained Manchester (37) soil series. and the Niniaret and Tisbury (21) soil series complex. The wetland-type soils are the very poorly drained Timakwa and Natchaug mucks (17), the poorly drained Raypol (12) soil series, and the poorly drained Fluvaquents (109) soil mapping unit. The regulated wetland resources include the riparian forest associated with the Hockanum River, a small seasonally flooded forested swamp that overflows northerly to the Hockanum River corridor, and a semipermanently flooded scrub shrub swamp, which is likely a vernal pool habitat. Dominant vegetation observed within the regulated wetlands included red maple. American elm, green ash, ironwood, spicebush, highbush blueberry, winterberry, multiflora rose, silky dogwood, firebush, buttonbush, Japanese barberry, sensitive, royal, cinnamon, and Massachusetts ferns, woodferns, jewelweed, jack in the pulpit, false nettle, Virginia jumpseed, clearweed, swamp dewberry, stout woodreed grass, white avens, tussock sedge, duckweed, and many others.

PAGE <u>2</u> OF <u>3</u>

### ON-SITE SOIL INVESTIGATION & WETLAND DELINEATION REPORT (CONTINUED)

PROJECT NAME & SITE LOCATION: (+/- 21.05 acres) (6 parcels) 291 Talcotville and Naek Roads, Vernon, CT

### Upland Soils

## SOIL MAP UNITS

- Manchester gravely sandy loam (37). This series consists of very deep, excessively drained soils formed in a shallow, loamy sand mantle underlain by gravelly sand, water deposited glacial outwash materials. They are level to very steep soils on outwash plains, terraces, deltas, kames and eskers. The soils formed in loamy over stratified sandy and gravelly glacial outwash derived mainly from Triassic sandstone, shale, conglomerate and basalt. Typically these soils have a reddish brown gravelly sandy loam surface layer 6 inches thick. The subsoil layer from 6 to 16 inches is yellowish red gravelly sandy loam. The substratum from 16 to 60 inches is yellowish brown stratified solutions.
- Nínígret fine sandy loam (21). This series consists of very deep moderately well drained soils formed in a coarse-loamy mantle underlain by sandy water deposited glacial outwash materials. They are nearly level to gently sloping soils on glaciofluvial landforms, typically in slight depressions and broad drainage ways. The soils formed in loamy over stratified sandy and gravelly outwash derived from a variety of acid rocks. Typically, these soils have a very dark grayish brown fine sandy loam surface layer 8 inches thick. The subsoil from 8 to 26 inches is yellowish brown fine sandy loam with mottles below 16 inches. The substratum from 26 to 60 inches is mottled, pale brown, loose, stratified loamy sand.
- **Tísbury sílt loam (21).** This series consists of deep, moderately well drained soils formed in a coarse-silty mantle underlain by sandy water deposited glacial outwash materials. They are level to gently sloping soils in broad drainage swales and low lying positions on outwash plains and terraces. The soils formed in loamy over stratified sandy and gravelly glacial outwash derived mainly from a acid crystalline rocks (granite, gneiss and schist). Typically these soils have a very dark grayish brown silt loam surface layer 8 inches thick. The subsoil from 8 to 26 inches is yellowish brown and brownish yellow silt loam, with mottles common below 16 inches. The substratum from 26 to 60 inches is grayish brown, mottled stratified sand and gravel.

### Wetland Soils

- Fluvaquents (109). This soil map unit consists of relatively recently formed, moderately well drained and well drained, floodplain soils. Fluvaquents are typically found in disturbed landscapes on floodplains where two or more feet of the original soil surface has been filled over or excavated. Most areas of Fluvaquents flood each year for short periods, mainly in the spring. The Fluvaquents soil mapping unit is a miscellaneous unit which includes a large variety of soil materials. Common locations of Fluvaquents include disturbed areas for community development and sand and gravel operations situated in the floodplains of rivers and major streams.
- **Raypol sílt loam (12).** This series consists of deep, poorly drained soils formed in a coarse-loamy mantle underlain by sandy water deposited glacial outwash materials. They are nearly level and gently sloping soils on outwash plains and high stream terraces. The soils formed in loamy over stratified sandy and gravelly glacial outwash derived mainly from acid rocks. Typically these soils have very dark brown, silt loam Ap horizons, grayish brown and dark yellowish brown, mottled, silt loam and very fine sandy loam B2 horizons over light olive brown, mottled gravelly sand IIC horizons at a depth of 29 inches.

PAGE <u>3</u> OF <u>3</u>

Wetland Soils

#### DATE: 12/11/2018

### **ON-SITE SOIL INVESTIGATION & WETLAND DELINEATION REPORT** (CONTINUED)

PROJECT NAME & SITE LOCATION: (+/- 21.05 acres) (6 parcels) 291 Talcotville and Naek Roads, Vernon, CT

### SOIL MAP UNITS

Timakwa and Natchaug mucks (17). The Timakwa series consists of very deep, very poorly drained soils formed in formed in woody and herbaceous organic materials 16-50 inches thick overlying sand deposits over sandy deposits in depressions on lake plains, outwash plains, till plains, moraines, pond basins, and flood plains. Adrian soils are in extinct lake and pond basins, primarily within outwash plains. Basins range from nearly an acre to several hundred acres in size. Saturated hydraulic conductivity is moderately low to high in the organic layers and high or very high in the sandy material. Slope ranges from 0 to 2 percent. Mean annual temperature is about 48 degrees F and the mean annual precipitation is about 47 inches. Adjacent upland soils are generally sandy. Typically these soils have a black muck layer that is 33 inches thick. The substratum to a depth of 60 inches is gray, loose sand.

The Natchaug series consists of very deep, very poorly drained soils formed in well-decomposed organic materials 16-50 inches thick overlying loamy mineral deposits, deposits in depressions on lake plains, outwash plains, till plains, moraines, and flood plains. These soils have moderate to very rapid permeability in the organic material and moderately slow to moderately rapid permeability in the loamy material. Slope ranges from 0 to 2 percent. Mean annual temperature is about 48 degrees F. and mean annual precipitation is about 47 inches. Typically these soils have a black muck layer that is 33 inches thick. The substratum to a depth of 60 inches is dark gray, friable, gravelly silt loam.

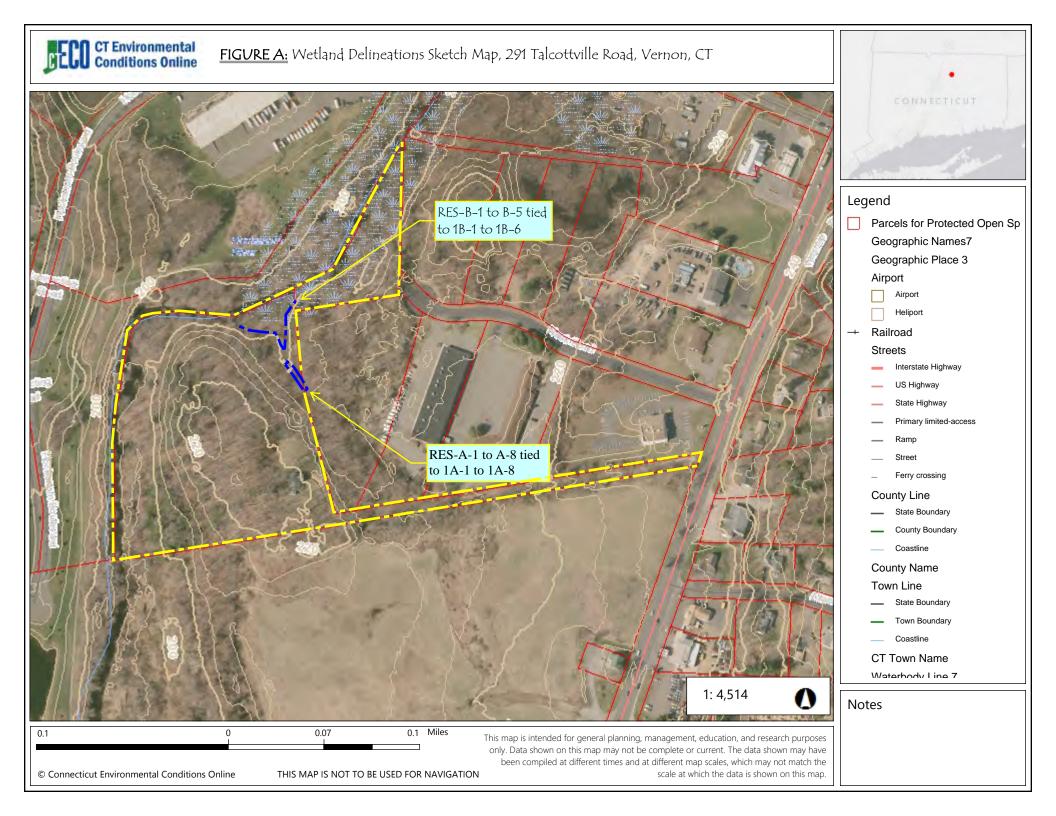
Any accompanying soil logs and soil maps, and the on-site soil investigation narrative are in accordance with the taxonomic classification of the National Cooperative Soil Survey of the USDA Natural Resource Conservation Service, and with the Connecticut Soil Legend (DEP Bulletin No.5, 1983), as amended by USDA-NRCS. Jurisdictional wetland boundaries were delineated pursuant to the Connecticut General Statutes (CGS Sections 22a-36 to 22a-45), as amended. The site investigation was conducted and/or reviewed by the undersigned Registered Soil Scientist(s) [registered with the Society of Soil Scientists of Southern New England (SSSSNE) in accordance with the standards of the Federal Office of Personnel Management].

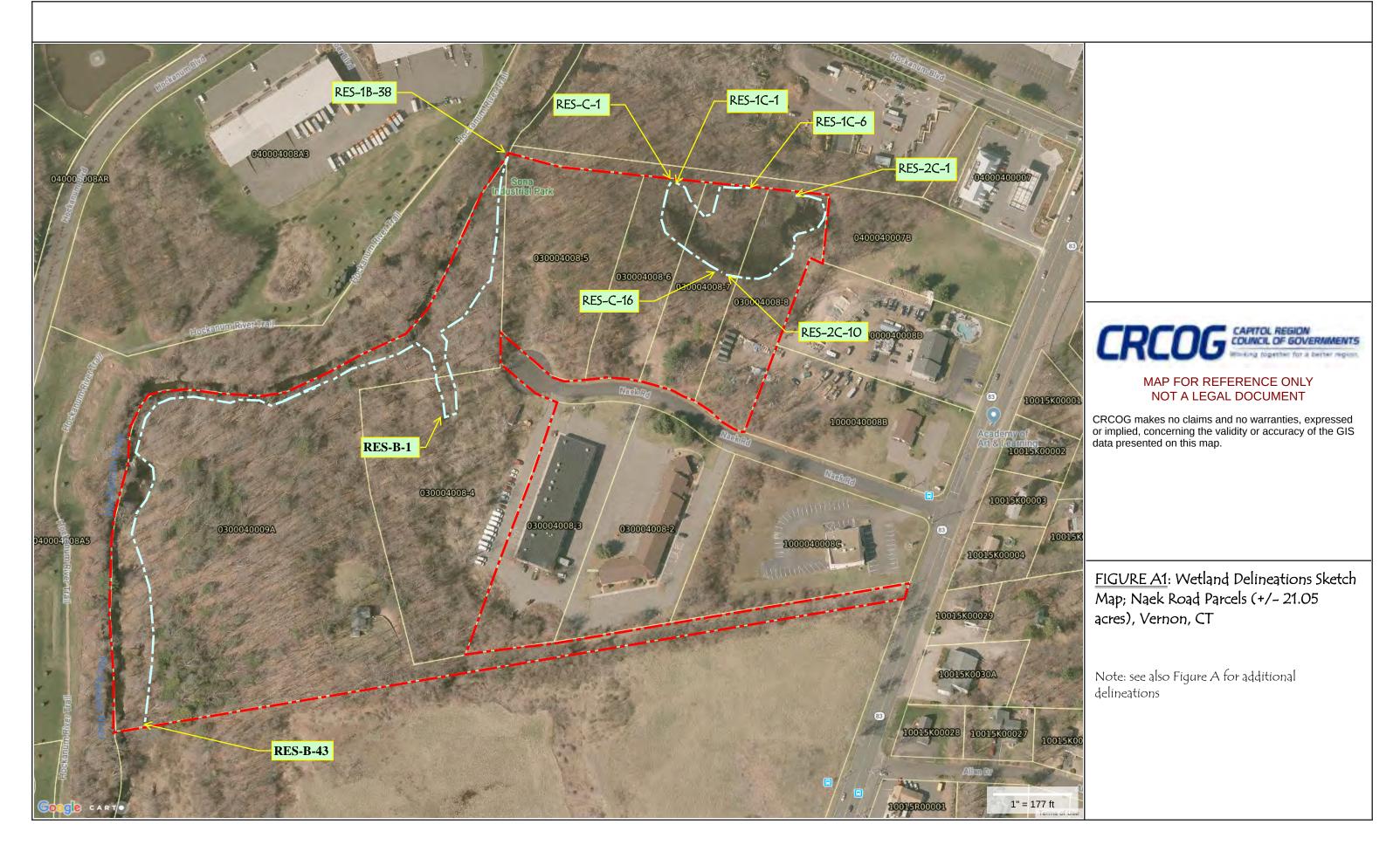
Respectfully submitted,

**REMA ECOLOGICAL SERVICES, LLC** 

age 1. Lagar

George T. Logan, MS, PWS, CSE Registered Soil Scientist Field Investigator/Senior Reviewer







USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey

Area of Interest (AOI)       Stony Spot       1:12         Soils       Very Stony Spot       Wat         Soil Map Unit Polygons       Wet Spot       Enking         Soil Map Unit Lines       Met Spot       Enking         Soil Map Unit Points       Other       Inne         Soil Map Unit Points       Special Line Features       Scan         Special Point Features       Streams and Canals       Pleat         Borrow Pit       Transportation       sca         Soil Closed Depression       Interstate Highways       Coor         Gravel Pit       Wis Routes       Major Roads       projoidist         Gravelly Spot       Major Roads       Alba       Alba         Area of Interest Flow       Background       Acrial Photography       This	MAP INFORMATION
Miscellaneous Water       Soil         ●       Perennial Water       Soil         ●       Rock Outcrop       1:50         +       Saline Spot       Dat         Sandy Spot       The         ●       Severely Eroded Spot       con         ●       Scille Law       ima	MAP INFORMATION         The soil surveys that comprise your AOI were mapped at :12,000.         Varning: Soil Map may not be valid at this scale.         Enlargement of maps beyond the scale of mapping can cause nisunderstanding of the detail of mapping and accuracy of soil ne placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed cale.         Please rely on the bar scale on each map sheet for map measurements.         Source of Map:       Natural Resources Conservation Service Veb Soil Survey URL:         Coordinate System:       Web Mercator (EPSG:3857)         Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts listance and area. A projection that preserves area, such as the Abers equal-area conic projection, should be used if more focurate calculations of distance or area are required.         This product is generated from the USDA-NRCS certified data a first eversion date(s) listed below.         Soil Survey Area:       State of Connecticut         Survey Area Data:       Version 16, Sep 15, 2017         Soil map units are labeled (as space allows) for map scales :50,000 or larger.       Date(s) aerial images were photographed:       Mar 28, 2011—Apr 8, 2011         The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background magery displayed on these maps. As a result, some minor thifting of map unit boundaries may be evident.



# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
6	Wilbraham and Menlo soils, 0 to 8 percent slopes, extremely stony	2.5	2.6%
17	Timakwa and Natchaug soils, 0 to 2 percent slopes	2.6	2.7%
20A	Ellington silt loam, 0 to 5 percent slopes	1.7	1.8%
30A	Branford silt loam, 0 to 3 percent slopes	0.6	0.6%
30B	Branford silt loam, 3 to 8 percent slopes	3.6	3.8%
32A	Haven and Enfield soils, 0 to 3 percent slopes	2.8	2.9%
32B	Haven and Enfield soils, 3 to 8 percent slopes	9.1	9.4%
33B	Hartford sandy loam, 3 to 8 percent slopes	1.3	1.3%
37C	Manchester gravelly sandy loam, 3 to 15 percent slopes	17.6	18.3%
63B	Cheshire fine sandy loam, 3 to 8 percent slopes	13.5	14.0%
63C	Cheshire fine sandy loam, 8 to 15 percent slopes	0.1	0.1%
64B	Cheshire fine sandy loam, 3 to 8 percent slopes, very stony	0.7	0.7%
66B	Narragansett silt loam, 2 to 8 percent slopes	0.5	0.6%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	6.7	6.9%
109	Fluvaquents-Udifluvents complex, frequently flooded	9.5	9.8%
306	Udorthents-Urban land complex	23.5	24.5%
Totals for Area of Interest		96.2	100.0%

The Village at Naek Road Naek Road Vernon, Connecticut

# **STORMWATER MANAGEMENT REPORT**

October 8, 2020

PREPARED FOR: The Rashid Hamid Family, LLP 27 Naek Road Vernon, Connecticut

PREPARED BY: Gardner & Peterson Associates, LLC 178 Hartford Turnpike Tolland, CT 06084

# TABLE OF CONTENTS

I.	Stormwater Management Narrative	1-4
II.	USGS Topographic Quadrangle Map	5
III.	FEMA Flood Insurance Rate Map	6
IV.	Hydrologic Soil Group Map and Legend	7-8
V.	Deep Test Pit Data	9
VI.	Gutter Flow and Storm Sewer Design	10-11
VII.	<ul> <li>Computation Sheets</li> <li>a. WQV / Forebay Design</li> <li>b. Ground Water Volume (GRV)</li> <li>c. Grass Swale Design</li> <li>d. Shear Stress in Vegetative Channel</li> <li>e. Capacity of Existing Drainage System</li> <li>f. Rain Garden / Bioretention Design</li> </ul>	12 13 14 15 15 16
VIII.	Pre & Post Development Runoff Analysis	17-51
IX.	Roof Infiltration Analysis	52-75
X.	Rainfall Report	76
XI.	Drainage Area Maps a. Existing Conditions b. Proposed Conditions	A1 A2

#### The Village at Naek Road

#### **Summary:**

This application proposes to construct eighteen new multi-family buildings on 21.6 acres, located on the northerly and southerly side of Naek Road. Access to the proposed development will be along the frontage on Naek Road with an emergency access through an existing easement to the Trail Run apartments located immediately south of this project. The new buildings will be serviced by public sanitary sewer and water services.

#### **Existing Conditions:**

Currently this project consists of 7 parcels that will be combined as a result of this project. The entire site is wooded except for a house located at 291 Talcottville Road, which will be removed to develop this project. Wetland areas have been delineated near the northeast corner of this site and along the Hockanum River which abuts the site to the west. Furthermore, a small wetland was also delineated toward the middle of the site which follows the floodplain of the Hockanum River. Stormwater runoff from this site drains westerly to the Hockanum River or northerly to the northeasterly wetland. A drainage system currently located in Naek Road will also collect water from a portion of this site. Runoff from Naek Road is conveyed northerly through a drainage easement where it discharges approximately 65 feet from the Hockanum River. The following pre and post development runoff analyses, compare the pre and post development rates of runoff at three locations; the Naek Road drainage system, the northeasterly wetland, and the Hockanum River to ensure that this development will not create an increase in runoff.

This site is mostly located within Zone 'X' (area determined to be outside 500-year floodplain), and partially withing Zone 'AE' (special flood hazard area inundated by the 100-year flood, base flood elevations determined) and partially within Zone 'X' (areas of 500-year flood; area of 100-year flood with average depths of less than 1 food or with drainage areas less than 1 square mile; and areas protected by levees from 100-year flood) per "FIRM Flood Insurance Rate Map Town of Vernon, Connecticut, Tolland County, Community-Panel Number 090131 0005 C, Map Revised August 9, 1999". This site is not located within the Level A Aquifer Protection Area as depicted on the Zoning Map, Vernon, CT dated 7/31/2020.

According to the NRCS Web Soil Survey the portion of this site located to the north of Naek Road is classified as Manchester gravelly sandy loam (Hydrologic Soil Group 'A'), the area to the south of Naek Road is classified as Charlton-Chatfield complex (Hydrologic Soil Group 'B'), and the portions of the site adjacent to the Hockanum River is classified as Fluvaquents-Udifluvents complex and Timakwa and Natchaug soils (Hydrologic Soil Group 'D'). Manchester gravelly sandy loam is typically an excessively drained soil with a low moistureholding capacity, while Charlton-Chatfield soils are typically well drained soils covered with cobbles, stones or boulders. Eighteen test pits were excavated on this property and permeability samples were tested to determine where suitable soils are located for the infiltration of stormwater into the ground. The soil profiles located on page 9 indicate that the Manchester gravelly sandy loam is located on the north side of Naek Road and on 37 Naek Road more or less. The soil profiles in these areas generally indicate that the groundwater is deep, and the soils are suitable for stormwater infiltration.

#### **Stormwater Management:**

The proposed stormwater management system has been designed to comply with the "Connecticut Department of Transportation Drainage Manual, 2000", the "2004 Connecticut Stormwater Quality Manual" and the "Low Impact Development Stormwater Quality Manual Town of Vernon, February 2013". These manuals require that a stormwater management system for new projects control stormwater peak rates of runoff and provide stormwater quality treatment. The stormwater management system for this project utilizes conventional and LID systems to collect, convey, retain, infiltrate and treat stormwater runoff prior to reaching the drainage system in Naek Road or any wetland areas.

Runoff from the newly paved areas and the front portion of the building rooftops will be collected in a drainage system that conveys the runoff to one of two new stormwater basins on site. Before entering the basin, pretreatment is provided by deep sump catch basins, oil/water separators, and grass swales to remove grit and floatables from the runoff. The runoff is discharged into a sediment forebay that has been designed to contain 10% of the Water Quality Volume (WQv) as recommended in the 2004 Connecticut Stormwater Quality Manual before entering the wet pond portion of the stormwater basins that is used for primary treatment and runoff attenuation. Runoff from smaller storms will be completely infiltrated back into the ground once treated by the previously mentioned treatment-train. The bottom of both basins will be excavated down to the native sandy soils to allow this to occur. Furthermore, to ensure lasting infiltration, an infiltration trench has been incorporated into the basin and located furthest from the basin inlets to increase travel time in the basin.

Runoff from larger storms that is not infiltrated, will exit the northerly basin and be piped to the drainage system in Naek Road. This flow from the southerly basin will exit the basin over a designed spillway and travel overland to a wetland system. Runoff exiting both basins will eventually make its way to the Hockanum River. Considering the proximity of the Hockanum River, the stormwater basins have been designed to detain flow the 2-year and 10-year storms and allow flow from the 100-year storm to exit through the high-level outlet with minimal detention. The purpose of this design is to allow the water from the basin to reach the Hockanum River prior to the river's peak. Therefore, not increasing flow to the peak of the river. The existing drainage system in Naek Road has also been analyzed and it was determined that the system has adequate capacity to convey the post-development flow from storms up to and including the 100-year storm. The results of the pre-development and post-development analysis are tabulated below:

Hydrograph \ Storm Frequency	2-Yr	10-Yr
#12: Proposed to River (cfs)	7.84	22.39
#11: Existing to River (cfs)	9.77	31.15

Multiple stormwater infiltration systems have been designed where the Manchester gravelly sandy loam was found. Water from the rear of the new building rooftops, which is considered clean water, will be collected and infiltrated it back into the ground in underground leaching chambers. The chambers have been designed to store runoff from the 100-year storm off the rooftops and grassland collected in the watershed to the chambers.

To maintain pre-development annual groundwater recharge volumes, this site has been evaluated for pre- and post-development Groundwater Runoff Volume (GRv) as described in the 2004 *Connecticut Stormwater Quality Manual*. This will ensure that water table levels, stream baseflow and wetland moisture levels will be maintained post-development. To determine the required GRv, the Hydrologic Soil Group Approach was utilized. The GRv analyses indicate that with the use of the designed rain gardens, infiltration chambers, and infiltration stormwater basins, this project will maintain the pre-development GRv once constructed. Even though the infiltration chambers and infiltration basins are sized for larger storms, for this calculation, the water quality volume was used to determine the provided contribution to the groundwater.

#### **Erosion & Sediment Control:**

The erosion & sediment control plan for this site consists of the use of soil stockpile areas, check dams, silt fencing, and coir logs down gradient of all disturbed areas. An anti-tracking pad will be installed at the entrance to the site. A more detailed E&S narrative in included in the plan set.

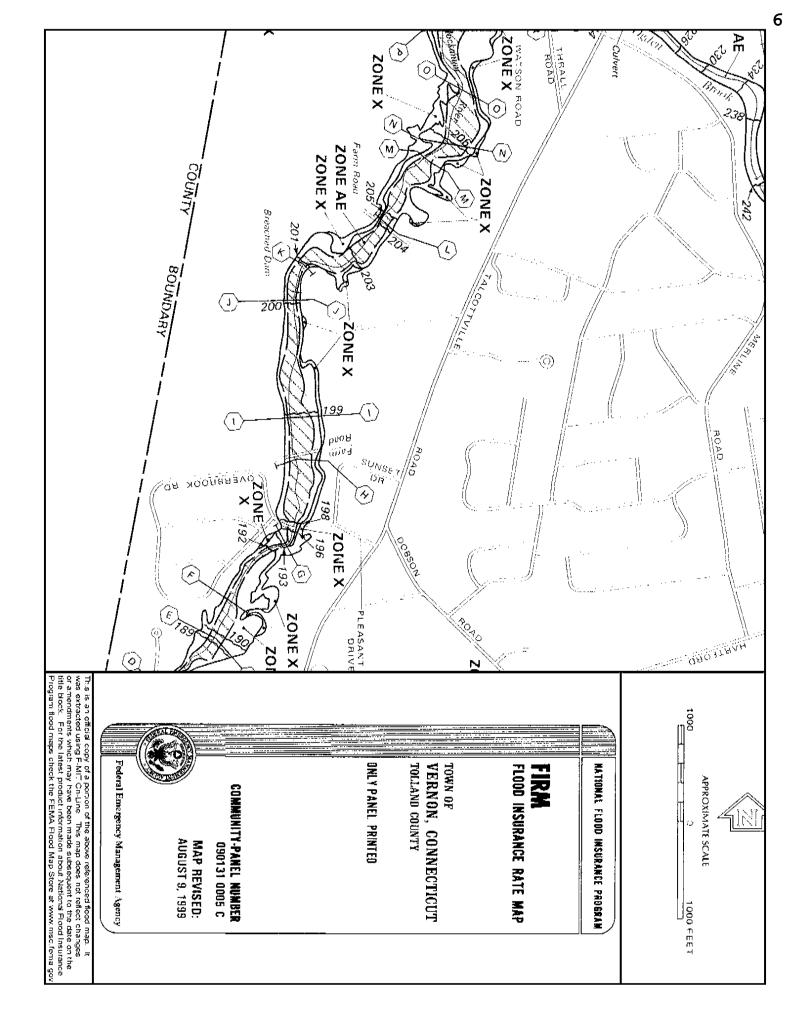
All sediment and erosion control procedures and construction of all stormwater drainage structures shall essentially be in accordance with the "2002 Connecticut Guidelines For Soil Erosion and Sediment Control" by the Connecticut Council on Soil and Water Conservation.

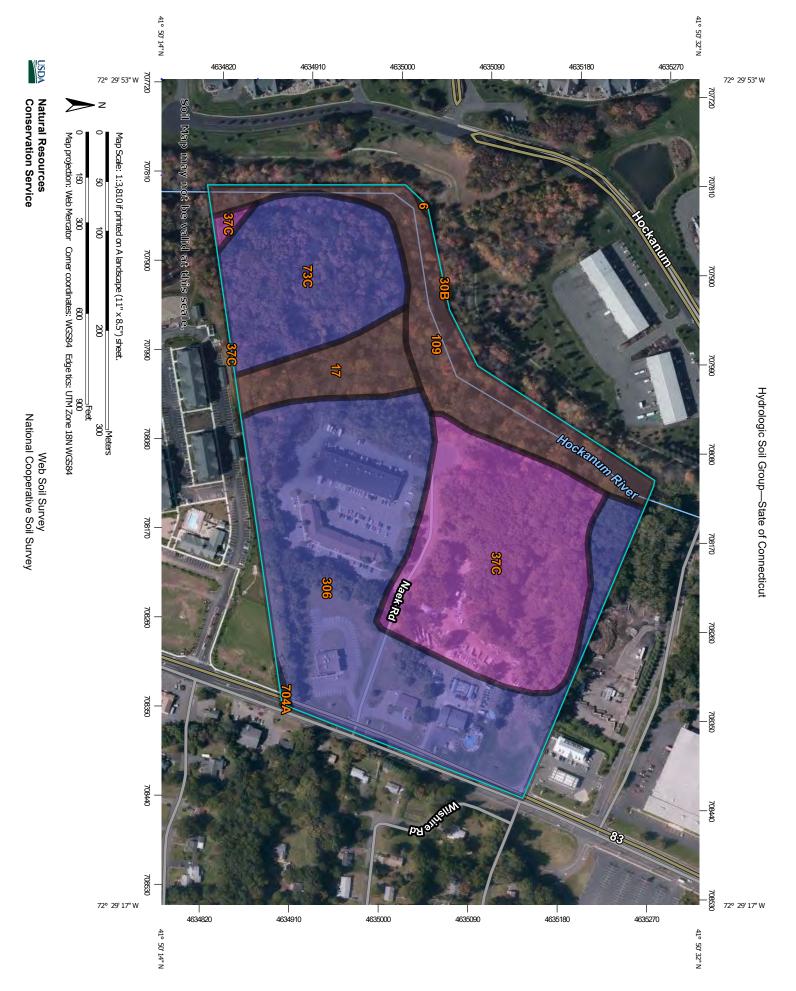


Eric R. Peterson, P.E. 23430

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# Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
6	Wilbraham and Menlo soils, 0 to 8 percent slopes, extremely stony	C/D	0.0	0.0%
17	Timakwa and Natchaug soils, 0 to 2 percent slopes	B/D	2.5	5.8%
30B	Branford silt loam, 3 to 8 percent slopes	В	0.0	0.0%
37C	Manchester gravelly sandy loam, 3 to 15 percent slopes	A	10.5	24.9%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	В	6.4	15.1%
109	Fluvaquents-Udifluvents complex, frequently flooded	B/D	5.6	13.4%
306	Udorthents-Urban land complex	В	17.1	40.6%
704A	Enfield silt loam, 0 to 3 percent slopes	В	0.0	0.1%
704B	Enfield silt loam, 3 to 8 percent slopes	В	0.0	0.0%
Totals for Area of Inter	rest		42.2	100.0%



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Job:	5768 –	5768 – The Village at Naek Road							
Sheet No:	9	of	76						
Calculated By:	ERP	Date	10/08/2020						
Checked By:		Rev.							

TEST PIT DATA:	
WITNESSED BY E. PETERSON, P.E.	
GARDNER & PETERSON ASSOCIATES, LLC	
0.510.0.10.0.0	
06/02/2020	TP 314:
TP 303:	LEDGE @ 24"
0-9" TOPSOIL	
9-14" COARSE LOAMY SAND	TP 314A:
14-108" COARSE SAND W/ COBBLES	0-36" FRACTURED ROCK
TP 305:	TP 315:
0-13" TOPSOIL	LEDGE @ 36" (WEST)
13-22" Y.BR. FINE SANDY LOAM	LEDGE @ 30" (EAST)
22-72" R.BR. TILL, COMPACT	
MOTTLING @ 16"	TP 316:
SEEPAGE @ 68"	0-4" TOPSOIL
	4-33" BR. FINE SANDY LOAM W/ COBBLES
TP 307:	33-54" BR. COMPACT TILL W/ FLAT BOULDERS
0-18" TOPSOIL/FILL	54-78" SAND & GRAVEL W/ BOULDERS
18-30" Y.BR. FINE SANDY LOAM	LEDGE @ 78"
30-72" R.BR. TILL	PERM #12 @ 23" RATE: 0.4 FT/DAY
MOTTLING @ 18"	TERM #12 @ 25 RATE. 0.4 F1/DAT
	TP 317:
SEEPAGE @ 40"	
<b>TD</b> 200	0-10" TOPSOIL
TP 308:	10-58" BONEY BR. FINE SANDY LOAM
0-38" SAND & GRAVEL FILL	LEDGE @ 58"
38-44" BURIED TOPSOIL	
44-138" SAND & GRAVEL	TP 317A:
SHGW @ 108"	0-8" TOPSOIL
PERM @ 58" RATE: 190 FT/DAY	8-30" BR. FINE SANDY LOAM W/ COBBLES
	30-78" R.BR. COMPACT TILL W/ FLAT BOULDERS
TP 310:	LEDGE @ 78"
0-11" TOPSOIL	
11-28" BR. FINE SANDY LOAM	TP 318:
28-84" FIRM R.BR. SILT	0-8" TOPSOIL
84-144" MED. SAND W/ COBBLES, SOME SILT	8-36" Y.BR. FINE SANDY LOAM W/ COBBLES, FIRM
GW @ 126"	36-60" R.BR. TILL W/ COBBLES
PERM #1 @ 115' RATE: 70 FT/DAY	60-80" DECOMPOSED LEDGE
STANDPIPE SET: DRY ON 06/16/2020	
	TP 319:
TP 311:	0-9" TOPSOIL
0-11" TOPSOIL	9-24" Y.BR. LOAMY SAND W/ COBBLES
11-102" BR. SAND & GRAVEL	24-60" SAND & GRAVEL
192-144" COMPACT FINE SAND W/ SILT	60-132" COARSE SAND
PERM #2 @ 50" RATE: 61 FT/DAY	PERM #70 @ 36" RATE: 370 FT/DAY
	TERM #70 @ 50 KITE. 570 T I/DAT
TP 312:	TP 320:
0-16" TOPSOIL	LEDGE @ 32"
16-32" FINE SANDY LOAM	
	TP 321:
32-144" SAND & GRAVEL	
PERM #3 @ 36" RATE: 41 FT/DAY	0-12" TOPSOIL
TD 212.	12-20" Y.BR. FINE SANDY LOAM
TP 313:	20-116" SAND & GRAVEL
0-7" TOPSOIL	SEEPAGE @ 116"
7-15" Y.BR. FINE SANDY LOAM	
15-43" R.BR LOAMY SAND W/ COBBLES, SOMEWHAT	08/16/2020
FIRM	TP H1:
LEDGE @ 43"	0-6" TOPSOIL
	6-28" Y.BR. FINE SANDY LOAM
	28-36" MED. SAND W/ COBBLES
	PERM #1 @ 32" RATE: 12 FT/DAY

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JOB	5768 - The Village	at Na	aek Road
SHEET NO.	10	OF	76
CALCULATED BY	ERP	DATE	10/8/2020
CHECKED BY		REV.	

### **GUTTER FLOW ANALYSIS**

AI Entering Catch Basin	0.17	0.24	0.16	0.13	0.49	0.23	0.21	0.19	0.34	0.07	0.25	0.33	0.26	0.09	2.61	0.09	
AI Bypassing Inlet	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Q Bypassing Inlet (cfs)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Width of Flow (ft)	4.5	5.2	4.4	4.3	7	5.0	5	4.7	9	3	5.2	9	5.8	3.8	ΡΤ	2.8	
Depth of Flow at Gutter (ft)	0.14	0.17	0.13	0.12	0.21	0.15	0.15	0.14	0.19	0.09	0.17	0.19	0.18	0.11	LOW	0.09	
Cross Slope fo Shoulder	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.1	0.03	
Grade of Gutter (ft/ft)	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.08	
Q To Inlet (cfs)	0.9	1.3	0.8	0.7	2.5	1.2	1.2	1.0	1.8	0.3	1.3	1.8	1.4	0.5	10.4	0.5	
10yr Rainfall Intensity (in/hr)	5.3	5.3	5.1	5.5	5.1	5.3	5.5	5.3	5.3	3.9	5.3	5.3	5.3	5.5	4.0	5.3	
Total AI	0.17	0.24	0.16	0.13	0.49	0.23	0.21	0.19	0.34	0.07	0.25	0.33	0.26	0.09	2.61	0.09	
Sum Al	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
AI	0.17	0.24	0.16	0.13	0.49	0.23	0.21	0.19	0.34	0.07	0.25	0.33	0.26	0.09	2.61	0.09	
Runoff Coeficient	0.73	0.73	0.71	0.74	0.77	0.77	0.76	0.75	0.72	0.52	0.77	0.73	0.73	0.76	0.52	0.76	
Area (Acres)	0.23	0.33	0.23	0.17	0.64	0.3	0.27	0.25	0.47	0.13	0.33	0.45	0.35	0.12	5.01	0.12	
Time To Inlet (Min)	8	8	6	7	6	8	7	8	œ	16	8	8	8	7	15	8	
Inlet Number	CB 4	CB 5	CB 11	CB 12	CB 15	CB 16	CB 18	CB 19	CB 21	CB 24	CB 25	CB 26	CB 27	CB 28	FE 29	CB 30	

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#### JOB 5768 - The Village at Naek Road

#### **STORM SEWER DESIGN**

N'	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012
Headwater (ft)	0.5	0.8	0.7	0.5	0.7	0.7	0.9	1.1	0.6	0.8	0.8	1.1	0.4	0.7	0.9	1.0	1.1	1.7	2.0
Full Capacity (cfs)	10.5	8.5	15.6	5.2	5.3	15.3	7.4	16.9	7.4	12.8	5.3	5.2	11.3	6.6	6.8	5.3	6.5	17.4	17.4
Average Velocity (fps)	8.6	6.9	12.7	4.2	4.3	12.5	6.1	13.8	9	10.4	4.4	4.2	9.2	5.4	5.5	4.4	5.3	5.5	5.5
Slope (%)	2.26	1.47	4.92	0.55	0.57	4.78	1.12	5.83	1.11	3.33	0.58	0.54	2.59	0.88	0.94	0.58	0.86	0.50	0.50
Length of Pipe (ft)	40	47	35	35	89	97	17	32	18	75	207	150	77	28	21	278	35	140	90
Pipe Size (in)	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	15	24	24
Q In System (cfs)	0.9	2.2	1.5	0.8	1.5	1.5	2.5	3.7	1.2	2.1	2.1	3.9	0.3	1.3	2.5	3.6	3.8	10.4	14.1
10yr Rainfall Intensity (in	5.3	5.3	/ Basin =	5.1	5.1	5.1	5.1	5.1	5.5	5.3	5.3	5.3	3.9	5.3	3.9	3.9	3.8	4	3.8
Sum AI In System	0.17	0.41	Out of N'ly	0.16	0.29	0.29	0.49	0.72	0.21	0.40	0.40	0.74	0.07	0.25	0.65	0.91	1.00	2.61	3.70
AI Entering Catch Basin	0.17	0.24		0.16	0.13	0	0.49	0.23	0.21	0.19	0	0.34	0.07	0.25	0.33	0.26	0.09	2.61	0.09
Accumulated Time (min)	8	8	1	6	6	6	6	6	7	8	8	8	16	8	16	16	17	15	17
Time In Pipe (sec)	5	7	ю	8	21	8	ю	2	З	7	47	36	8	5	4	63	7	25	16
Time To Inlet (Min)	œ	ø	:	6	2	0	6	8	7	œ	0	8	16	8	8	8	2	15	8
Line Segment	4-5	5-6	8-EX	11-12	12-13	13-14	15-16	16-17	18-19	19-20	20-21	21-22	24-26	25-26	26-27	27-28	28-30	29-30	30-31

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Job:	5768 –	The Village	at Naek Road	
Sheet No:	12	of	76	
Calculated By:	ERP	Date	10/08/2020	
Checked By:		Rev		
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ETERMINE THE WATE	ER QUALITY VOLUME:
$WQV = \frac{1" x R x A}{12}$	<u>A</u> $R = 0.05 + (0.009 \text{ x I})$
Northerly Stormw	vater Basin:
-	West Inlet:       A = 0.80 Acres       I = 56%       R = 0.55         WQV = 1,600 cu.ft.       Size Forebay for 10% WQV:       Volume (required) = 10% x 1,600 = 160 cu.ft.         Volume (required) = 10% x 1,600 = 160 cu.ft.       Volume (provided) = 168 cu.ft.
J	East Inlet: $A = 0.45$ Acres $I = 64\%$ $R = 0.63$ WQV = 1,030 cu.ft. Size Forebay for 10% WQV: Volume (required) = 10% x 1,030 = 103 cu.ft. Volume (provided) = 183 cu.ft.
Southerly Stormw	North Inlet: $A = 0.40$ Acres $I = 87.5\%$ $R = 0.84$
	WQV = 1,220 cu.ft. Size Forebay for 10% WQV: Volume (required) = 10% x 1,220 = 122 cu.ft. Volume (provided) = 140 cu.ft.
:	South Inlet: $A = 9.45$ Acres $I = 44.4\%$ $R = 0.45$ WQV = 16,090 cu.ft. Size Forebay for 10% WQV:
	Volume (required) = $10\% \times 16,090 = 1609$ cu.ft. Volume (provided) = $1,628$ cu.ft.

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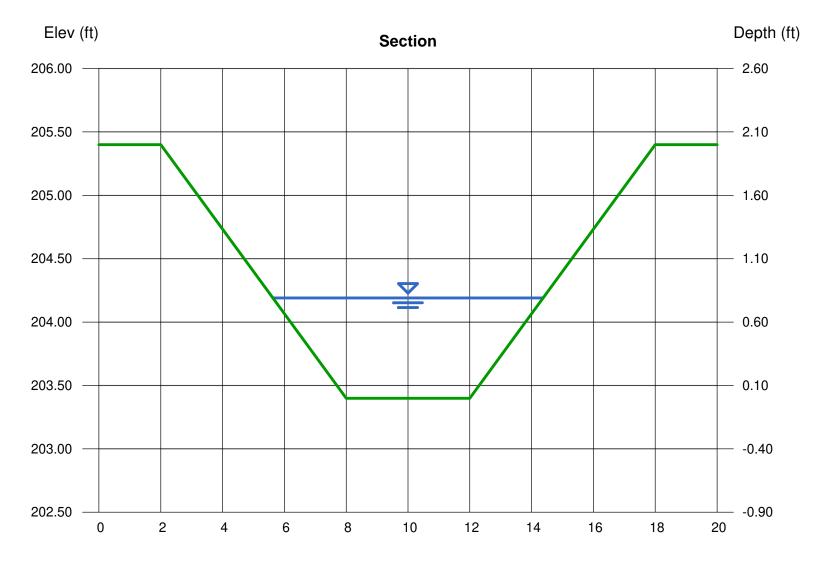
Job:	5768 – The Village at Naek Road						
Sheet No:	13	of	76				
Calculated By:	ERP	Date	10/08/2020				
Checked By:		Rev					

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GRV = (D)(A)(I) 12	GRV = Groundwater Recharge Volume D = Depth of runoff to be recharged (A soils=0.40 in, B soils=0.25 in) A = Site area I = Net increase in site imperviousness
To Northeasterly Wetland: A = 2.98 acres $A_I = 0.42$ acres I = 0.141 D = 0.40	
$GRV = (0.40) \times (2.98) \times 12$	(0.141) x 43560 = 610 cu.ft. required
$\label{eq:WQV Provided} WQV \mbox{ Provided} \mbox{ CB 2: } Rain \mbox{ CB 1: } Remainder of Site: \\ A = 18.63 \mbox{ acres } A_I = 4.78 \mbox{ acres } I = 0.257 \\ D = 0.25 \mbox{ D} = 0.25 $	: 591 cu.ft. Farden: <u>719 cu.ft.</u> 1310 cu.ft. > 610 cu.ft. √
$GRV = (0.25) \times (18.63)$ 12	x (0.257) x 43560 = 4,345 cu.ft. required
WQV Provided CB 1: CB 3: CB 9: CB 10 CB 23 Rain C N'1y E S'1y B Total:	360 cu.ft.         429 cu.ft.         309 cu.ft.         :       598 cu.ft.         :       722 cu.ft.         :       89 cu.ft.         :       2644 cu.ft.

Hydraflow Express Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc.

# **Grass Lined Swale into Southerly Basin**



14

Reach (ft)

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5768 – The Village at Naek Road							
15	of	76					
ERP	Date	10/08/2020					
	Rev						
-	15	15 of ERP Date	15 of 76 ERP Date 10/08/2020				

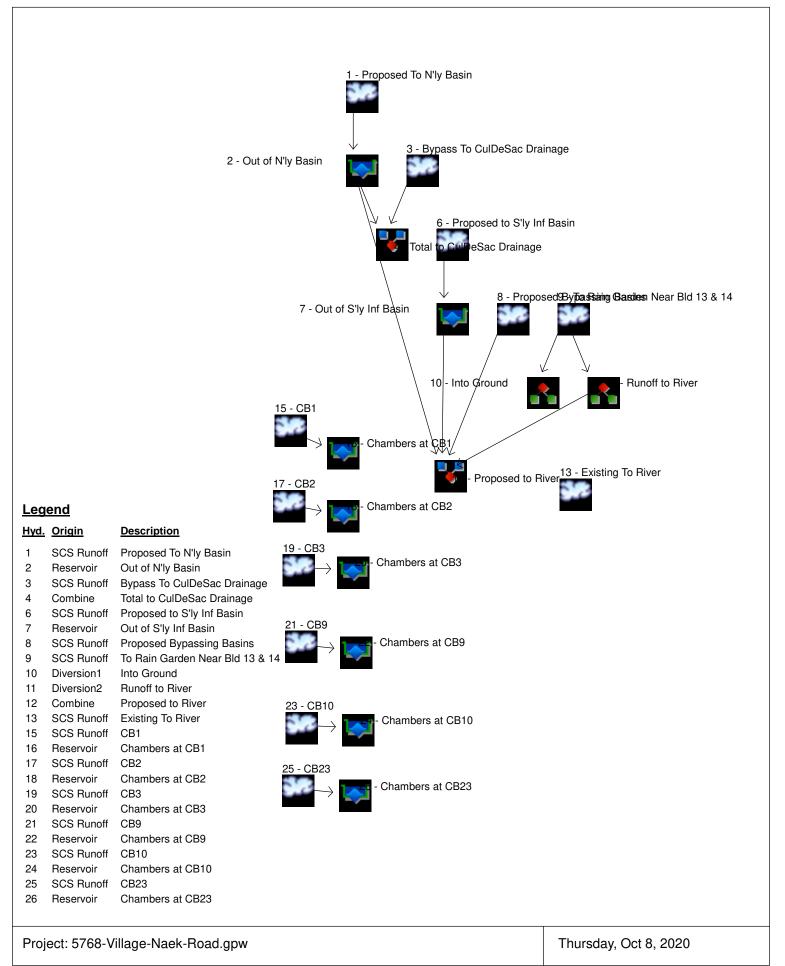
Tabl	ble 7-4 CT DOT Drainage Manual:	
1 801	Type 'A' Vegetative Channel: Permissible Unit Shear Stress = 3.70 l	$p/ft^2$
Max	$ \begin{array}{ll} \mbox{aximum Shear Stress: } \tau_d = \delta dS & \mbox{Eqn. 7.12 (CT DOT Drainage Manual} \\ \delta = 62.4 \mbox{ lb/ft3} \\ d = \mbox{maximum depth flow} = 0.79 \mbox{ ft (Pa} \\ S = \mbox{Average bed slope} = 1.5\% \mbox{ or } 0.01 \\ \tau_d = (62.4)(0.79)(0.015) \\ \tau_d = 0.74 \mbox{ lb/ft}^2 & < 3.70 \mbox{ lb/ft}^2 &  \end{array} $	ge 14)
DETERMIN	NE CAPACITY IN EXISTING DRAINAGE SYSTEM OFF THE END OF NAI	EK ROAD:
	"RCP: $S = 1.24\%$ $L = 150'$ "RCP: $S = 0.85\%$ $L = 252'$	
Prop	oposed Peak Flow to System = 20.23 cfs (100 year)	
Capa	apacity of Flattest Culvert (Manning's Formula): $Q = \frac{1.49 \text{ x A x } R^{2/3} \text{ x } S^{1/2}}{n}$	
	n = 0.013 $A = 3.1416$ $WP = 6.2832$ $R = A/WP$	= 0.5
	$Q = \frac{1.49 \text{ x } 3.1416 \text{ x } 0.5^{2/3} \text{ x } 0.0085^{1/2}}{0.013}$	
	Q = 20.9  cfs > 20.23  cfs	
	$HW/D = 1.4 \rightarrow HW = 1.4 \text{ x } 2.0 = 2.8 \text{ ft}$	
	Available Head = 8 ft in STMH at inlet end of pipe $$	
	Therefore, system has capacity to convey post-development 100-year flow	
Determine W	Width of Outlet Spillway to Southerly Stormwater Basin	
Spill	illway shall act as an emergency spillway and shall convey 100-year Peak Flow $Q_{100IN} = 38.32$ cfs	Entering the Basin
Capa	pacity of Spillway (Q) = $3.33 \text{ x} [W-0.2H] \text{ x } H^{1.5}$ For $H = 1.0'$ W = 12' $Q = 3.33 \text{ x} [12-(0.2x1.0)] \text{ x } 1^{1.5}$ Q = 39.3  cfs > 38.3  cfs =	
	12 ft wide spillway has capacity to convey the 100-year peak flow entering the b	

A 12 ft wide spillway has capacity to convey the 100-year peak flow entering the basin

#### GARDNER & PETERSON ASSOCIATES, LLC 178 HARTFORD TURNPIKE TOLLAND, CT 06084 TEL: 860-871-0808 www.GardnerPeterson.com

5768 – The Village at Naek Road						
16	of	76				
ERP	Date	10/08/2020				
	Rev.					
	16	16 of ERP Date	16 of 76 ERP Date 10/08/2020			

SIZE RAIN GARDENS / BIORETENTIO	DN:
$SA = WQv / h_f$ where:	
$\begin{split} SA &= Surface \ Area \ of \ Filter \ Bed \ (\\ WQv &= Water \ Quality \ Volume \ (c\\ h_f &= Depth \ of \ ponding \ above \ soil \\ For \ Soil \ Class \ 'A' \rightarrow h_f \\ For \ Soil \ Class \ 'B' \rightarrow h_f \end{split}$	f) surface per soil class (ft) = 12" or 1.0'
<u>Near Building #2:</u>	
$\begin{array}{l} A=0.33 \text{ Acres} \\ A_{I}=0.20 \text{ acres} \\ I=60.6\% \end{array}$	R = 0.05 + 0.009 I R = 0.60 $WQv = \frac{1" x R x A}{12} = (1) (0.60) (0.33) = 0.0165 \text{ ac-ft or } 720 \text{ cf}$
SA = 720 / 1.00 = 720 sc	
Surface Area Provided =	= 15' x 48' = 720 sq.ft.
Near Building #13 & #14	<u>4:</u>
$\begin{array}{l} A=0.13 \text{ Acres} \\ A_{I}=0.05 \text{ acres} \\ I=38.5\% \end{array}$	R = 0.05 + 0.009 I R = 0.40 WQv = $\frac{1" \times R \times A}{12} = (1) (0.40) (0.13) = 0.0043$ ac-ft or 190 cf
SA = 190 / 0.75 = 254 sc	
Surface Area Provided =	$= 11' \times 24' = 264 $ sq.ft.



# Hydrograph Return Period Recap Hydrafilew Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd.	Hydrograph	Inflow				Hydrograph					
No.	type (origin)	Hyd(s)	1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	description
1	SCS Runoff			1.402			3.123			5.626	Proposed To N'ly Basin
2	Reservoir	1		0.000			0.135			1.525	Out of N'ly Basin
3	SCS Runoff			4.302			10.07			18.70	Bypass To CulDeSac Drainage
4	Combine	2, 3		4.302			10.18			20.23	Total to CulDeSac Drainage
6	SCS Runoff			11.25			22.52			38.32	Proposed to S'ly Inf Basin
7	Reservoir	6		0.000			9.729			32.45	Out of S'ly Inf Basin
8	SCS Runoff			7.839			20.18			39.11	Proposed Bypassing Basins
9	SCS Runoff			0.155			0.338			0.600	To Rain Garden Near Bld 13 & 14
10	Diversion1	9		0.155			0.238			0.067	Into Ground
11	Diversion2	9		0.059			0.338			0.600	Runoff to River
12	Combine	2, 7, 8, 11		7.839			22.39			71.20	Proposed to River
13	SCS Runoff			9.773			31.15			66.10	Existing To River
15	SCS Runoff			0.011			0.179			0.632	CB1
16	Reservoir	15		0.000			0.000			0.000	Chambers at CB1
17	SCS Runoff			0.153			0.462			0.961	CB2
18	Reservoir	17		0.000			0.000			0.000	Chambers at CB2
19	SCS Runoff			0.159			0.363			0.664	CB3
20	Reservoir	19		0.000			0.000			0.000	Chambers at CB3
21	SCS Runoff			0.040			0.185			0.459	CB9
22	Reservoir	21		0.000			0.000			0.000	Chambers at CB9
23	SCS Runoff			0.104			0.387			0.884	CB10
24	Reservoir	23		0.000			0.000			0.000	Chambers at CB10
25	SCS Runoff			0.335			0.730			1.300	CB23
26	Reservoir	25		0.000			0.000			0.000	Chambers at CB23
Pro	j. file: 5768-V	/illage-Na	ek-Road	.apw					Thu	ursdav. C	Oct 8, 2020

# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	1.402	2	724	4,414				Proposed To N'ly Basin
2	Reservoir	0.000	2	726	0	1	207.39	968	Out of N'ly Basin
3	SCS Runoff	4.302	2	732	18,919				Bypass To CulDeSac Drainage
4	Combine	4.302	2	732	18,919	2, 3			Total to CulDeSac Drainage
6	SCS Runoff	11.25	2	732	46,600				Proposed to S'ly Inf Basin
7	Reservoir	0.000	2	1410	0	6	203.15	21,324	Out of S'ly Inf Basin
8	SCS Runoff	7.839	2	732	36,338				Proposed Bypassing Basins
9	SCS Runoff	0.155	2	724	484				To Rain Garden Near Bld 13 & 14
10	Diversion1	0.155	2	724	191	9			Into Ground
11	Diversion2	0.059	2	742	293	9			Runoff to River
12	Combine	7.839	2	732	36,631	2, 7, 8,			Proposed to River
13	SCS Runoff	9.773	2	734	52,246	11			Existing To River
15	SCS Runoff	0.011	2	762	257				CB1
16	Reservoir	0.000	2	762	0	15	207.85	0.725	Chambers at CB1
17	SCS Runoff	0.153	2	734	786				CB2
18	Reservoir	0.000	2	808	0	17	206.03	5.69	Chambers at CB2
19	SCS Runoff	0.159	2	734	749				СВЗ
20	Reservoir	0.000	2	784	0	19	201.25	7.55	Chambers at CB3
21	SCS Runoff	0.040	2	746	309				CB9
22	Reservoir	0.000	2	732	0	21	206.01	0.621	Chambers at CB9
23	SCS Runoff	0.104	2	742	677				CB10
24	Reservoir	0.000	2	788	0	23	205.01	1.61	Chambers at CB10
25	SCS Runoff	0.335	2	734	1,549				CB23
26	Reservoir	0.000	2	762	0	25	208.03	4.38	Chambers at CB23
5768-Village-Naek-Road.gpw					Return F	Period: 2 Ye	ar	Thursday, (	Dct 8, 2020

# Hydrograph Report

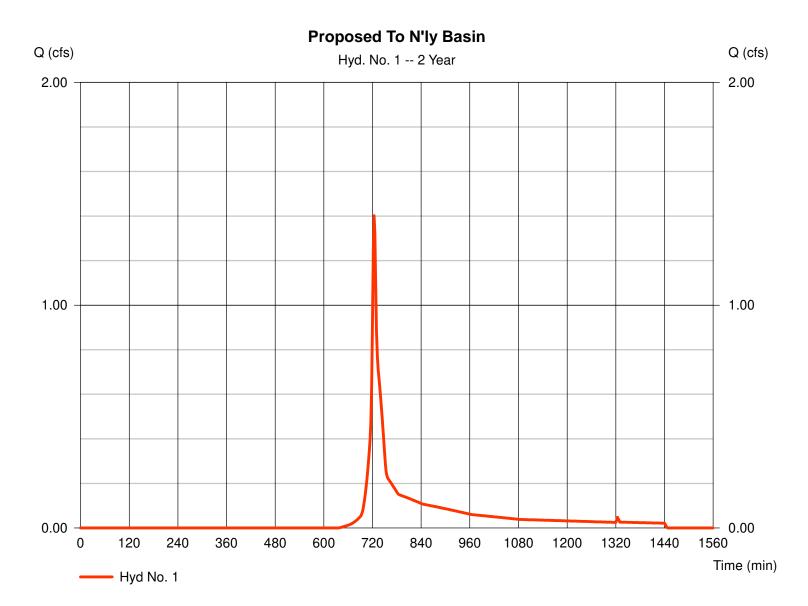
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

# Hyd. No. 1

Proposed To N'ly Basin

Hydrograph type	= SCS Runoff	Peak discharge	= 1.402 cfs
Storm frequency	= 2 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 4,414 cuft
Drainage area	= 1.250 ac	Curve number	= 74*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 5.60 min
Total precip.	= 3.20 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(0.740 x 98) + (0.510 x 39)] / 1.250



Thursday, Oct 8, 2020

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

# Hyd. No. 1

Proposed To N'ly Basin

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 30.0 = 3.20 = 4.00		0.011 70.0 3.20 2.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 4.13	+	0.91	+	0.00	=	5.04
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 80.00 = 2.00 = Paved = 2.87		20.00 15.00 Unpave 6.25	d	0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.46	+	0.05	+	0.00	=	0.52
<b>Channel Flow</b> X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	$\begin{array}{rcrr} = & 0.00 \\ = & 0.00 \\ = & 0.010 \\ = & 0.015 \\ = & 0.00 \\ = & 0.0 \end{array}$		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							

# Hydrograph Report

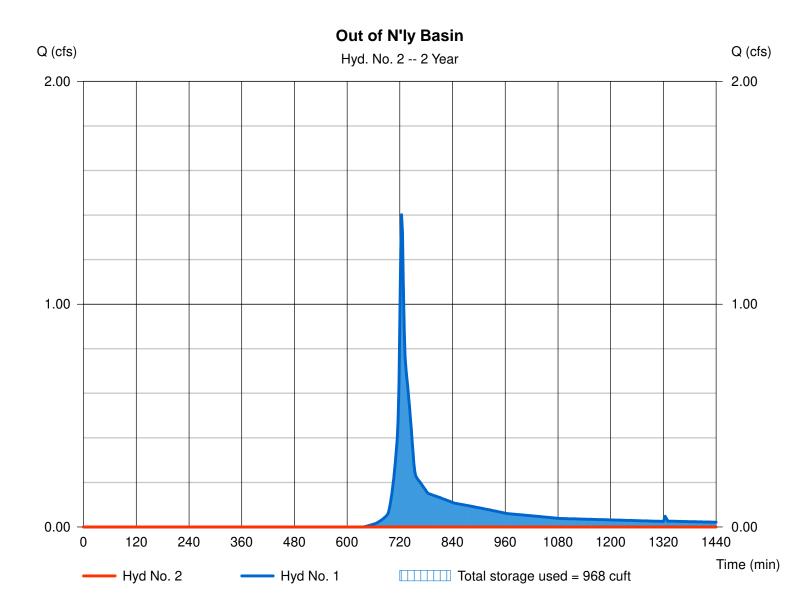
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

## Hyd. No. 2

Out of N'ly Basin

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 2 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 1 - Proposed To N'ly Basin	Max. Elevation	= 207.39 ft
Reservoir name	<ul> <li>N'ly Infiltration Basin</li> </ul>	Max. Storage	= 968 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



22

# **Pond Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

#### Pond No. 4 - N'ly Infiltration Basin

#### Pond Data

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 207.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	207.00	1,981	0	0
1.00 3.00	208.00 210.00	2,976 3,968	2,479 6,944	2,479 9,423

#### **Culvert / Orifice Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 207.70	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 36.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 8.00	0.00	0.00	n/a					
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 20.500 (l	by Contour)	)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

**Weir Structures** 

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

- · · · J · ·	J.											
Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0	207.00	0.00								0.000		0.000
2,479	208.00	0.42 ic								1.412		1.835
9,423	210.00	7.65 ic								1.883		9.529
	Storage cuft 0 2,479	Storage cuft         Elevation ft           0         207.00           2,479         208.00	Storage cuft         Elevation ft         Clv A cfs           0         207.00         0.00           2,479         208.00         0.42 ic	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs           0         207.00         0.00            2,479         208.00         0.42 ic	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs         Clv C cfs           0         207.00         0.00             2,479         208.00         0.42 ic	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs         Clv C cfs         PrfRsr cfs           0         207.00         0.00              2,479         208.00         0.42 ic	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs         Clv C cfs         PrfRsr cfs         Wr A cfs           0         207.00         0.00                                                                                            -	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs         Clv C cfs         PrfRsr cfs         Wr A cfs         Wr B cfs           0         207.00         0.00	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs         Clv C cfs         PrfRsr cfs         Wr A cfs         Wr B cfs         Wr C cfs           0         207.00         0.00	Storage cuftElevation ftClv A cfsClv B cfsClv C cfsPrfRsr cfsWr A cfsWr B cfsWr C cfsWr D cfs0207.000.002,479208.000.42 ic	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs         Clv C cfs         PrfRsr cfs         Wr A cfs         Wr B cfs         Wr C cfs         Wr D cfs         Exfil cfs           0         207.00         0.00              0.000           2,479         208.00         0.42 ic              1.412	Storage cuft         Elevation ft         Clv A cfs         Clv B cfs         Clv C cfs         PrfRsr cfs         Wr A cfs         Wr B cfs         Wr D cfs         Clv D cfs         Exfil User cfs         User cfs         cfs

# Hydrograph Report

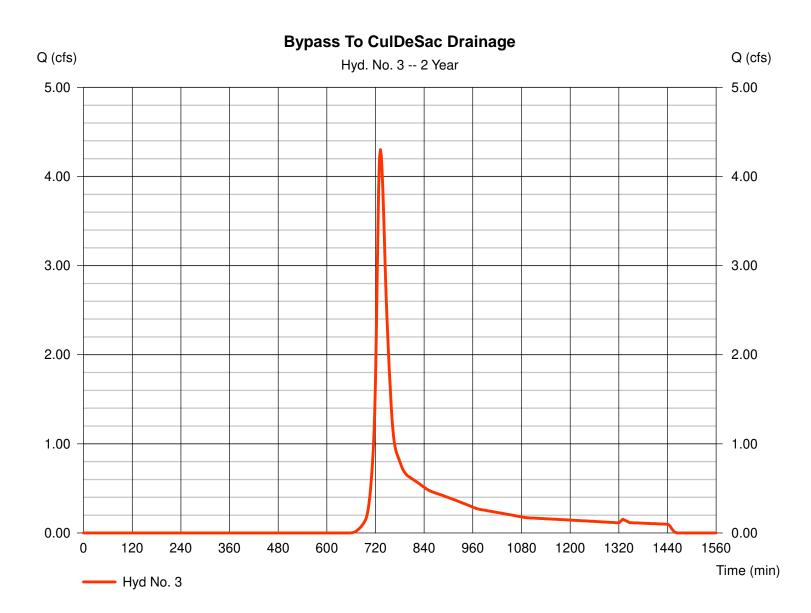
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

# Hyd. No. 3

Bypass To CulDeSac Drainage

Hydrograph type	= SCS Runoff	Peak discharge	= 4.302 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 18,919 cuft
Drainage area	= 5.750 ac	Curve number	= 72*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.10 min
Total precip.	= 3.20 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.430 x 98) + (0.480 x 30) + (0.920 x 55) + (0.320 x 39) + (1.600 x 61)] / 5.750



24

Thursday, Oct 8, 2020

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# Hyd. No. 3

Bypass To CulDeSac Drainage

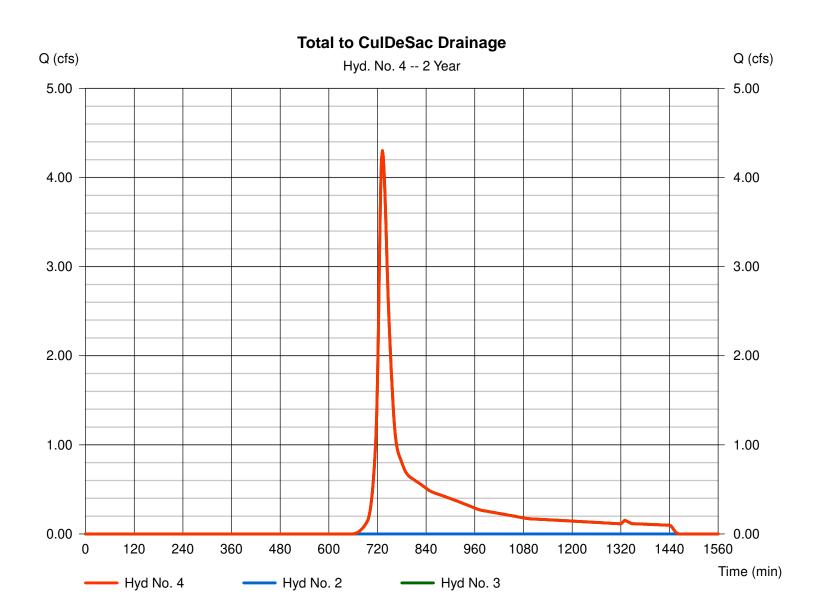
Description	<u>A</u>		<u>B</u>		<u>C</u>		<b>Totals</b>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.20 = 5.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 9.89	+	0.00	+	0.00	=	9.89
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 559.00 = 3.80 = Unpaved = 3.15	d	68.00 2.30 Paved 3.08		0.00 0.00 Paved 0.00		
Travel Time (min)	= 2.96	+	0.37	+	0.00	=	3.33
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 1.23 = 3.93 = 0.50 = 0.013 = 3.72 = 22.0		1.77 4.71 1.10 0.013 6.23 222.0		3.14 6.28 2.00 0.013 10.19 105.0		
Travel Time (min)	= 0.10	+	0.59	+	0.17	=	0.86
Total Travel Time, Tc							14.10 min

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### Hyd. No. 4

Total to CulDeSac Drainage

Hydrograph type	= Combine	Peak discharge	= 4.302 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 18,919 cuft
Inflow hyds.	= 2, 3	Contrib. drain. area	a = 5.750 ac



26

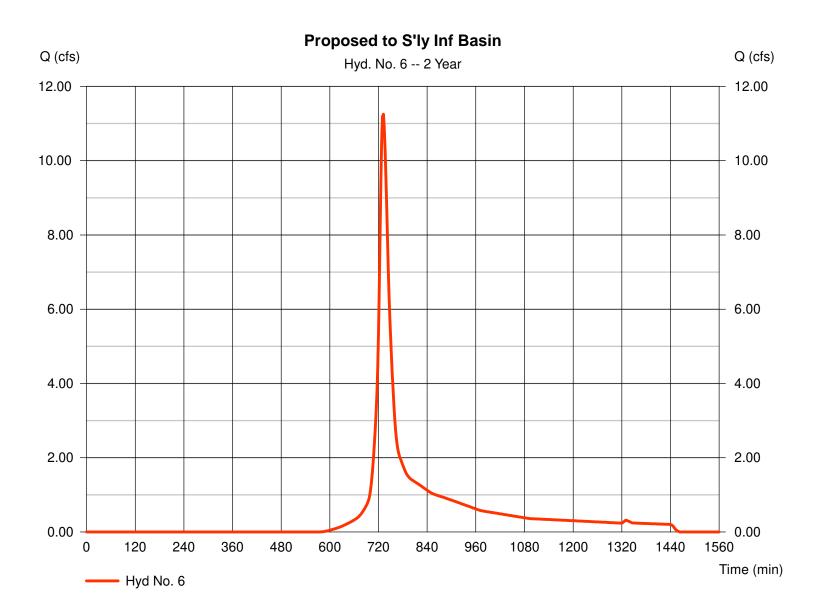
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### Hyd. No. 6

Proposed to S'ly Inf Basin

Hydrograph type	= SCS Runoff	Peak discharge	= 11.25 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 46,600 cuft
Drainage area	= 9.850 ac	Curve number	= 79*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.10 min
Total precip.	= 3.20 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.550 x 98) + (0.020 x 30) + (1.540 x 55) + (1.080 x 80) + (2.660 x 61)] / 9.850



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

### Hyd. No. 6

Proposed to S'ly Inf Basin

<b>Description</b>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.20 = 5.00		0.011 0.0 3.20 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 9.89	+	0.00	+	0.00	=	9.89
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 193.00 = 2.20 = Unpave = 2.39	d	293.00 3.50 Unpave 3.02	d	419.00 1.90 Paved 2.80		
Travel Time (min)	= 1.34	+	1.62	+	2.49	=	5.45
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 3.14 = 6.28 = 0.50 = 0.013 = 5.09 = 230.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.75	+	0.00	+	0.00	=	0.75
Total Travel Time, Tc						16.10 min	

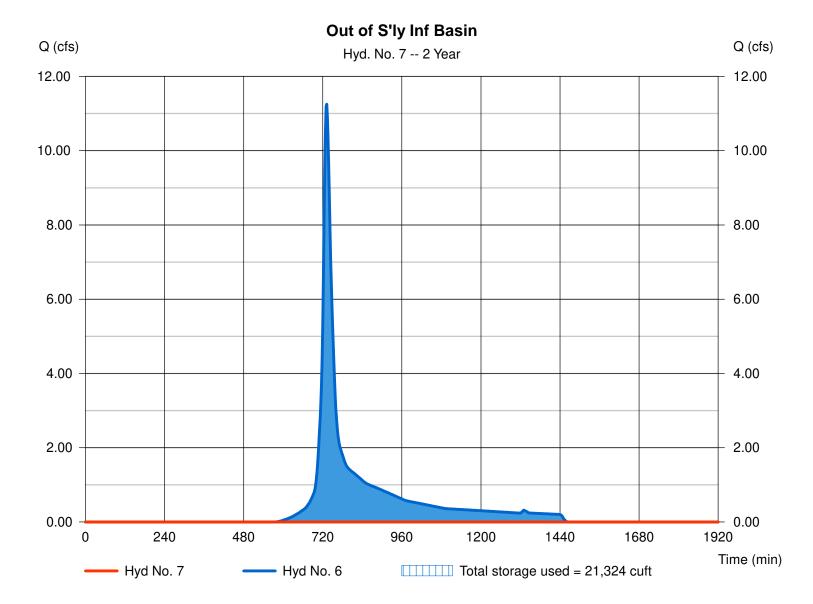
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### Hyd. No. 7

Out of S'ly Inf Basin

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 2 yrs	Time to peak	= 1410 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 6 - Proposed to S'ly Inf Basin	Max. Elevation	= 203.15 ft
Reservoir name	= S'ly Basin-Inf	Max. Storage	= 21,324 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



### **Pond Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

#### Pond No. 5 - S'ly Basin-Inf

#### **Pond Data**

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 200.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)	
0.00	200.00	4,779	0	0	
1.00	201.00	5,786	5,283	5,283	
2.00	202.00	7,236	6,511	11,794	
3.00	203.00	8,863	8,050	19,843	
4.00	204.00	10,781	9,822	29,665	
5.00	205.00	12,843	11,812	41,477	

#### **Culvert / Orifice Structures**

#### [A] [B] [C] [PrfRsr] [A] [B] [C] [D] = 0.00 0.00 0.00 = 12.00 0.00 0.00 Rise (in) 0.00 Crest Len (ft) 0.00 Span (in) = 0.00 0.00 0.00 0.00 Crest El. (ft) = 204.00 0.00 0.00 0.00 No. Barrels = 0 0 0 0 Weir Coeff. = 3.33 3.33 3.33 3.33 Invert El. (ft) = 0.00 0.00 0.00 0.00 Weir Type = Ciplti -----------= 0.00 0.00 0.00 0.00 Multi-Stage = No No No No Length (ft) = 0.00 0.00 0.00 Slope (%) n/a N-Value = .013 .013 .013 n/a Orifice Coeff. = 0.60 0.60 0.60 0.60 Exfil.(in/hr) = 6.000 (by Contour) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	200.00					0.00				0.000		0.000
1.00	5,283	201.00					0.00				0.804		0.804
2.00	11,794	202.00					0.00				1.005		1.005
3.00	19,843	203.00					0.00				1.231		1.231
4.00	29,665	204.00					0.00				1.497		1.497
5.00	41,477	205.00					39.96				1.784		41.74

30

#### Weir Structures

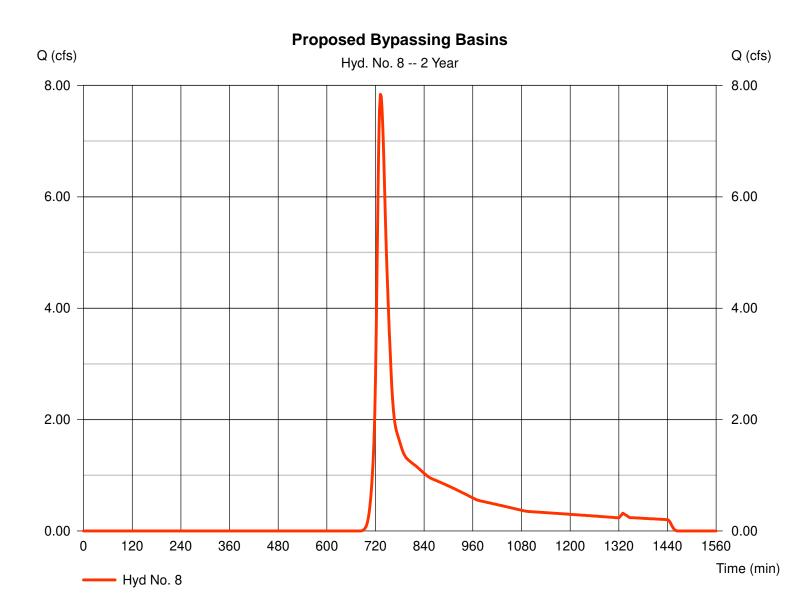
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

### Hyd. No. 8

Proposed Bypassing Basins

Hydrograph type	= SCS Runoff	Peak discharge	= 7.839 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 36,338 cuft
Drainage area	= 13.170 ac	Curve number	= 69*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.90 min
Total precip.	= 3.20 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.790 x 98) + (1.090 x 30) + (2.600 x 55) + (0.520 x 39) + (2.560 x 61) + (3.610 x 77)] / 13.170



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### Hyd. No. 8

Proposed Bypassing Basins

<b>Description</b>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.20 = 5.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 9.89	+	0.00	+	0.00	=	9.89
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 559.00 = 3.80 = Unpave = 3.15	d	68.00 2.30 Paved 3.08		66.00 1.00 Unpave 1.61	ed	
Travel Time (min)	= 2.96	+	0.37	+	0.68	=	4.01
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 1.77 = 4.71 = 1.10 = 0.013 = 6.23 = 222.0		3.14 6.28 2.00 0.013 10.19 105.0		3.14 6.28 0.60 0.013 5.58 419.0		
Travel Time (min)	= 0.59	+	0.17	+	1.25	=	2.02
Total Travel Time, Tc						15.90 min	

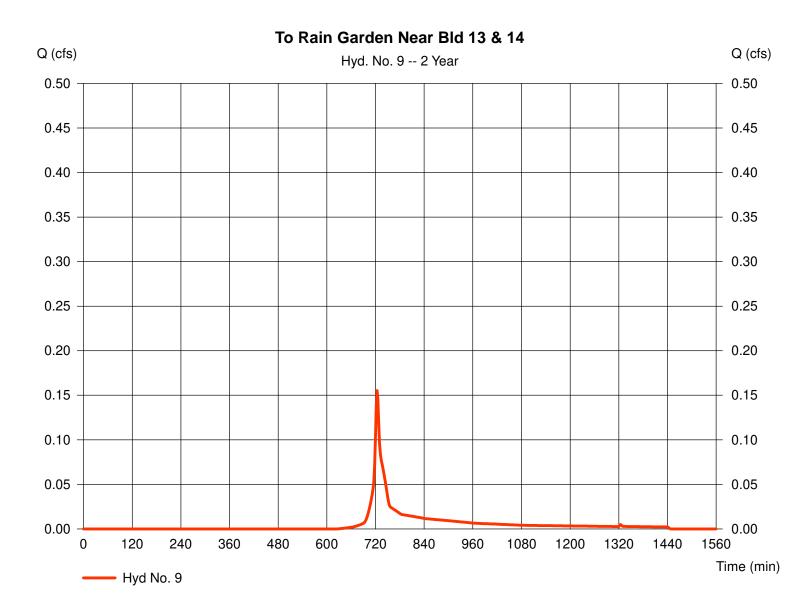
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### Hyd. No. 9

To Rain Garden Near Bld 13 & 14

Hydrograph type	= SCS Runoff	Peak discharge	= 0.155 cfs
Storm frequency	= 2 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 484 cuft
Drainage area	= 0.130 ac	Curve number	= 75*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= USER	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.20 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
· · ·			

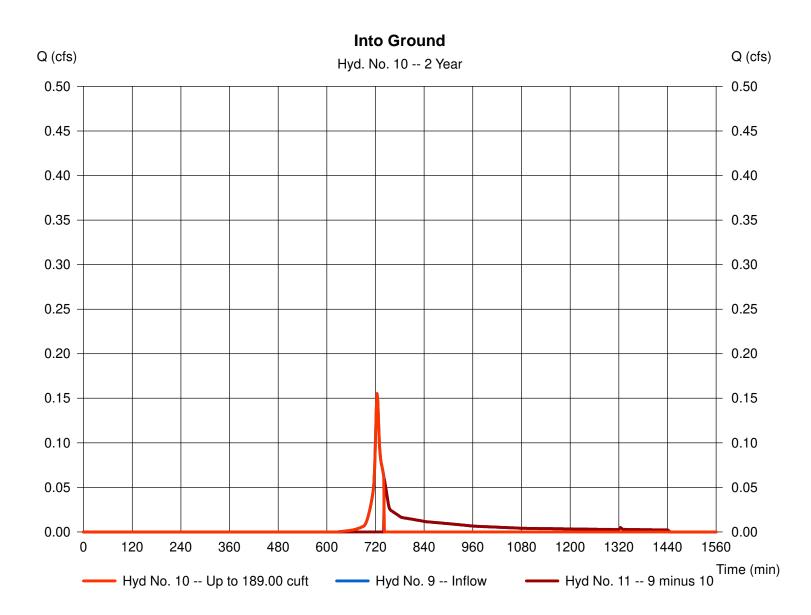
* Composite (Area/CN) = [(0.050 x 98) + (0.080 x 61)] / 0.130



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#### Hyd. No. 10

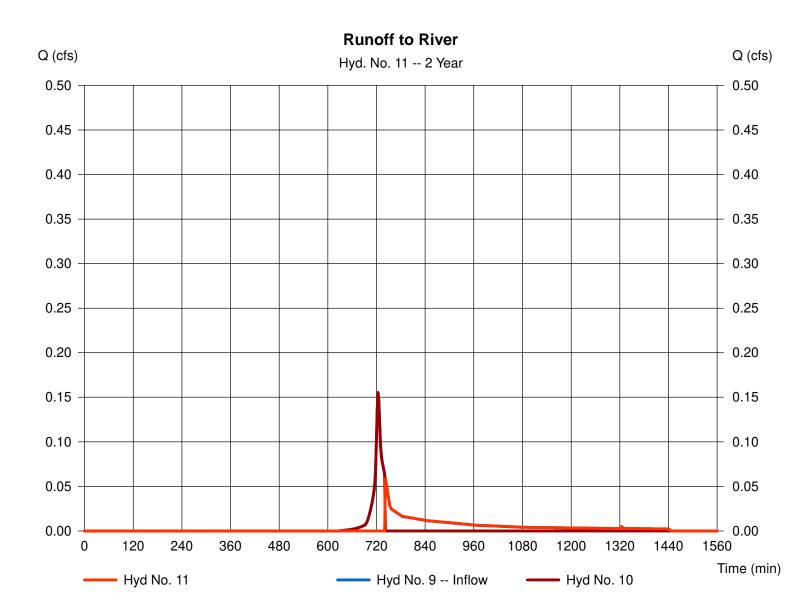
Into Ground



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#### Hyd. No. 11

Runoff to River

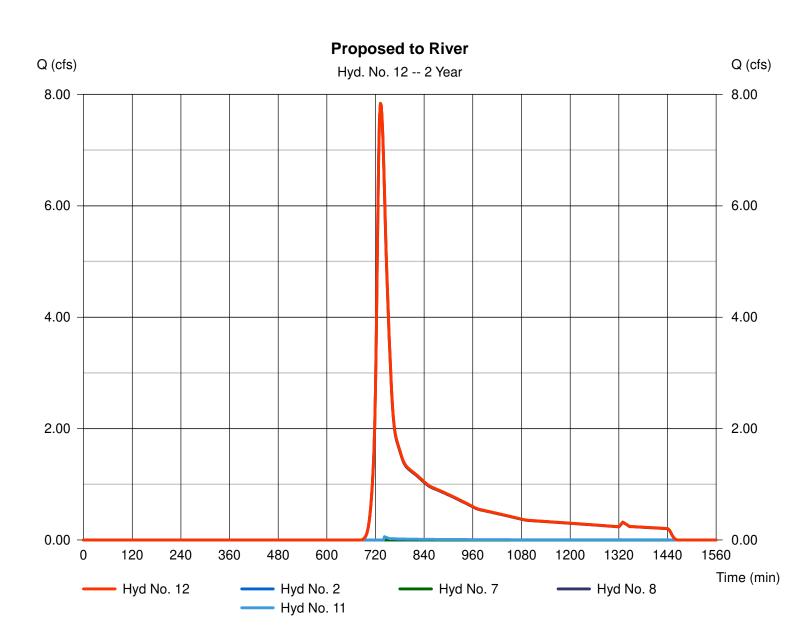


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#### Hyd. No. 12

Proposed to River

Hydrograph type	= Combine	Peak discharge	= 7.839 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 36,631 cuft
Inflow hyds.	= 2, 7, 8, 11	Contrib. drain. area	a = 13.170 ac



36

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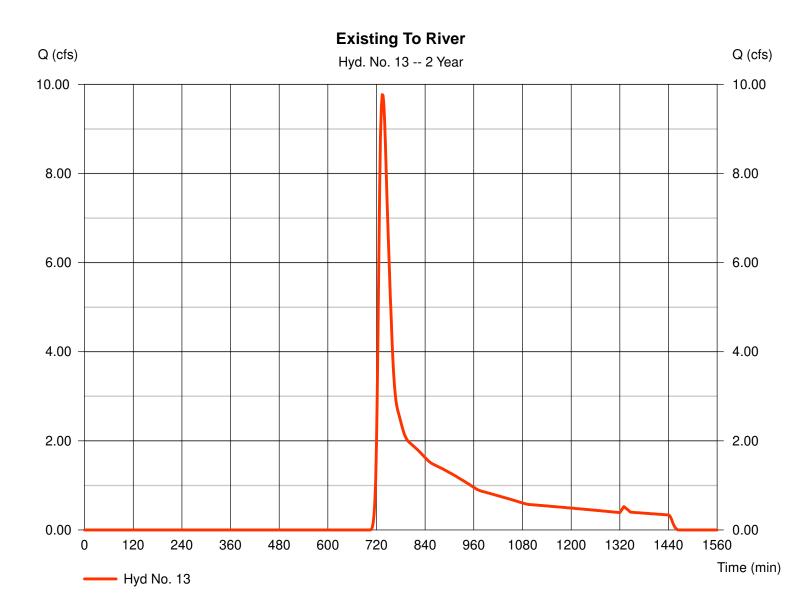
#### Thursday, Oct 8, 2020

### Hyd. No. 13

**Existing To River** 

Hydrograph type	= SCS Runoff	Peak discharge	= 9.773 cfs
Storm frequency	= 2 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 52,246 cuft
Drainage area	= 26.400 ac	Curve number	= 64*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.90 min
Total precip.	= 3.20 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) =  $[(4.310 \times 98) + (3.500 \times 30) + (8.910 \times 55) + (5.370 \times 77) + (0.780 \times 39) + (3.530 \times 61)] / 26.400$ 



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### Hyd. No. 13

Existing To River

<b>Description</b>	<u>A</u>	Ā		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	-			0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 9	.89 +	+	0.00	+	0.00	=	9.89
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 3	Inpaved		68.00 2.30 Paved 3.08		66.00 1.00 Unpaved 1.61	d	
Travel Time (min)	= 2	2.96 +	+	0.37	+	0.68	=	4.01
<b>Channel Flow</b> X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 6	.71 .10 .013		3.14 6.28 2.00 0.013 10.19 105.0		3.14 6.28 0.60 0.013 5.58 419.0		
Travel Time (min)	= 0	).59 +	+	0.17	+	1.25	=	2.02
Total Travel Time, Tc					15.90 min			

# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	3.123	2	724	9,383				Proposed To N'ly Basin
2	Reservoir	0.135	2	736	141	1	207.86	2,129	Out of N'ly Basin
3	SCS Runoff	10.07	2	732	41,617				Bypass To CulDeSac Drainage
4	Combine	10.18	2	732	41,758	2, 3			Total to CulDeSac Drainage
6	SCS Runoff	22.52	2	730	91,696				Proposed to S'ly Inf Basin
7	Reservoir	9.729	2	746	20,708	6	204.39	34,263	Out of S'ly Inf Basin
8	SCS Runoff	20.18	2	732	84,522				Proposed Bypassing Basins
9	SCS Runoff	0.338	2	724	1,012				To Rain Garden Near Bld 13 & 14
10	Diversion1	0.238	2	720	213	9			Into Ground
11	Diversion2	0.338	2	724	799	9			Runoff to River
12	Combine	22.39	2	744	106,170	2, 7, 8, 11			Proposed to River
13	SCS Runoff	31.15	2	732	135,690				Existing To River
15	SCS Runoff	0.179	2	742	1,223				CB1
16	Reservoir	0.000	2	780	0	15	208.19	62.6	Chambers at CB1
17	SCS Runoff	0.462	2	732	1,993				CB2
18	Reservoir	0.000	2	712	0	17	206.97	197	Chambers at CB2
19	SCS Runoff	0.363	2	734	1,620				CB3
20	Reservoir	0.000	2	892	0	19	202.41	200	Chambers at CB3
21	SCS Runoff	0.185	2	736	962				CB9
22	Reservoir	0.000	2	756	0	21	206.04	2.85	Chambers at CB9
23	SCS Runoff	0.387	2	736	1,907				CB10
24	Reservoir	0.000	2	726	0	23	205.51	56.2	Chambers at CB10
25	SCS Runoff	0.730	2	734	3,239				CB23
26	Reservoir	0.000	2	712	0	25	209.03	151	Chambers at CB23
576	8-Village-Nae	ek-Road.	gpw		Return P	l Period: 10 Y	/ear	Thursday,	Oct 8, 2020

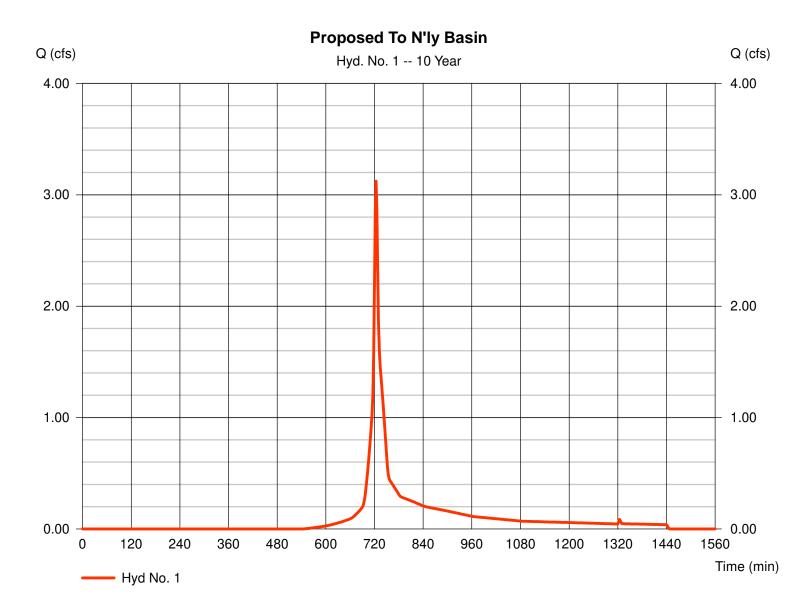
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### Hyd. No. 1

Proposed To N'ly Basin

Hydrograph type	= SCS Runoff	Peak discharge	= 3.123 cfs
Storm frequency	= 10 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 9,383 cuft
Drainage area	= 1.250 ac	Curve number	= 74*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 5.60 min
Total precip.	= 4.80 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(0.740 x 98) + (0.510 x 39)] / 1.250



Thursday, Oct 8, 2020

40

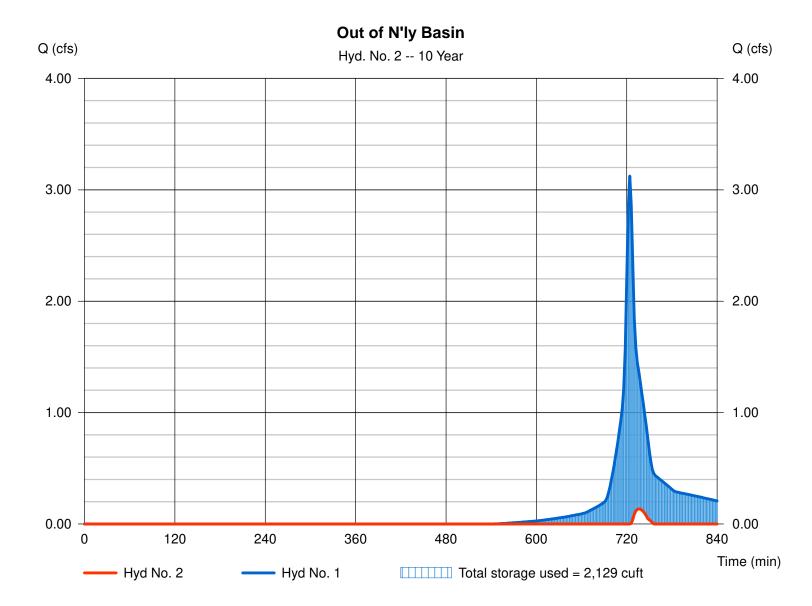
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#### Hyd. No. 2

Out of N'ly Basin

Hydrograph type	= Reservoir	Peak discharge	= 0.135 cfs
Storm frequency	= 10 yrs	Time to peak	= 736 min
Time interval	= 2 min	Hyd. volume	= 141 cuft
Inflow hyd. No.	= 1 - Proposed To N'ly Basin	Max. Elevation	= 207.86 ft
Reservoir name	<ul> <li>N'ly Infiltration Basin</li> </ul>	Max. Storage	= 2,129 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



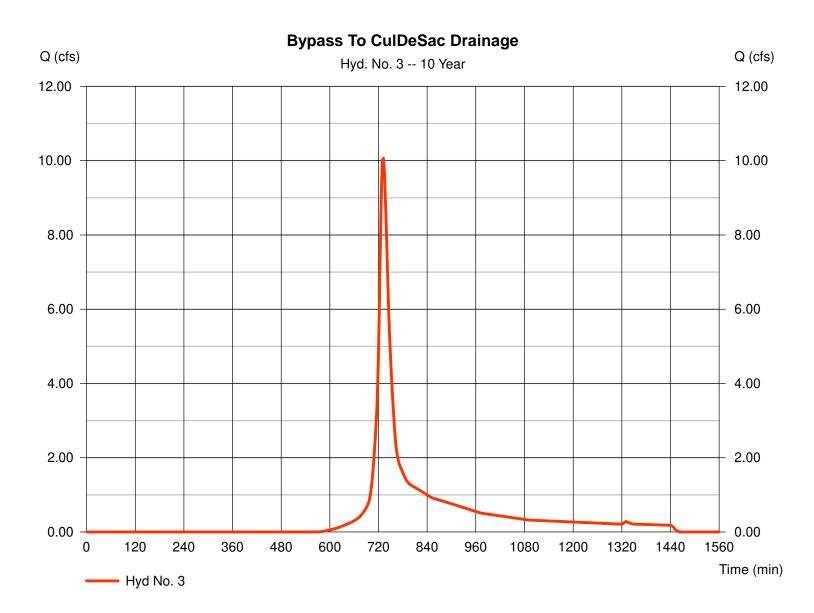
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### Hyd. No. 3

Bypass To CulDeSac Drainage

Hydrograph type	= SCS Runoff	Peak discharge	= 10.07 cfs
Storm frequency	= 10 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 41,617 cuft
Drainage area	= 5.750 ac	Curve number	= 72*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.10 min
Total precip.	= 4.80 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.430 x 98) + (0.480 x 30) + (0.920 x 55) + (0.320 x 39) + (1.600 x 61)] / 5.750

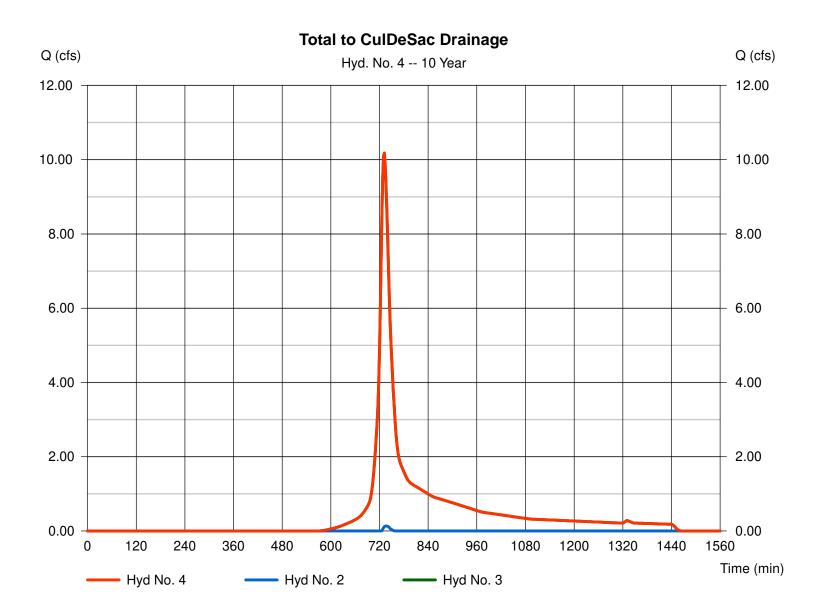


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### Hyd. No. 4

Total to CulDeSac Drainage

Hydrograph type	= Combine	Peak discharge	= 10.18 cfs
Storm frequency	= 10 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 41,758 cuft
Inflow hyds.	= 2, 3	Contrib. drain. area	a = 5.750 ac



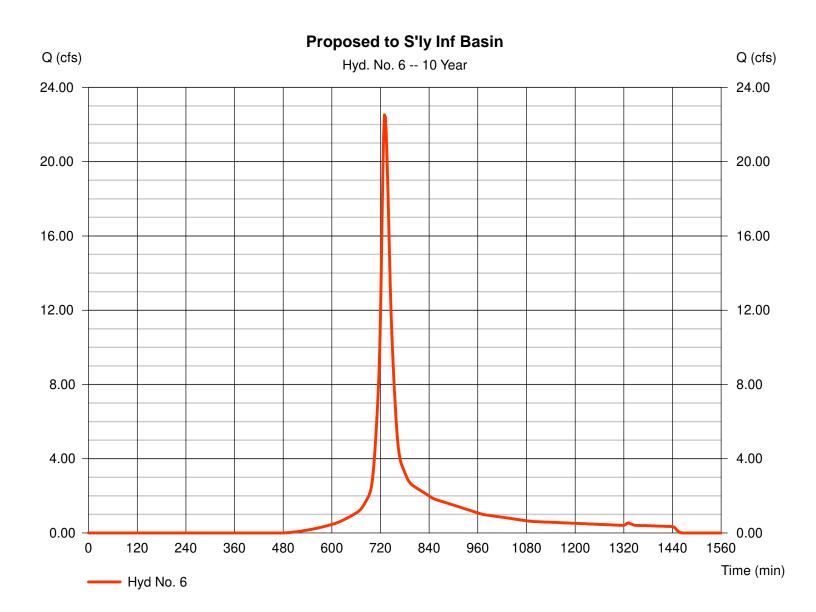
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### Hyd. No. 6

Proposed to S'ly Inf Basin

Hydrograph type	= SCS Runoff	Peak discharge	= 22.52 cfs
Storm frequency	= 10 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 91,696 cuft
Drainage area	= 9.850 ac	Curve number	= 79*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.10 min
Total precip.	= 4.80 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.550 x 98) + (0.020 x 30) + (1.540 x 55) + (1.080 x 80) + (2.660 x 61)] / 9.850



44

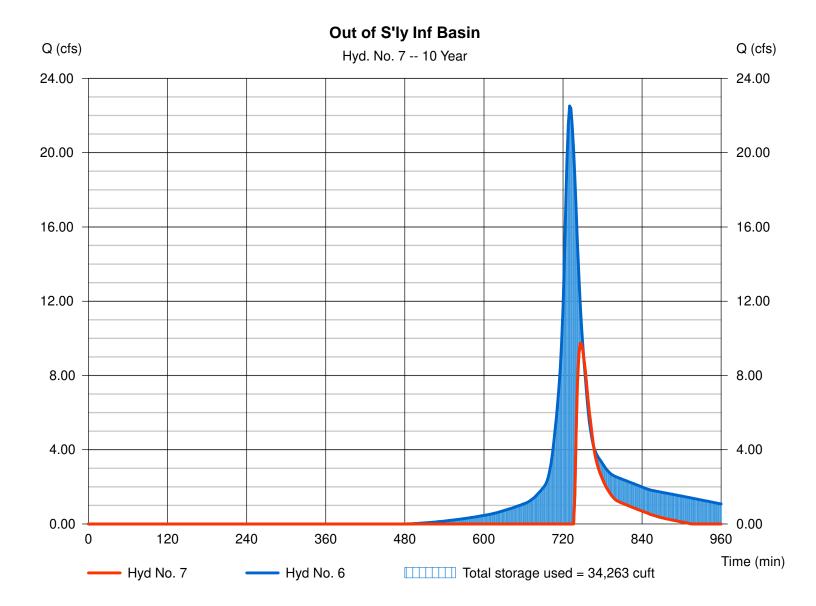
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### Hyd. No. 7

Out of S'ly Inf Basin

Hydrograph type	= Reservoir	Peak discharge	= 9.729 cfs
Storm frequency	= 10 yrs	Time to peak	= 746 min
Time interval	= 2 min	Hyd. volume	= 20,708 cuft
Inflow hyd. No.	= 6 - Proposed to S'ly Inf Basin	Max. Elevation	= 204.39 ft
Reservoir name	= S'ly Basin-Inf	Max. Storage	= 34,263 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



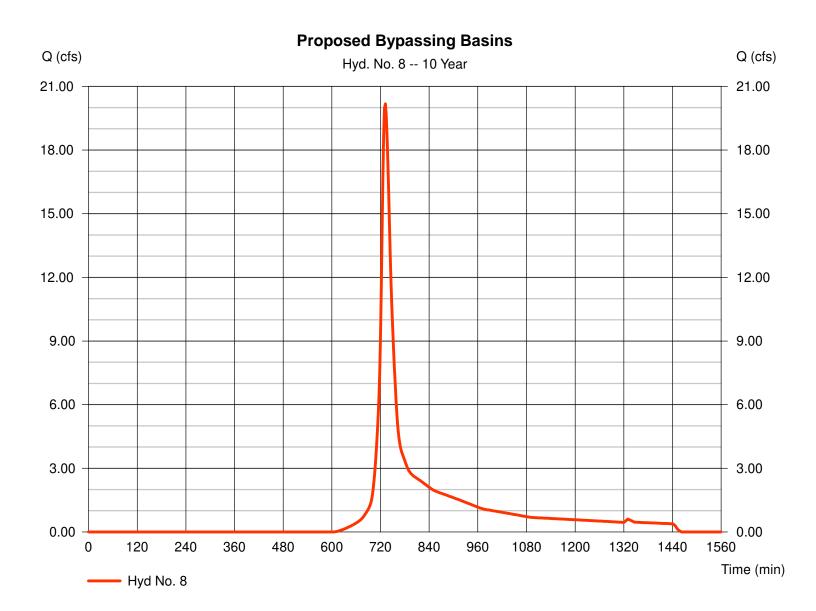
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### Hyd. No. 8

Proposed Bypassing Basins

Hydrograph type	= SCS Runoff	Peak discharge	= 20.18 cfs
Storm frequency	= 10 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 84,522 cuft
Drainage area	= 13.170 ac	Curve number	= 69*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.90 min
Total precip.	= 4.80 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	

* Composite  $(Area/CN) = [(2.790 \times 98) + (1.090 \times 30) + (2.600 \times 55) + (0.520 \times 39) + (2.560 \times 61) + (3.610 \times 77)] / 13.170$ 



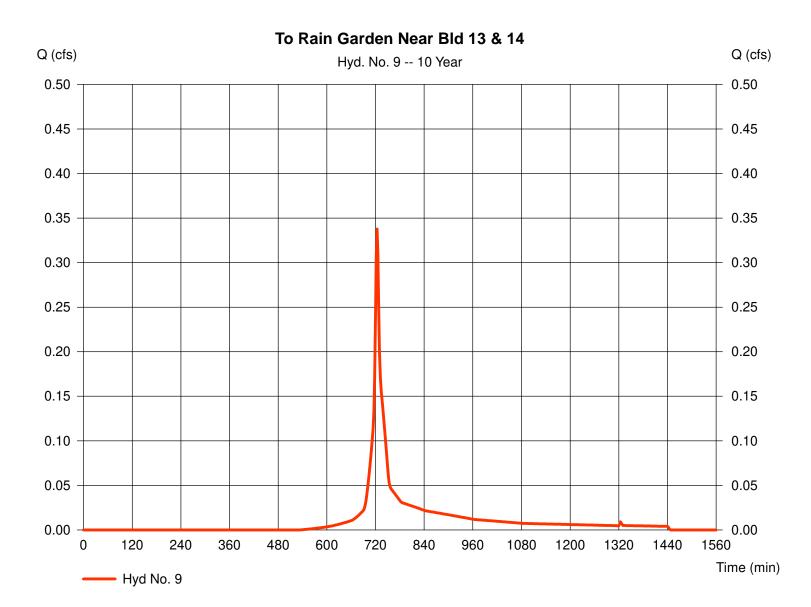
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### Hyd. No. 9

To Rain Garden Near Bld 13 & 14

Hydrograph type	= SCS Runoff	Peak discharge	= 0.338 cfs
Storm frequency	= 10 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 1,012 cuft
Drainage area	= 0.130 ac	Curve number	= 75*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= USER	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.80 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(0.050 x 98) + (0.080 x 61)] / 0.130



Thursday, Oct 8, 2020

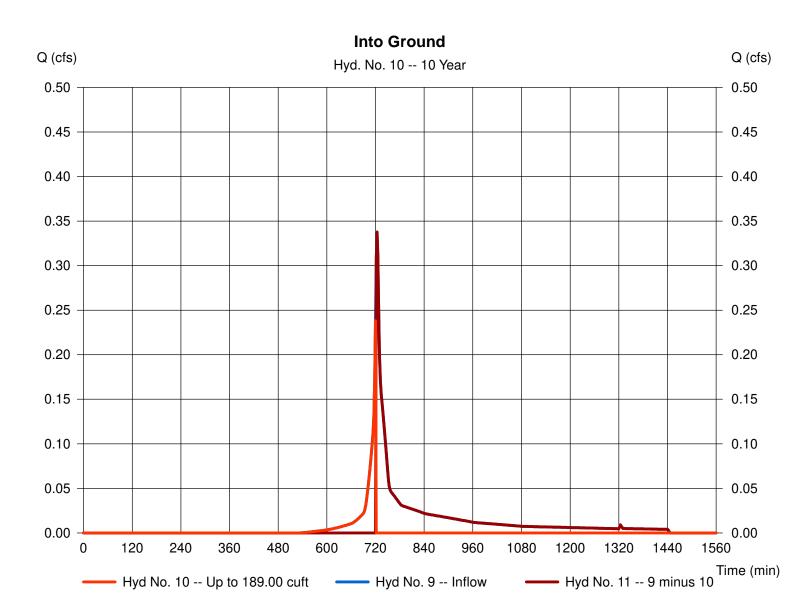
47

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#### Hyd. No. 10

Into Ground

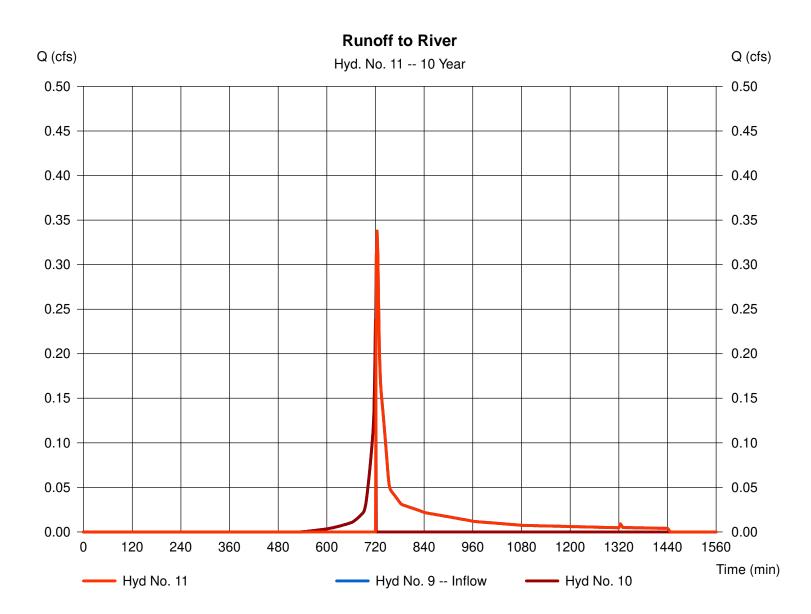
Hydrograph type	<ul> <li>Diversion1</li> <li>10 yrs</li> <li>2 min</li> <li>9 - To Rain Garden Near Bld 13 &amp; 14</li> </ul>	Peak discharge	= 0.238 cfs
Storm frequency		Time to peak	= 720 min
Time interval		Hyd. volume	= 213 cuft
Inflow hydrograph		2nd diverted hyd.	= 11
Diversion method	= First Flush Volume	Volume Up To	= 189.00  cuft



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#### Hyd. No. 11

Runoff to River

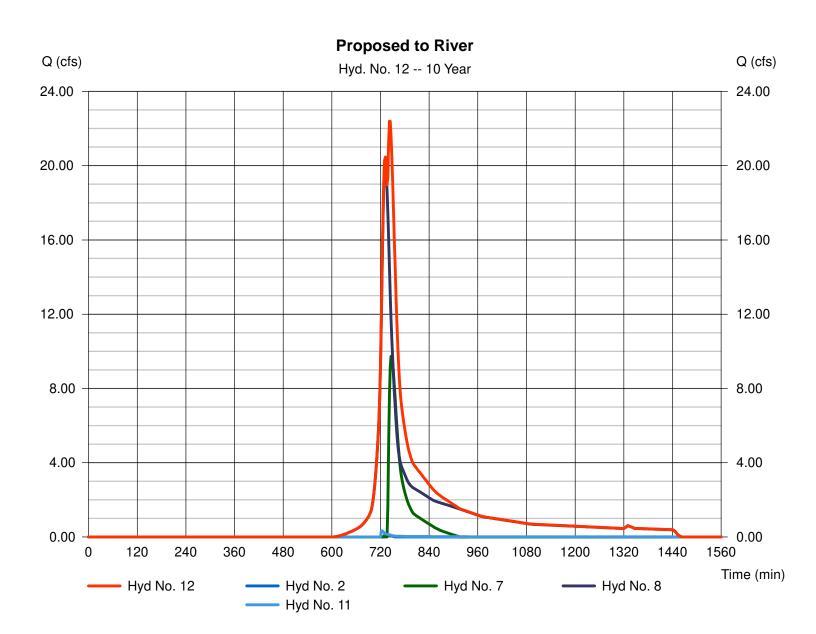


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#### Hyd. No. 12

Proposed to River

= Combine	Peak discharge	= 22.39 cfs
= 10 yrs	Time to peak	= 744 min
= 2 min	Hyd. volume	= 106,170 cuft
= 2, 7, 8, 11	Contrib. drain. area	1 = 13.170 ac
-	= 10 yrs = 2 min	= 10 yrs Time to peak = 2 min Hyd. volume



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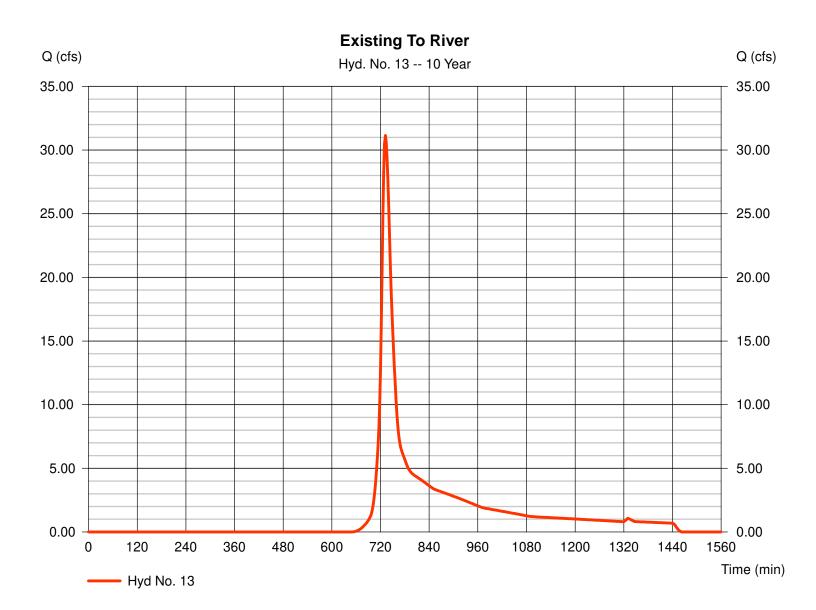
#### Thursday, Oct 8, 2020

### Hyd. No. 13

**Existing To River** 

Hydrograph type	= SCS Runoff	Peak discharge	= 31.15 cfs
Storm frequency	= 10 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 135,690 cuft
Drainage area	= 26.400 ac	Curve number	= 64*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.90 min
Total precip.	= 4.80 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) =  $[(4.310 \times 98) + (3.500 \times 30) + (8.910 \times 55) + (5.370 \times 77) + (0.780 \times 39) + (3.530 \times 61)] / 26.400$ 



51

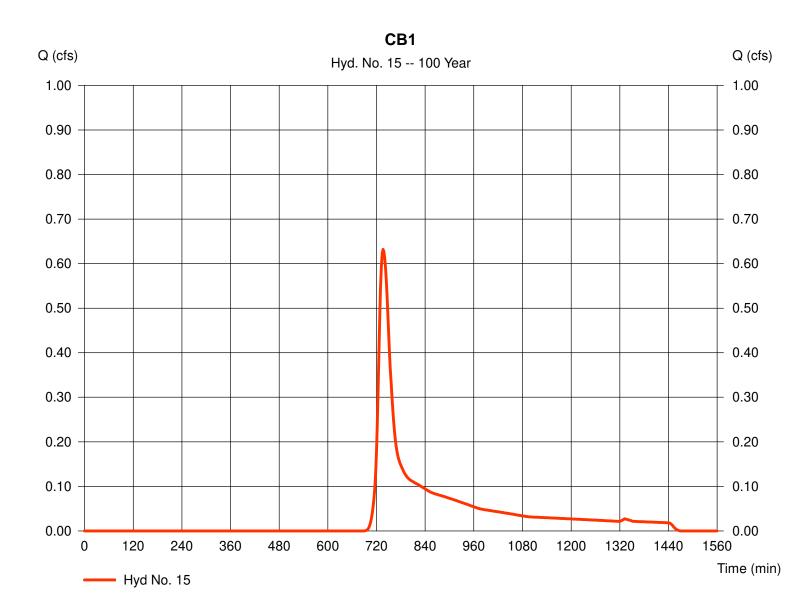
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#### Hyd. No. 15

#### CB1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.632 cfs
Storm frequency	= 100 yrs	Time to peak	= 736 min
Time interval	= 2 min	Hyd. volume	= 3,217 cuft
Drainage area	= 0.550 ac	Curve number	= 50*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 17.20 min
Total precip.	= 6.90 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) =  $[(0.080 \times 98) + (0.030 \times 55) + (0.400 \times 39) + (0.040 \times 61)] / 0.550$ 



52

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### Hyd. No. 15

CB1

<b>Description</b>		<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	=	0.400 62.0 3.20 4.00		0.240 38.0 3.20 4.00		0.011 0.0 0.00 0.00		
Travel Time (min)	=	11.10	+	4.99	+	0.00	=	16.09
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	=	190.00 7.00 Unpavec 4.27	ł	23.00 33.00 Unpave 9.27	d	35.00 1.00 Unpave 1.61	d	
Travel Time (min)	=	0.74	+	0.04	+	0.36	=	1.14
<b>Channel Flow</b> X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= = =	0.00 0.00 0.015 0.00 0.01		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							17.20 min	

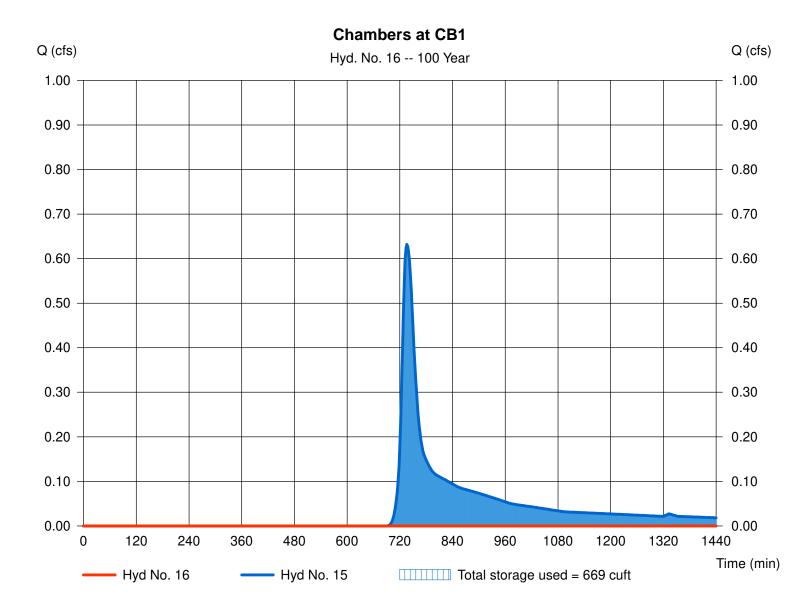
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#### Hyd. No. 16

Chambers at CB1

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 100 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 15 - CB1	Max. Elevation	= 211.49 ft
Reservoir name	= CB 1	Max. Storage	= 669 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



### **Pond Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Pond No. 6 - CB 1

#### Pond Data

**UG Chambers -** Invert elev. = 207.85 ft, Rise x Span =  $4.00 \times 4.00$  ft, Barrel Len = 40.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No **Encasement -** Invert elev. = 207.85 ft, Width = 6.00 ft, Height = 4.00 ft, Voids = 30.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	207.85	n/a	0	0
0.40	208.25	n/a	74	74
0.80	208.65	n/a	74	147
1.20	209.05	n/a	74	221
1.60	209.45	n/a	74	294
2.00	209.85	n/a	74	368
2.40	210.25	n/a	74	442
2.80	210.65	n/a	74	515
3.20	211.05	n/a	74	589
3.60	211.45	n/a	74	663
4.00	211.85	n/a	74	736

#### **Culvert / Orifice Structures**

#### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 20.500 (b	y Wet area	a)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

oluge	/ Otorage /	Disonarge	TUDIC										
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	207.85									0.000		0.000
0.40	74	208.25									0.129		0.129
0.80	147	208.65									0.144		0.144
1.20	221	209.05									0.159		0.159
1.60	294	209.45									0.175		0.175
2.00	368	209.85									0.190		0.190
2.40	442	210.25									0.205		0.205
2.80	515	210.65									0.220		0.220
3.20	589	211.05									0.235		0.235
3.60	663	211.45									0.251		0.251
4.00	736	211.85									0.266		0.266

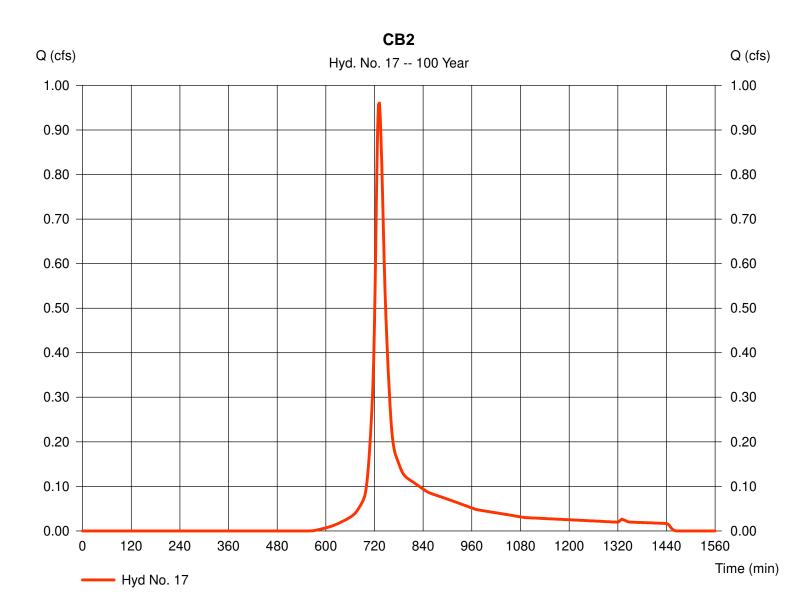
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#### Hyd. No. 17

CB2

Hydrograph type	= SCS Runoff	Peak discharge	= 0.961 cfs
Storm frequency	= 100 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 3,962 cuft
Drainage area	= 0.370 ac	Curve number	= 65*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.40 min
Total precip.	= 6.90 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(0.160 x 98) + (0.210 x 39)] / 0.370



56

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### Hyd. No. 17

CB2

Description	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 80.0 = 3.20 = 1.25	)	0.240 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 14.4	1 +	0.00	+	0.00	=	14.41
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 0.00 = 0.00 = Unpa = 0.00	ved	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	$\begin{array}{r} = \ 0.00 \\ = \ 0.00 \\ = \ 0.00 \\ = \ 0.015 \\ = \ 0.00 \\ = \ 0.0 \end{array}$	5	0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							

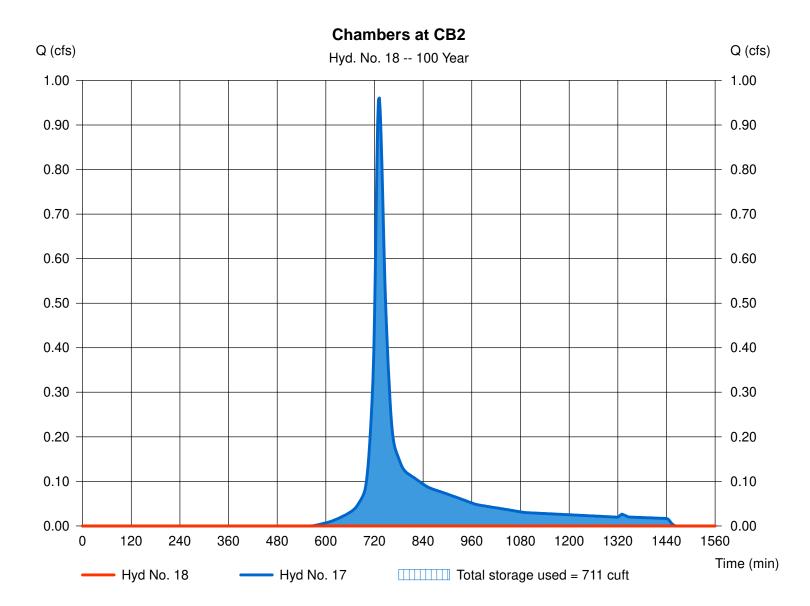
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#### Hyd. No. 18

Chambers at CB2

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 100 yrs	Time to peak	= 824 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow byd, No	= 17 - CB2	Max, Elevation	= 209 52 ft
Inflow hyd. No.	= 17 - CB2	Max. Elevation	= 209.52 ft
Reservoir name	= CB 2	Max. Storage	= 711 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



### **Pond Report**

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Pond No. 7 - CB 2

#### Pond Data

**UG Chambers -** Invert elev. = 206.00 ft, Rise x Span =  $4.00 \times 4.00$  ft, Barrel Len = 44.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No **Encasement -** Invert elev. = 206.00 ft, Width = 6.00 ft, Height = 4.00 ft, Voids = 30.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft) Contour area (sqft)		Incr. Storage (cuft)	Total storage (cuft)		
0.00	206.00	n/a	0	0		
0.40	206.40	n/a	81	81		
0.80	206.80	n/a	81	162		
1.20	207.20	n/a	81	243		
1.60	207.60	n/a	81	324		
2.00	208.00	n/a	81	405		
2.40	208.40	n/a	81	486		
2.80	208.80	n/a	81	567		
3.20	209.20	n/a	81	648		
3.60	209.60	n/a	81	729		
4.00	210.00	n/a	81	810		

#### **Culvert / Orifice Structures**

#### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 35.000 (k	by Wet area	a)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

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Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	206.00									0.000		0.000
0.40	81	206.40									0.242		0.242
0.80	162	206.80									0.271		0.271
1.20	243	207.20									0.299		0.299
1.60	324	207.60									0.328		0.328
2.00	405	208.00									0.356		0.356
2.40	486	208.40									0.385		0.385
2.80	567	208.80									0.414		0.414
3.20	648	209.20									0.442		0.442
3.60	729	209.60									0.471		0.471
4.00	810	210.00									0.499		0.499

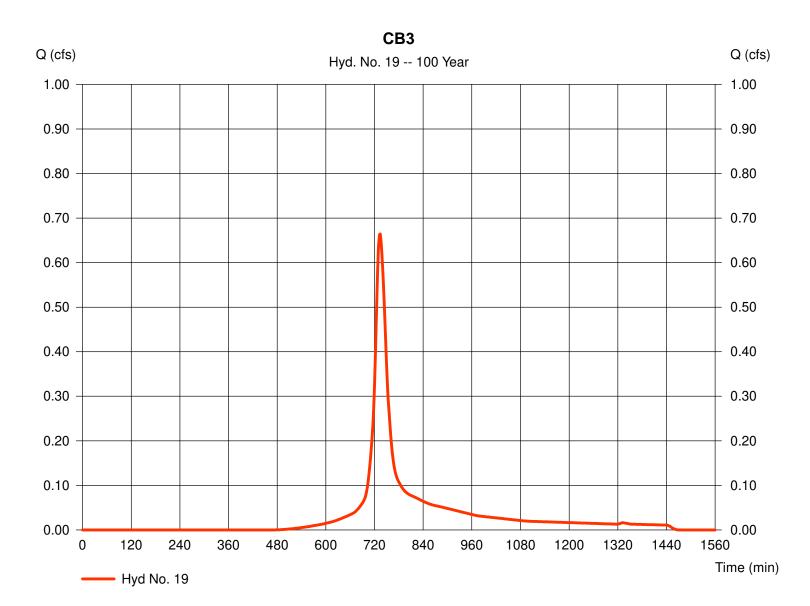
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#### Hyd. No. 19

CB3

Hydrograph type	= SCS Runoff	Peak discharge	= 0.664 cfs
Storm frequency	= 100 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 2,934 cuft
Drainage area	= 0.210  ac	Curve number	= 2,934 cuit = 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 18.50 min
Total precip.	= 6.90 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(0.120 x 98) + (0.090 x 39)] / 0.210



60

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### Hyd. No. 19

CB3

Description	A		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 35.0 = 3.20 = 5.00		0.240 65.0 3.20 1.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 4.27	+	13.34	+	0.00	=	17.61
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 85.00 = 1.00 = Unpavec = 1.61	ł	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.88	+	0.00	+	0.00	=	0.88
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	$\begin{array}{rcrr} = & 0.00 \\ = & 0.00 \\ = & 0.010 \\ = & 0.015 \\ = & 0.00 \\ = & 0.0 \end{array}$		0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							18.50 min

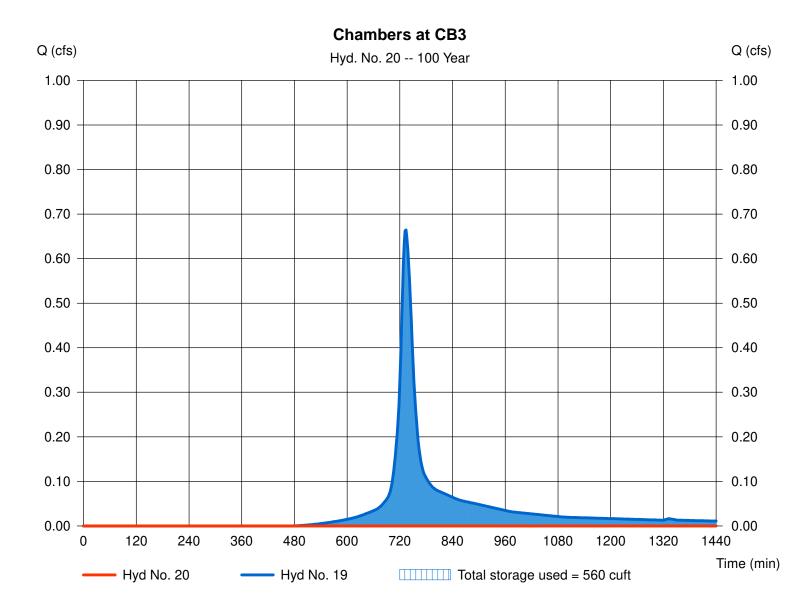
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### Hyd. No. 20

Chambers at CB3

cfs
in
3 ft
uft

Storage Indication method used. Exfiltration extracted from Outflow.



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Pond No. 8 - CB 3

### Pond Data

**UG Chambers -** Invert elev. = 201.20 ft, Rise x Span =  $4.00 \times 4.00$  ft, Barrel Len = 36.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No **Encasement -** Invert elev. = 201.20 ft, Width = 6.00 ft, Height = 4.00 ft, Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	201.20	n/a	0	0
0.40	201.60	n/a	66	66
0.80	202.00	n/a	66	133
1.20	202.40	n/a	66	199
1.60	202.80	n/a	66	265
2.00	203.20	n/a	66	331
2.40	203.60	n/a	66	398
2.80	204.00	n/a	66	464
3.20	204.40	n/a	66	530
3.60	204.80	n/a	66	596
4.00	205.20	n/a	66	663

### **Culvert / Orifice Structures**

#### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 30.500 (b	by Wet area	a)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

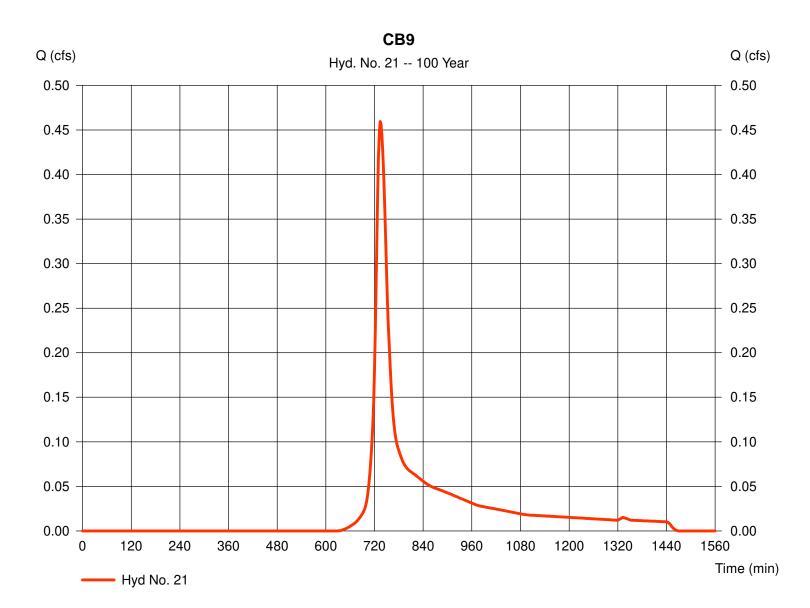
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Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	201.20									0.000		0.000
0.40	66	201.60									0.173		0.173
0.80	133	202.00									0.193		0.193
1.20	199	202.40									0.213		0.213
1.60	265	202.80									0.234		0.234
2.00	331	203.20									0.254		0.254
2.40	398	203.60									0.274		0.274
2.80	464	204.00									0.295		0.295
3.20	530	204.40									0.315		0.315
3.60	596	204.80									0.335		0.335
4.00	663	205.20									0.356		0.356

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### Hyd. No. 21

CB9

* Composite (Area/CN) = [(0.080 x 98) + (0.170 x 39)] / 0.250



64

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## Hyd. No. 21

CB9

Description		<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= =	0.240 100.0 3.20 1.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	=	18.83	+	0.00	+	0.00	=	18.83
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= =	83.00 1.00 Unpaved 1.61		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	=	0.86	+	0.00	+	0.00	=	0.86
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= = =	0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc								19.70 min

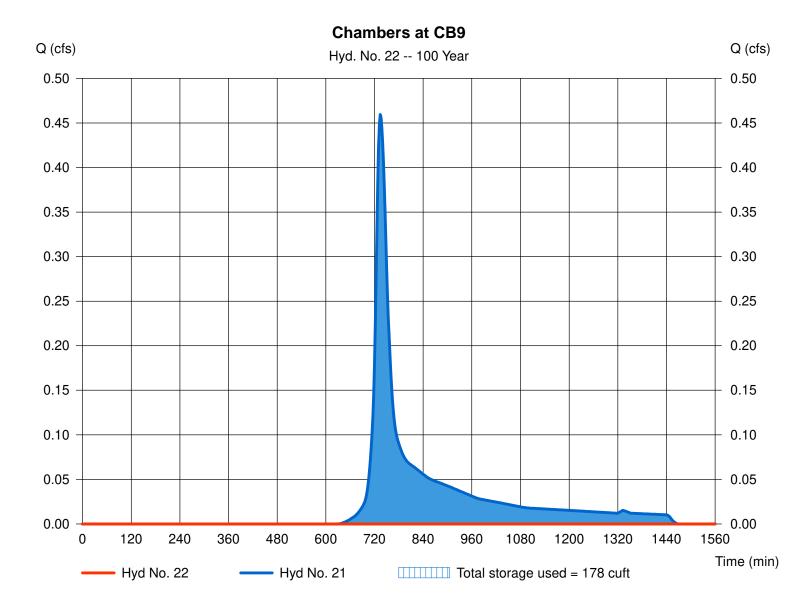
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### Hyd. No. 22

Chambers at CB9

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 100 yrs	Time to peak	= 712 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 21 - CB9	Max. Elevation	= 208.43 ft
Reservoir name	= CB 9	Max. Storage	= 178 cuft
		-	

Storage Indication method used. Exfiltration extracted from Outflow.



66

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#### Pond No. 9 - CB 9

### Pond Data

**UG Chambers -** Invert elev. = 206.00 ft, Rise x Span =  $4.00 \times 4.00$  ft, Barrel Len = 16.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No **Encasement -** Invert elev. = 206.00 ft, Width = 6.00 ft, Height = 4.00 ft, Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	206.00	n/a	0	0
0.40	206.40	n/a	29	29
0.80	206.80	n/a	29	59
1.20	207.20	n/a	29	88
1.60	207.60	n/a	29	118
2.00	208.00	n/a	29	147
2.40	208.40	n/a	29	177
2.80	208.80	n/a	29	206
3.20	209.20	n/a	29	236
3.60	209.60	n/a	29	265
4.00	210.00	n/a	29	294

### **Culvert / Orifice Structures**

### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 85.000 (b	y Wet area	a)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

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Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	206.00									0.000		0.000
0.40	29	206.40									0.214		0.214
0.80	59	206.80									0.239		0.239
1.20	88	207.20									0.264		0.264
1.60	118	207.60									0.290		0.290
2.00	147	208.00									0.315		0.315
2.40	177	208.40									0.340		0.340
2.80	206	208.80									0.365		0.365
3.20	236	209.20									0.390		0.390
3.60	265	209.60									0.416		0.416
4.00	294	210.00									0.441		0.441

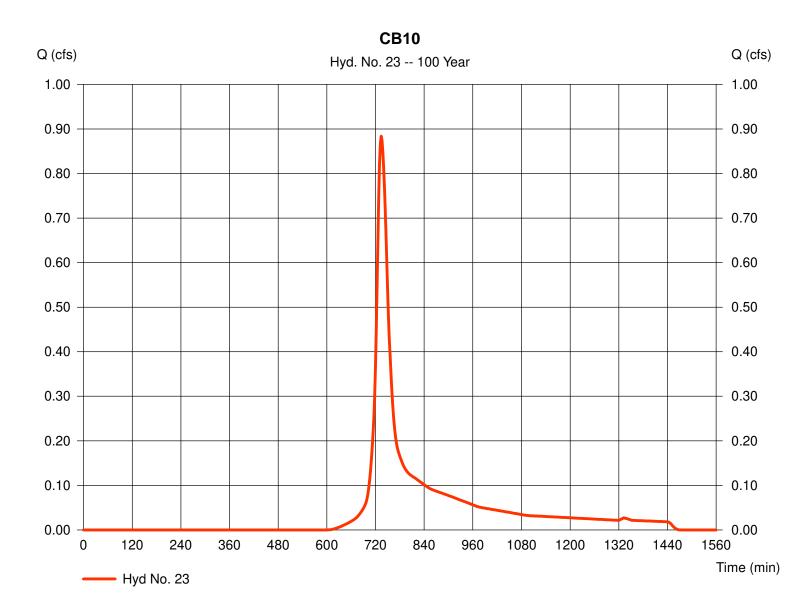
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### Hyd. No. 23

CB10

Hydrograph type	= SCS Runoff	Peak discharge	= 0.884 cfs
Storm frequency	= 100 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 4,010 cuft
Drainage area	= 0.420 ac	Curve number	= 61*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 19.60 min
Total precip.	= 6.90 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(0.160 x 98) + (0.260 x 39)] / 0.420



68

Thursday, Oct 8, 2020

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## Hyd. No. 23

CB10

<b>Description</b>		<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>		
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= =	0.240 100.0 3.20 1.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00				
Travel Time (min)	=	18.83	+	0.00	+	0.00	=	18.83		
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= =	91.00 1.70 Unpaved 2.10		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00				
Travel Time (min)	=	0.72	+	0.00	+	0.00	=	0.72		
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= = =	0.00 0.00 0.015 0.00 0.015		0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.015 0.00 0.0				
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00		
Total Travel Time, Tc	Total Travel Time, Tc									

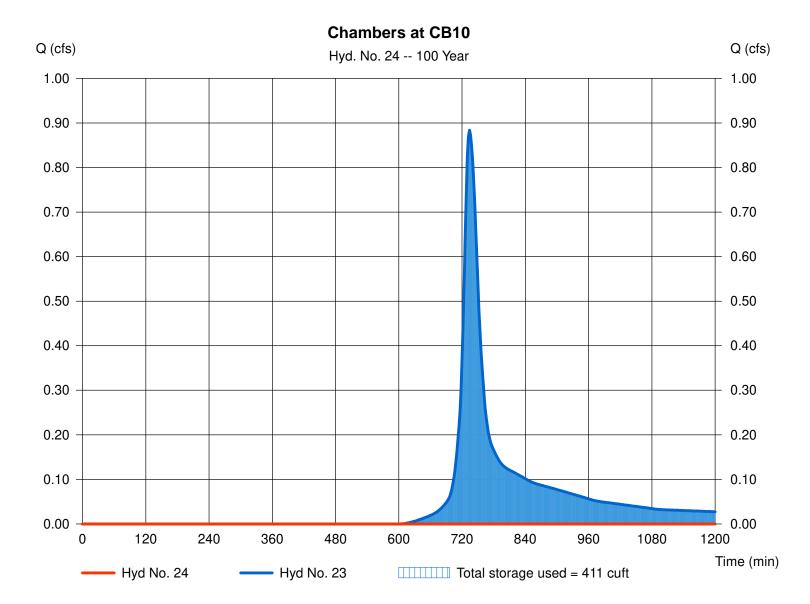
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### Hyd. No. 24

Chambers at CB10

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 100 yrs	Time to peak	= 810 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 23 - CB10	Max. Elevation	= 208.73 ft
Reservoir name	= CB 10	Max. Storage	= 411 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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70

Thursday, Oct 8, 2020

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#### Pond No. 10 - CB 10

#### Pond Data

**UG Chambers -** Invert elev. = 205.00 ft, Rise x Span =  $4.00 \times 4.00 \text{ ft}$ , Barrel Len = 24.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No **Encasement -** Invert elev. = 205.00 ft, Width = 6.00 ft, Height = 4.00 ft, Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	205.00	n/a	0	0
0.40	205.40	n/a	44	44
0.80	205.80	n/a	44	88
1.20	206.20	n/a	44	133
1.60	206.60	n/a	44	177
2.00	207.00	n/a	44	221
2.40	207.40	n/a	44	265
2.80	207.80	n/a	44	309
3.20	208.20	n/a	44	353
3.60	208.60	n/a	44	398
4.00	209.00	n/a	44	442

### **Culvert / Orifice Structures**

#### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 85.000 (b	y Wet area	a)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

Oluge /	otoruge / i	Disonarge	labic										
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	205.00									0.000		0.000
0.40	44	205.40									0.321		0.321
0.80	88	205.80									0.359		0.359
1.20	133	206.20									0.397		0.397
1.60	177	206.60									0.434		0.434
2.00	221	207.00									0.472		0.472
2.40	265	207.40									0.510		0.510
2.80	309	207.80									0.548		0.548
3.20	353	208.20									0.586		0.586
3.60	398	208.60									0.623		0.623
4.00	442	209.00									0.661		0.661

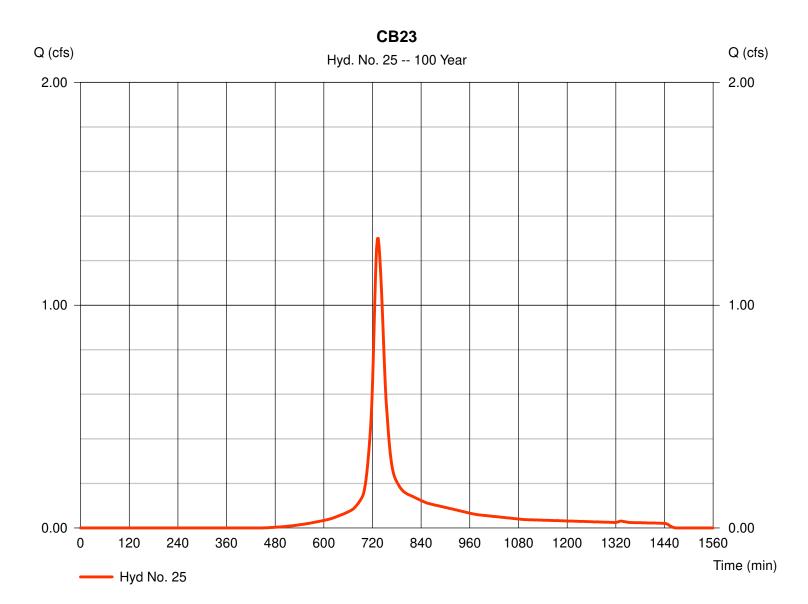
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

## Hyd. No. 25

### CB23

Hydrograph type	= SCS Runoff	Peak discharge	= 1.300 cfs
Storm frequency	= 100 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 5,750 cuft
Drainage area	= 0.390 ac	Curve number	= 75*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 17.40 min
Total precip.	= 6.90 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(0.200 x 98) + (0.110 x 61) + (0.080 x 39)] / 0.390



Thursday, Oct 8, 2020

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

## Hyd. No. 25

CB23

Description	<u>A</u>		<u>B</u>		<u>C</u>		<b>Totals</b>
<b>Sheet Flow</b> Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.20 = 1.40		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 16.46	+	0.00	+	0.00	=	16.46
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 112.00 = 1.40 = Unpay = 1.91	-	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.98	+	0.00	+	0.00	=	0.98
<b>Channel Flow</b> X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	$\begin{array}{r} = \ 0.00 \\ = \ 0.00 \\ = \ 0.015 \\ = \ 0.00 \\ = \ 0.00 \\ = \ 0.0 \end{array}$		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							17.40 min

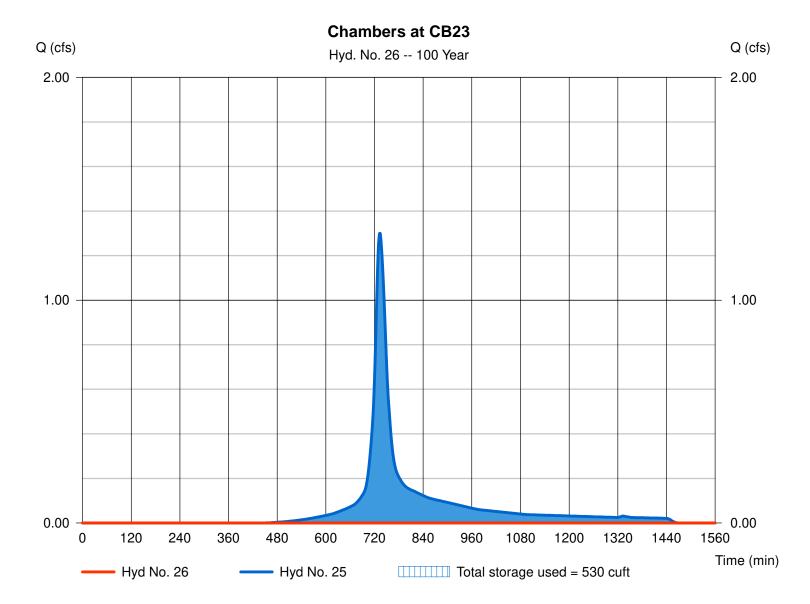
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### Hyd. No. 26

Chambers at CB23

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 100 yrs	Time to peak	= 786 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 25 - CB23	Max. Elevation	= 211.60 ft
Reservoir name	= CB 23	Max. Storage	= 530 cuft
Inflow hyd. No.	= 25 - CB23	Max. Elevation	= 211.60 ft

Storage Indication method used. Exfiltration extracted from Outflow.



74

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#### Pond No. 11 - CB 23

### Pond Data

**UG Chambers -** Invert elev. = 208.00 ft, Rise x Span =  $4.00 \times 4.00$  ft, Barrel Len = 16.00 ft, No. Barrels = 2, Slope = 0.00%, Headers = No **Encasement -** Invert elev. = 208.00 ft, Width = 6.00 ft, Height = 4.00 ft, Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	208.00	n/a	0	0
0.40	208.40	n/a	59	59
0.80	208.80	n/a	59	118
1.20	209.20	n/a	59	177
1.60	209.60	n/a	59	236
2.00	210.00	n/a	59	294
2.40	210.40	n/a	59	353
2.80	210.80	n/a	59	412
3.20	211.20	n/a	59	471
3.60	211.60	n/a	59	530
4.00	212.00	n/a	59	589

### **Culvert / Orifice Structures**

### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a	-				
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 100.000	(by Wet are	ea)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage /	Storage /	Discharge 1	Table	ince outlows a	re analyzed un								gence (3).
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	208.00									0.000		0.000
0.40	59	208.40									0.504		0.504
0.80	118	208.80									0.563		0.563
1.20	177	209.20									0.622		0.622
1.60	236	209.60									0.681		0.681
2.00	294	210.00									0.741		0.741
2.40	353	210.40									0.800		0.800
2.80	412	210.80									0.859		0.859
3.20	471	211.20									0.919		0.919
3.60	530	211.60									0.978		0.978
4.00	589	212.00									1.037		1.037

# **Hydraflow Rainfall Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2009 by Autodesk, Inc. v6.066

Return Period	Intensity-I	Duration-Frequency	Equation Coefficient	ts (FHA)
(Yrs)	В	D	E	(N/A)
1	26.1693	6.2000	0.7786	
2	30.1225	6.6000	0.7676	
3	0.0000	0.0000	0.0000	
5	52.3308	9.8000	0.8367	
10	54.7383	10.8000	0.8016	
25	101.9813	15.8000	0.8971	
50	98.1551	15.7000	0.8577	
100	106.5909	17.0000	0.8462	
	1		1	1

File name: CT-DOT.IDF

### Intensity = B / (Tc + D)^E

Return Period		Intensity Values (in/hr)										
(Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	3.99	2.99	2.43	2.06	1.80	1.60	1.45	1.32	1.22	1.14	1.06	1.00
2	4.59	3.49	2.85	2.43	2.13	1.90	1.72	1.58	1.46	1.36	1.27	1.20
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	5.49	4.30	3.57	3.06	2.69	2.40	2.17	1.99	1.84	1.71	1.60	1.50
10	5.99	4.81	4.04	3.51	3.11	2.80	2.55	2.35	2.18	2.03	1.91	1.80
25	6.70	5.52	4.71	4.12	3.66	3.30	3.01	2.76	2.56	2.38	2.23	2.10
50	7.30	6.06	5.20	4.57	4.09	3.70	3.38	3.12	2.90	2.71	2.54	2.40
100	7.79	6.55	5.68	5.02	4.51	4.10	3.76	3.48	3.24	3.04	2.86	2.70

Tc = time in minutes. Values may exceed 60.

	Precip. file name: TollandCounty.pcp							
Storm Distribution	Rainfall Precipitation Table (in)							
	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	2.60	3.20	0.00	4.10	4.80	5.50	6.20	6.90
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Thursday, Oct 8, 2020